## Gurotec

The specialist for fastening technologie

# FASTENING FOR THE ■ CONSTRUCTION WITH CLT 

WOOD CONNECTORS
SCREWS

BIM-PORTAL

SPECIAL COMPONENIS

## f © 》 温 in



## Solid timber construction

| Product finder | $4-5$ |
| :--- | ---: |
| Company portrait | $6-9$ |
| Eurotec Coach | 10 |
| Eurotec BIM online portal | 11 |
| CLT Basics | $12-15$ |
| Wood connectors | $16-73$ |
| Screws | $74-133$ |
| Further products | $134-175$ |
| Special components | $176-178$ |

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## PRODUCT FINDER

|  | Sill plate | Wall-Concrete | Wall-Wall | Beam | Wall-Ceiling |
| :---: | :---: | :---: | :---: | :---: | :---: |
| WOOD CONNECTORS |  |  |  |  |  |
| CLT system inside corner | x | x | $\checkmark$ | x | $\checkmark$ |
| CLT system angle | x | x | $\checkmark$ | $x$ | $\checkmark$ |
| Shearing angle | x | $\checkmark$ | $\checkmark$ | x | $\checkmark$ |
| HB flat shearing angle | x | $\checkmark$ | $x$ | x | $x$ |
| HH flat shearing angle | x | x | x | x | x |
| Shearing plate | x | $\checkmark$ | $\checkmark$ | x | $x$ |
| Tension strap HB60/70 | $\checkmark$ | $\checkmark$ | x | x | x |
| Tension strap HH60/70 | x | x | $\checkmark$ | x | $\checkmark$ |
| Shear wall connector | x | x | $\checkmark$ | x | x |
| Assembly connector | x | x | $\checkmark$ | x | $x$ |
| Magnus hook connector | x | x | x | $\checkmark$ | $x$ |
| T-profile | x | x | x | $\checkmark$ | x |
| Hidden ground anchor | x | x | x | x | $\checkmark$ |

## SCREWS

| Rock concrete screw | $\checkmark$ | $\checkmark$ | x | x | x |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Konstrux fully treaded screw | x | x | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| Angle-bracket screw | x | $\checkmark$ | $\checkmark$ | x | $\checkmark$ |
| Panelwwistec | x | x | $\checkmark$ | $\checkmark$ | r |
| SawTec | x | x | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| Topdvo rooting screw | x | x | x | x | x |

## FURTHER PRODUCTS

| Lifting anchor, ball supporting bolt | x | x | x | x | x |
| :---: | :---: | :---: | :---: | :---: | :---: |
| IdeeFix | x | $\checkmark$ | x | $\checkmark$ | $\checkmark$ |
| SonoTec sound insulation cork | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| Bolt anchor | $\checkmark$ | x | x | x | $x$ |
| Silent EPDM decoupling profile | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| Ecktec | x | x | x | x | x |

$\checkmark$ USABLE XNOT USABLE $\quad-$ RREEEVANT

| Ceiling-Ceiling | Wall-Floor | Roof | Stairs | Insulation | Handling | Page |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| x | $\checkmark$ | - | - | - | - | 18-23 |
| x | $\checkmark$ | - | - | - | - | 24-27 |
| x | $\checkmark$ | - | - | - | - | 28-31 |
| x | x | - | - | - | - | 32-33 |
| $x$ | $\checkmark$ | - | - | - | - | 34-35 |
| x | x | - | - | - | - | 36-39 |
| $x$ | x | - | - | - | - | 40-41 |
| x | $\checkmark$ | - | - | - | - | 42-43 |
| x | x | - | - | - | - | 44-45 |
| $x$ | x | - | - | - | $\checkmark$ | 46-47 |
| x | $x$ | - | - | - | - | 48-67 |
| x | $\times$ | - | - | - | - | 68-71 |
| x | $\checkmark$ |  | - |  | - | 72-73 |


| x | x | x | x | x | - | 76-79 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | - | 80-107 |
| $\checkmark$ | $\checkmark$ | x | x | $\times$ | - | 108-109 |
| $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | - | 110-123 |
| $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | - | 124-127 |
| $\times$ | $\times$ | x | x | $\checkmark$ | - | 128-133 |
| x | x | x | x | x | $\checkmark$ | 136-147 |
| x | $\checkmark$ | $\times$ | x | $\times$ | - | 148-154 |
| $\checkmark$ | $\checkmark$ | $\checkmark$ | x | $\times$ | - | 156-167 |
| $\times$ | $\times$ | $\times$ | x | $x$ | - | 168-171 |
| $\checkmark$ | $\checkmark$ | x | $\checkmark$ | x | - | 172-173 |
| x | x | $\times$ | x | $\times$ | x | 174-175 |

We are a medium-sized company engaged in the development, production and sale of products for the construction sector. To this end, we supply products
for the areas of timber-frame construction, deck construction and concrete fastening. We supply specialist dealers across Europe, who are responsible for distribution to skilled craftsmen.

## OUR MILESTONES

## 1999

The two managing directors, Gregor Mamys and Markus Rensburg, founded Eurotec GmbH on 1 May 1999. The company began its life in a small basement with an adjoining garage, whose 5 pallet bays served as a warehouse.

## 2003

After multiple relocations within Hagen, the decision was made in 2003 to move to a company building in Werkzeugstraße. At the time, the warehouse had space for approx. 300 pallet bays.
This warehouse also quickly became too small. After several expansions, capacity ran out and it was time for a new company building! The managing directors looked for and found a suitable location in Hagen.

## 2007

In 2007, the Eurotec team and its 30 members of staff moved into the new building at Unter dem Hofe 5 . These newly built premises consisted of an office wing and an adjoining warehouse with approx. 3,500 pallet bays.

## 2010

Just three years later, the new building would, in turn, become the old building. A new warehouse building was built, providing a further 7,500 pallet bays and offices upstairs.

## 2012

In 2012, we decided to take the next important step. The foundation stone was laid for the production hall, paving the way for in-house production.

## 2013

From 7 January 2013 onwards,we produced a selected part of our proprietary product range in our own production hall in Hagen.

## 2014

In 2014, intensive work began on further expanding in-house production.

## 2015

Production capacity is expanded in 2015 to enable us to offer a wide range of solutions from our very own production facilities.

## 2016

In 2016, the company starts actively to build a new hall to relocate its machinery. Additional office space is being created in Hagen, since the company is enjoying steady growth. The next step is to expand the storage capacities in what was formerly the machinery hall.

## 2018

Completion of the new production hall in early 2018 means that all of the machinery can be moved. Construction work starts on another warehouse.

## 2019

On 1 May 2019 we celebrated our company's 20th anniversary. The injection moulding is extended by two additional injection moulding machines to a total of four machines. In addition the screw production is expanded by another multi-stage press. So we now have a total of five machines for screw production at our disposal.

## 2021

Our fleet of machinery continues to grow. Two more plastics machines will be added to our company's stock this year. We are expanding our online offering also, with the valuable Eurotec Coach and Eurotec BIM online portal.

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## INHOUSE PRODUCTION IN HAGEN

When production began in 2013, we took an important step forward in the company's history. Our success and ever-growing production facilities show that we are establishing ourselves in the market with our producs. The benefits of in-house production are obvious, as we can better implement and constantly monitor our customers' high quality requirements. Short delivery times and swift responses to the demand of the market are additional advantages.

## QUALITY MANAGEMENT

Quality forms the basis for all of Eurotec's activities. Offering our customers flawless products and services and ensuring $100 \%$ adherence to deadlines are our prime objectives.
We expect an unreserved commitment to quality from each of our employees. Training and further development of customer- and qualityoriented mindset and acting is always in the priority.
The compliance with legal and regulatory requirements in an economic framework, while promoting environmentally conscious action, is an obligation for us.
QUALITY FROM EUROPE - AND WE'RE PROUD OF IT!

## CALCULATIONS AND PLANNING

Gladly we will advise you on your construction projects.
Contact our engineering department or use the free calculation software in the service section of our website:

## www.eurotec.team

For calculations and planning in the areas of terrace construction, timber construction, concrete, façade, we are happy to assist you.

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## SCREW PRODUCTION



Since the start of production in 2013, production has expanded steadily. We now manufacture an ever-increasing part of our screw range ourselves at the Hagen site. These include a number of special construction screws, for example, including the KonstruX fully threaded screws or Topduo roofing screws.

We make cold formed parts with a diameter of up to 10 mm and a length of up to $1,000 \mathrm{~mm}$ in our production facility. We can automate up to 8 machining steps on our machines, which makes our work very cost-effective. Relocating the production facilities to a bigger hall meant that this area would also be expanded to include additional machines.


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## QUALITY ASSURANCE AND CERTIFICATIONS



Our ulimate goal is to provide our customers with flawless products and services. We also guarantee $100 \%$ adherence to delivery dates. We expect every one of our employees to commit to quality unwaveringly. Training and further development of customer- and quality-oriented ways of thinking and acting are always in focus. We feel duty-bound to comply with legal and regulatory requirements and within a given an economic framework, while at the same time promoting environmentally conscious action.

We are proud of the fact that almost all of our products in the wood, façade and concrete segments are ETA-cerifified. It goes without saying that our quality assurance does daily checks on the batches produced for standards such as conformity to drawings, functionality, appearance, and compliance with customer-specific specifications. That is the only way we can be sure to deliver the consistently high quality our customers have come to expect from us.


## Gurotec COACM



On construction site, not all processes run according to plan and sometimes there may be a lag of technical understanding, basic knowledge or the correct organisation of the workflow. With our new format Eurotec Coach we provide all the required knowledge with the help of videos, brochures and expert articles which you require to become a pro!

OUR BIM-ONLINE PORTAL - ALL DATA AT ONE SIGHT


Many people are involved in the construction of a building, such as architects, planners, craftsmen and service providers. All these people need important data and information for their work.

In our new Eurotec BIM online portal, we provide you with up-to-date BIM-relevant data for our product range.

You have full access to 3D/CAD data, DWG files, important product information, ETA certifications and much more. All functions of the portal are
available to you free of charge! The download of the files is possible after a quick registration.



CIT BASICS

CLT (Cross Laminated Timber) panels consist of several layers of wooden boards stacked crosswise typically at an angle of 90 degrees). They are glued together on their broad faces and sometimes also on the narrow faces.

A cross-section of a CLT element has at least three bonded sheet layers arranged in an alternating way and orthogonal to the adjacent layers. In special configurations, successive layers can be arranged in the same direction, creating a double layer for example, double longitudinal layers on the outer surfaces and/or additional double layers at the core of the panel) to achieve specific structural capacities.

CLT products will typically be manufactured with an odd number of layers. Gluing three to seven layers together is common. The thickness of the individual layers of wood can vary from 16 mm to 51 mm , while the width can vary from about 60 mm to 240 mm .

The panel sizes vary depending on the manufacturer. Typical widths are $0.6 \mathrm{~m}, 1.2 \mathrm{~m}, 2.4 \mathrm{~m}$, and 3 m . The length can be up to 18 m . In special cases, the thickness can be up to 500 mm . Typical thicknesses are between 60 and 300 mm , however.
(Transport regulations may limit the CLT panel sizes).
The timber in the outer layers of the CLT panels that are used as walls are aligned up and down, parallel to the gravity loads, to maximise the vertical loading capacity of the wall. Similarly, in floor and roof systems, the outer layers run parallel to the main tension direction.

## ADVANTAGES OF BUIIDING WITH CLT

- CLT allows screw connection in any direction, irrespective of the grain direction, as the layering of the boards means that no grain direction has to be observed.
- Reduced construction time due to prefabrication of the elements

Enables almost film-free construction due to the diffusion-open properties of the CLT elements.

- CLT has both sound and heat insulating properties.
- A wide range of architectural design options.
- All components of a house (walls, ceilings, and roof) can be made of CLT.
- Lower weight compared to concrete and bricks
- No construction waste when demolishing buildings. CLT is completely ecologically recyclable.



## PRODUCTION OF CLT

## 1




The boards are sorted after the soffwood boards have gone through a drying process (more than 48 hours). Growth deviations in the wood that would reduce the strength, or are simply unsightly, are marked. The sections that have such defects are cut out.

The boards of different lengths are joined together to create an almost endless strand of wooden boards, which is necessary for CLT production. This is done by means of finger joints. The resulting boards are then planed to eliminate thickness deviations between the boards.

The manufactured boards are applied manually or mechanically to form a layer. Adhesive is applied to the resulting surface after a layer has been completely applied. The most common method here is a glue curtain through which the layer is passed.

4


Another layer is placed on top of the glued layer. This is aligned so that the fibre direction of the new layer runs at an angle of $90^{\circ}$ to the fibres of the board below. Glue is then applied to the new layer also. This process is repeated until the desired number of board layers is achieved.

Once the desired number of layers is reached, the glued lamellas are pressed. The size of the press bed determines the possible panel size. As soon as the adhesive has cured, the CLT panel is reworked to remove any dirt, adhesive residues, or protruding wood. This is done by planing and grinding the CLT panel.

## BUIILING WITH CROSS LAMINATED TIMBER

The construction phases of modern timber construction methods, such as building with cross laminated fimber, are very different from that of the conventional solid construction method. Whereas with solid construction most of the work takes place on the building site, with timber construction much of the work has now shifted from the construction site to the factory.

The keyword here is prefabrication. All wall, ceiling, and roof elements are delivered to the construction site not as unprocessed CLT panels and thus raw material. They are prepared in special joinery centres for later assembly.

In the CNC joinery centres, the manufactured CLT panels are further processed into individual elements. All necessary work that is required on the construction site for fasteners of all kinds and/or for geometries that would be too difficult to realise on the construction site, is carried out here. Common joinery work carried out in the factory includes:

- Windows and door cut-outs
- Angled cuts in the gable area
- Cuts and notches
- Milling of folding systems (for example: joint deck board fold, tier fold)
- Special geometries for special connectors

Such complex processing steps, especially through the use of computer-controlled processing machines, increase the amount ofu pfront planning work. Positions for connectors and installations within the house (electrical/water) must be able to be provided with the necessary information. Furthermore, care is taken to ensure that all components are matched to each other to the millimetre in the final assembly, so that there are no problems in the final assembly.

E-Trdice
Wood connectors
Mooq couveojots

|  |  |
| :--- | :--- | :--- |

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## CLT SYSTEM INSIDE CORNER <br> DEVELOPED FOR MODERN TIMBER CONSTRUCTION

## ADVANTAGES

- Combining several CLT system inside corners, an effective connection of different elements with each other is created
- Fewer connectors required
- Versatile applications


## INSTRUCTIONS FOR USE

The CLT system inside corner can be used to connect internal corners with each other. It can be used both individually and in combination with several CLT system inside corners. A hexagon head screw can be led from one element, through the wall, to the other element, for this purpose. If this is applied in all possible directions, a stable construction for wall nodes is created. This can also be achieved with the combination of our IdeeFix. Although the individual corners are not directly connected to each other, it results in a very secure connection between the wall and ceiling or floor elements.



Versatility is very important to us. One of our new products is the CLT system inside corner. A strong connection of wall nodes is achieved when it is used in combination. The inside corner is also an unbeatable solution for timber-timber connections at corner points.

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## CLT SYSTEM INSIDE CORNER - COMBINATION

The CLT system inside corner is an extremely combinable connector. Wall nodes can be connected in a number of different ways.

A construction can be extremely strengthened by connecting several interior corners of a system through the wood. This can be achieved with our IdeeFix or also hexagonal bolts, for example. There are numerous possibilities.

In contrast to using the connector individually (see examples), the most force can be absorbed and distributed when the internal corners of the system are positioned opposite each other.


With KonstruX and IdeeFix


With KonstruX and Hexagon head screw M16


CLT SYSTEM INSIDE CORNE


HEXAGON HEAD SCREWS (ACCORDING TO MATERIAL THICKNESS|

## Common combination example



With Hexagon head screw M16 built into ceiling and walls


Partial construction from two system inside corners in combination with the IdeeFix

## Eurotec

## POSSIBLE APPLICATIONS



WALL JUNCTION - VISIBLE SOLID WOOD CEILING



CANTILEVER STRUCTURES


## Gurotec

## CLT SYSTEM ANGLE <br> developed for modern tmber construction

## ADVANTAGES

- High load bearing capacity
- Versatile applications
- Compatible with SKO4


## DESCRIPTION

The CLT system angle is ideally suited for use in solid timber construction. The scope of application is limited to the use of CLT (cross-laminated timber). The solid construction allows it to transmit major forces. In contrast to the standard angles (on the following pages), the system angle CLT can be combined with our IdeeFix. This makes it possible to construct complex connections.

## INSTRUCTIONS FOR USE

Either $5 \times 60 \mathrm{~mm}$ angle fiting screws or the Paneltwistec $5 \times 120 \mathrm{~mm}$, in combination with the KonstruX CH $10 \times 125 \mathrm{~mm}$, are used for the CLT system angle. When used with IdeeFix, only 4 IdeeFix and 4 KonstruX are needed - see application picture. It is possible to combine IdeeFix and screw bolts through a wall also. The load values, which are regulated according to ETA, must be observed. For further information, please contact our technical department technik@eurotec.team or +492331 6245-444.

| Art. no. | Name | Dimensions [mm] ${ }^{\text {a/ }}$ | Material | Material thickness [mm] | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 954180 | CII sysiem angle | $230 \times 80 \times 120$ | S250 Gavanised | 4 | 1 |




KonstruX + Angle-bracket screw $5 \times 60 \mathrm{~mm}$
KonstruX + Ideefix


KonstruX + Angle-bracket screw + IdeeFix


Connected with M16 hexagon head screws

## Eurotec

## CLT SYSTEM ANGLE - STATIC VALUES



| Load direction FI; F2/F3;/F5 |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vertical leg connection Angle-hracket screw $05 \mathrm{~mm} \mathrm{n}=43$ | 5,0x 40 | 5,0 50 | 5,0 60 | 5,0x 70 | 5,0×40 | 5,0×50 | $5,0 \times 60$ | 5,0x70 | 5,0 40 | 5,0 50 | $5,0 \times 60$ | 5,0x70 |
| Horizontal leg connection | Angle-bracket screw $5,0 \times 40$ <br> $n=43$ | Angle-bracket <br> screw 5,0 x 50 <br> n=43 | Angle-bracket <br> screw 5,0 $\times 60$ <br> n=43 | Angle-bracket <br> screw $5,0 \times 70$ <br> $n=43$ | $\text { IdeeFix } 040$ n=3 | Ideefix@ 40 <br> n=3 | Ideefix 040 <br> n=3 | Ideefix 040 <br> $\mathrm{n}=3$ | $\begin{gathered} \text { M16 } 8.8 \\ \mathrm{n}=3 \end{gathered}$ | $\begin{gathered} \text { M16 } 8.8 \\ n=3 \end{gathered}$ | $\begin{gathered} \text { M16 } 8.8 \\ n=3 \end{gathered}$ | $\begin{gathered} \text { M16 } 6.8 \\ \mathrm{n}=3 \end{gathered}$ |
|  | Konstrux $10 \times 125 \mathrm{n}=4$ |  |  |  |  |  |  |  |  |  |  |  |
|  | 55,8 | 62,4 | 69,1 | 75, 7 | 43,1 | 43,1 | 43,1 | 43,1 | 43,1 | 43,1 | 43,1 | 43,1 |
| $F_{23,12 k}[\mathrm{kN}]$ | 49,1 | 58,3 | 62,1 | 66,0 | 49,1 | 55,9 | 55,9 | 55,9 | 49,1 | 58,3 | $\begin{aligned} & 62,1 \\ & 60,5 \end{aligned}$ | $\begin{aligned} & 66,0 \\ & 60,5 \end{aligned}$ |
| F5, Rk pull $\perp$ on $\mathrm{CLI}[\mathrm{kN}]$ | 6,9 | 6,9 | 6,9 | 6,9 | 6,9 | 6,9 | 6,9 | 6,9 | 6,9 | 6,9 | 6,9 | 6,9 |


| Lood direction Fl ; F2/F3; /F5 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vertical leg connection | $\text { Ideefix } 040$ $\mathrm{n}=3$ | IdeeFix 040 $\mathrm{n}=2$ | IdeeFix 040 $\mathrm{n}=3$ | $\begin{gathered} \text { Ideefix } \emptyset 40 \\ n=2 \end{gathered}$ | Ideefix 040 $\mathrm{n}=3$ | Ideefix 040 $\mathrm{n}=2$ |
| Horizontal leg connection | $\begin{gathered} \text { Angle-bracket screw } \\ 5,0 \times 40 ; 50 ; 60 ; 70 \mathrm{n}=43 \end{gathered}$ | $\begin{gathered} \text { Angle-bracket screw } \\ 5,0 \times 40 ; 50 ; 60 ; 70 \mathrm{n}=43 \end{gathered}$ | IdeeFix 040 $n=3$ | $\text { Ideefix } 040$ $\mathrm{n}=2$ | $\begin{gathered} \text { M16 } 8.8 \\ n=3 \end{gathered}$ | $\begin{gathered} \text { M16 } 6.8 \\ \mathrm{n}=2 \end{gathered}$ |
|  | Konstru 10 x 125n=4 |  |  |  |  |  |
| $F_{1}$, Rkpull [kN] | 43,1 | 29,9 | 43,1 | 29,9 | 43,1 | 29,9 |
| $F_{23,}$, $\mathrm{lk}[\mathrm{kN}]$ | 26,0 | 22,3 | 26,0 | 22,3 | 26,0 | 22,3 |
| $F_{5}$, Rk pull $\perp$ on $\mathrm{CLT}[\mathrm{kN}]$ | 4,8 | 4,8 | 4,8 | 4,8 | 4,8 | 4,8 |


| Load direction F1; F2/F3; /F5 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vertical leg connection | $\begin{gathered} \text { M16 } 8.8 \\ \mathrm{n}=3 \end{gathered}$ | $\begin{gathered} \text { M16 } 8.8 \\ n=2 \end{gathered}$ | $\begin{gathered} \text { M16 } 8.8 \\ n=3 \end{gathered}$ | $\begin{gathered} \text { M16 } 8.8 \\ n=2 \end{gathered}$ | $\begin{gathered} \text { M16 } 8.8 \\ n=3 \end{gathered}$ | $\begin{gathered} \text { M16 } 6.8 \\ \mathrm{n}=2 \end{gathered}$ |
| Horizontal leg connection | $\begin{gathered} \text { Angle-bracket screw } \\ 5,0 \times 40 ; 50 ; 60 ; 70 n=43 \end{gathered}$ | Angle-bracket screw $5,0 \times 40 ; 50 ; 60 ; 70 n=43$ | Ideefix 040 <br> $\mathrm{n}=3$ | IdeeFix $\varnothing 40$ <br> $\mathrm{n}=2$ | $\begin{gathered} \text { M16 } 8.8 \\ n=3 \end{gathered}$ | $\begin{gathered} \text { M16 } 6.8 \\ \mathrm{n}=2 \end{gathered}$ |
|  | Konstrux 10x $125 \mathrm{n}=4$ |  |  |  |  |  |
| $F_{1, ~ \text { Rk pull [kN] }}$ | 43,1 | 43,1 | 43,1 | 29,9 | 43,1 | $\begin{gathered} 43,1 \\ 36,7 \end{gathered}$ |
| F23, $\mathrm{Rk}[\mathrm{kN}]$ | $\begin{gathered} 34,4 \\ 29,3 \end{gathered}$ | $\begin{aligned} & 29,6 \\ & 25,2 \end{aligned}$ | $\begin{gathered} 34,4 \\ 29,3 \end{gathered}$ | $\begin{aligned} & 29,6 \\ & 25,2 \end{aligned}$ | $\begin{aligned} & 34,4 \\ & 29,3 \end{aligned}$ | $\begin{aligned} & 29,6 \\ & 25,2 \end{aligned}$ |
| F5, Rk pull $\perp$ on [LIT[kN] | 4,8 | 4,8 | 4,8 | 4,8 | 4,8 | 4,8 |

$F 4$, $\mathrm{Rk}=54 \mathrm{kN}$ pressure $\perp$ on CLT ; independent of connections.
For connections with M18 8.8 if bolt head or nut is not located on CLI: Washer with $d_{0}=40 \mathrm{~mm}$.
$\rho \mathrm{k}=350 \mathrm{~kg} / \mathrm{m}^{3}$ conservative for some approved cross-laminated timber, increase of load-bearing capacities according to ETA-19/0020 with kdens $=\left(\frac{\rho_{\mathrm{k}}}{350 \mathrm{~kg} / \mathrm{m}^{3}}\right)$ possible.
The construction of the supporting structure should prevent the twisting of the cross laminated timber components.
In case of connection with CLI system angles on both sides, the values of this table may be applied for each of the two angles. The values for F23, Rk only change for the connection with M16 screws.
In other words, the values in italics must be used if CIT system brackets are fitted to the top and bottom of the ceiling.

Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by authorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.


## Gurotec

## SHEARING ANGLE

CONNECTOR DEVELOPED FOR MODERN TMBER CONSTRUCTION TO ABSORB SHEAR FORCES

## ADVANTAGES

- Many different fields of application
- For installation in timber-concrete, as well as timber-timber connections
- Very high shear load-bearing capacity
- Fewer connectors required

In combination with the pressure plate, the following tensile forces can be absorbed when fixing in concrete.

## DESCRIPTION

The shearing angle is an angle bracket for absorbing shearing forces. This product was specifically developed for modern timber construction. Thanks to various holes for anchoring in timber and concrete, our shearing angle can be used in timber frame as well as solid timber construction.


| Art. no. | Name | Dimensions [mm] | Material | Material thickness [mm] | PU |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 954112 | Schervinkel | $230 \times 120$ | 5250 Galvanised | 3 | 1 |



Shearing angle for fixing a wall to the concrete foundation.

| Shearing angle pressure plate | Art. no. | Dimensions $[\mathrm{mm}]$ | Material | Material thickness $[\mathrm{mm}]$ | PU |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | 954111 | $230 \times 70$ | 5235 Gavanised | 12 | 1 |



## SHEARING ANGLE - STATIC FULL UTILISATION VALUES



| Load direction F2/F3 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Connection Timber-Iimber |  |  |  |  |  |  |
| Verical leg cornection | Anchor nails $84 \times 40 \mathrm{n}=41$ | Anchor nails $9 \times 50 \mathrm{n}=41$ | Anchor nails $84 \times 60 \mathrm{n}=41$ | Angle-hrocket screw $05 \times 40 \mathrm{n}=41$ | Anglebracketescrew $05 \times 50 \mathrm{n}=41$ | Angle-hrackestrew $05 \times 60 \mathrm{n}=41$ |
|  | Panelwisisec CH $05 \times 120 \mathrm{n}=6$ |  |  |  |  |  |
| Horizontal leg comnection | Anchor nails $04 \times 40 \mathrm{n}=41$ | Anchor nails $4 \times 50 \mathrm{n}=41$ | Anchor nails $84 \times 60 \mathrm{n}=41$ | Angle-hracket screw $05 \times 40 \mathrm{n}=41$ | Angle-bracketescrew $05 \times 50 \mathrm{n}=41$ | Angle-hrackestrew $05 \times 60 \mathrm{n}=41$ |
|  | Panelwisistec $\mathrm{CH} 05 \times 120 \mathrm{n}=6$ |  |  |  |  |  |
| Char. Sheer carrying capacity [kN] | 30,5 | 36 | 37,2 | 41,9 | 44,6 | 47,6 |
| Char. Sheer carrying capacity [KN] (Use of Sonote SK04) | 22,6 | 26,6 | 27,5 | 32,7 | 34,8 | 37,1 |

 The minimum distanes between the comnetors and the edges according to EC 5 must be complied with.

| Lood direction F2/F3 |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Connection Timber-Concrete |  |  |  |  |  |  |  |  |  |  |  |  |
| Vericial leg comection | Anchor nails $04 \times 40 n=41$ | Anchor noils $04 \times 40 n=41$ | Anchor nails $04 \times 50 n=41$ | Anchor nails $04 \times 50 \mathrm{n}=41$ | Anchor nails <br> $04 \times 60 n=41$ | Anchor nails <br> $04 \times 60 n=41$ | $\begin{gathered} \text { ABS } \\ 05 \times 40 n=41 \end{gathered}$ | $\begin{gathered} \text { ABS } \\ 05 \times 40 \mathrm{n}=41 \end{gathered}$ | $\begin{gathered} \text { ABS } \\ 05 \times 50 \mathrm{n}=41 \end{gathered}$ | $\begin{gathered} \text { ABS } \\ 05 \times 50 \mathrm{n}=41 \end{gathered}$ | $\begin{gathered} \text { ABS } \\ 05 \times 60 \mathrm{n}=41 \end{gathered}$ | $\begin{gathered} \text { ABS } \\ 05 \times 60 \mathrm{n}=41 \end{gathered}$ |
| Paneltwistec CH $05 \times 120 \mathrm{n}=6$ |  |  |  |  |  |  |  |  |  |  |  |  |
| Horizontal leg comection 0 | Rock concretes screw $012,5 \times 120 \mathrm{n}=2$ | Bolt anchor $012 \times 110 \mathrm{n}=2$ | Rock concrete screw $012,5 \times 120 \mathrm{n}=2$ | Bolit anchor $012 \times 110 n=2$ | Rock concretes screw $012,5 \times 120 \mathrm{n}=2$ | Bolt anchor $012 \times 110 n=2$ | Rock concrete screw $012,5 \times 120 \mathrm{n}=2$ | $\begin{gathered} \text { Boltanchor } \\ 012 \times 110 n=2 \end{gathered}$ | Rock concretes screw $012,5 \times 120 \mathrm{n}=2$ | Bolt anchor $012 \times 110 n=2$ | Rock concrete screw $012,5 \times 120 \mathrm{n}=2$ | $\begin{gathered} \text { Bolt anchor } \\ 012 \times 110 \mathrm{n}=2 \end{gathered}$ |
| ind. pressure plate $230 \times 70$ |  |  |  |  |  |  |  |  |  |  |  |  |
| Char.-shearing capacity <br> [kN] | 30,5 | 23,4 | 36,0 | 23,4 | 37,2 | 23,4 | 41,9 | 23,4 | 44,6 | 23,4 | 47,6 | 23,4 |

The lood-bearing capacities were determined based on ETA-19/0020 Characterisici lood-bearing capacity in kN , wood strength lass $350 \mathrm{~kg} / \mathrm{m}^{3}$ char. Gross density. The minimum distances between the connectors and the edges according to EC 5 must be complied with.

Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by authorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

## Eurotec

## PARTIAL UTLISATION 1



| Lood direction F2/F3 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cometion Timber-Iimber |  |  |  |  |  |  |
| Vericicl leg connection | Anthor nils $04 \times 40 \mathrm{n}=34$ | Anctor nilis $84 \times 50 \mathrm{n}=34$ | Anchor nails $04 \times 60 n=34$ Paneltwistec CH | $\begin{aligned} & \text { ABS } 85 \times 40 \mathrm{n}=34 \\ & \times 120 \mathrm{n}=6 \end{aligned}$ | ABS $05 \times 50 \mathrm{n}=34$ | AB5 $55560 \mathrm{n}=34$ |
| Horiontidl leg comection | Anctor noils $04 \times 40 \mathrm{n}=34$ | Anctor nils $84 \times 50 \mathrm{n}=34$ | Anchor nails $84 \times 60 \mathrm{n}=34$ Paneltwisec CH | $\begin{aligned} & \text { ABS } 05 \times 40 n=34 \\ & \times 120 n=6 \end{aligned}$ | ABS $05 \times 50 \mathrm{n}=34$ | ABS $05 \times 60 \mathrm{n}=34$ |
| Chor:shearing capaity [KN] | 23,9 | 28,1 | 29,1 | 32,7 | 34,9 | 37,2 |
| Char: shearing capaity [kV] (use Sonoter SK04) | 17,1 | 20,8 | 21,5 | 25,5 | 27,2 | 29 |


| Load direction F2/F3 |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Comection Timber-Onrcete |  |  |  |  |  |  |  |  |  |  |  |  |
| Vericial leg connection | Anchor nails $04 \times 40$ $n=34$ | Anchor noils $04 \times 40$ n=34 | Anchor nails $04 \times 50$ $n=34$ | Anchor nails $04 \times 50$ n=34 | Anchor nails $04 \times 60$ $n=34$ | Anchor nails $04 \times 60$ $n=34$ | $\begin{gathered} \text { ABS } \\ 05 \times 40 \\ n=34 \end{gathered}$ | $\begin{gathered} \text { ABS } \\ 05 \times 40 \\ n=34 \end{gathered}$ | $\begin{gathered} \text { ABS } \\ 05550 \\ n=34 \end{gathered}$ | $\begin{gathered} \text { ABS } \\ 05 \times 50 \\ n=34 \end{gathered}$ | $\begin{gathered} \text { ABS } \\ 95 \times 60 \\ n=34 \end{gathered}$ | $\begin{gathered} \text { ABS } \\ 05 \times 60 \\ n=34 \end{gathered}$ |
| Pandtwistec CH $05 \times 120 \mathrm{n}=6$ |  |  |  |  |  |  |  |  |  |  |  |  |
| Horizontiol leg comnection | $\begin{aligned} & \text { Rock concrefe } \\ & \text { screw } \\ & 012,5 \times 120 \\ & n=2 \end{aligned}$ | Bolt anchor <br> $012 \times 110$ <br> $\mathrm{n}=2$ | $\begin{gathered} \text { Rock oncrete } \\ \text { screw } \\ 012,5 \times 120 \\ n=2 \end{gathered}$ | Bot anchor <br> $012 \times 110$ <br> $\mathrm{n}=2$ | $\begin{aligned} & \text { Rodk concrefie } \\ & \text { screve } \\ & 012,5 \times 120 \\ & n=2 \end{aligned}$ | Bolt anchor <br> $012 \times 110$ <br> $\mathrm{n}=2$ | $\begin{aligned} & \text { Rock concrefe } \\ & \text { screw } \\ & 012,5 \times 120 \\ & n=2 \end{aligned}$ | $\begin{aligned} & \text { Bolt anchor } \\ & 012 \times 110 \\ & n=2 \end{aligned}$ | $\begin{gathered} \text { Rock concrete } \\ \text { screw } \\ 012,5 \times 120 \\ n=2 \end{gathered}$ | Bolt anchor <br> $012 \times 110$ <br> $\mathrm{n}=2$ | $\begin{gathered} \text { Rock concrefe } \\ \text { scew } \\ 012,5 \times 120 \\ n=2 \end{gathered}$ | $\begin{aligned} & \text { Bolt anthor } \\ & 012 \times 110 \\ & n=2 \end{aligned}$ |
| ind. pressure plate $330 \times 70$ |  |  |  |  |  |  |  |  |  |  |  |  |
| Char:shearing crpacity [kN] | 23,9 | 23,4 | 28,1 | 23,4 | 29,1 | 23,4 | 32, | 23,4 | 34,9 | 23,4 | 37,2 | 23,4 |

The load.bearing capacities were defermined bosed on EA-19/0020 Characterisisic load-bearing capacity in KN , wood strenght loss $350 \mathrm{~kg} / \mathrm{m}^{3}$ char. GToss density.
The minimum distances bewven the comnectors and the edges according to EC 5 must be complied with.
 As per LBuO, plesse contuct a qualified strutural engineer for a poid proof of stability. We will be happy to efere yo to someone.


## Note

All values given refer to the drilling pattern shown. We recommend using this as it has a considerably higher shear carrying capacity compared to the rear holes

## PARTIAL UTILISATION 2



| Lood direction F2/F3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Connection Timber-Timber |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Vertical leg connection |  |  | Anchor noils $04 \times 40 \mathrm{n}=29$ |  | Anchor nails $04 \times 50 \mathrm{n}=29$ |  | 9 Anchor nails $04 \times 60 \mathrm{n}=29$ |  | Angle-bracket screw$05 \times 40 n=29$ |  |  | Angle-bracket screw $05 \times 50 n=29$ | Angle-bracket screw$05 \times 60 n=29$ |  |
|  |  |  | Paneltwistec CH05 $\times 120 \mathrm{n}=4$ |  |  |  |  |  |  |  |  |  |  |  |
| Horizontal leg connection |  |  | Anchor nails $04 \times 40 \mathrm{n}=29$ |  | Anchor nails $84 \times 50 \mathrm{n}=29$ |  | 29 Anchor nails $04 \times 60 \mathrm{n}=29$ |  | Angle-bracket screw $05 \times 40 n=29$ |  |  | Angle-bracket screw $05 \times 50 n=29$ | Angle-bracket screw$05 \times 60 n=29$ |  |
|  |  |  | Panethwistec CH05 $\times 120 \mathrm{n}=4$ |  |  |  |  |  |  |  |  |  |  |  |
| Char. Shear carrying capacity [KN] |  |  | 19,3 |  |  | 22,8 | 23,6 |  | 26,5 |  |  | 28,3 | 30,1 |  |
| Char. Shear carrying capacity [KN] (USe of Sonotec SK04) |  |  | 14,3 |  |  | 16,9 |  | 17,5 | 20,1 |  |  | 22,1 | 23,5 |  |
| Lood direction F2/F3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Connection Timber-Concrete |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Vertical leg connection | Anchor noils $04 \times 40 n=29$ | $\begin{gathered} \text { Anchor nails } \\ 04 \times 40 n=29 \end{gathered}$ | Anchor nails $04 \times 50 n=29$ | $\begin{gathered} \text { Anchor nails } \\ 04 \times 50 \mathrm{n}=29 \end{gathered}$ |  | Anchor nails $04 \times 60 n=29$ | Anchor nails $04 \times 60 n=29$ | Angle-bracket <br> screw $05 \times 40$ <br> $\mathrm{n}=29$ | Angle-bracket screw $05 \times 40$ n=29 | Angle-bracket <br> screw $05 \times 50$ <br> $\mathrm{n}=29$ |  | Angle-bracket <br> screw $05 \times 50$ <br> $\mathrm{n}=29$ | Angle-bracket <br> screw $05 \times 60$ <br> $\mathrm{n}=29$ | Angle-bracket <br> screw $05 \times 60$ <br> $\mathrm{n}=29$ |
|  | Paneltwistec CH0 $5 \times 120 \mathrm{n}=4$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Horizontal leg connection | Rock concrete screws $012,5 \times 120 \mathrm{n}=2$ | $\begin{aligned} & \text { Bolt anchor } \\ & 012 \times 110 \mathrm{n}=2 \end{aligned}$ | Rock concrete screws $012,5 \times 120 \mathrm{n}=2$ | $\begin{gathered} \text { Bolt anchor } \\ 012 \times 110 \mathrm{n}=2 \end{gathered}$ |  |  | Bolt anchor $012 \times 110 n=2$ |  | $\begin{aligned} & \text { Bolt anchor } \\ & 012 \times 110 n=2 \end{aligned}$ | Rock concrete screws $012,5 \times 120 \mathrm{n}=2$ |  | $\begin{gathered} \text { Bolt anchor } \\ 012 \times 110 \mathrm{n}=2 \end{gathered}$ | Rock concrete screws $012,5 \times 120 \mathrm{n}=2$ | $\begin{gathered} \text { Bolt anchor } \\ 012 \times 110 \mathrm{n}=2 \end{gathered}$ |
|  | ind. pressure plate $230 \times 70$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Char-Schertragfitiothkeit [kN] | 19,3 | 19,3 | 22,8 | 22, |  | 23,6 | 23,4 | 26,5 | 23,4 |  | 28,3 | 23,4 | 30,1 | 23,4 |

The load-bearing capacities were determined based on ETA-19/0020 Characteristic load-bearing capacity in kN , wood strength class $350 \mathrm{~kg} / \mathrm{m}^{3}$ char. Gross density.
The minimum distances between the connectors and the edges according to EC 5 must be complied with.
Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by authorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

## Gurotec

## HB FLAT SHEARING ANGLE

## CONNECTOR DEVELOPED FOR MODERN TIMBER CONSTRUCTION TO ABSORB SHEAR FORCES

## ADVANTAGES

- For assembly on concrete
- Very high shear load-bearing capacity
- Fewer connectors required
- In combination with the pressure plate, the following tensile forces can be absorbed when fixing in concrete.


## DESCRIPTION

The HB flat shearing angle (wood-concrete) is a bracket connector for absorbing shearing forces that was specifically developed for modern timber construction. Its low height means it is ideally suited to use in timber frame construction. The pressure plate allows the occurring loads to be optimally conducted into the concrete.


| Art. no. | Name | Dimensions [mm] ${ }^{\text {a/ }}$ | Material | Material thickness [mm] | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 954087 | HB lat shearing ongle | $230 \times 100 \times 70$ | S250 Gavanised | 3 | I |
| 954111 | Pressure plate Shearing angle | $230 \times 68$ | S235 Gavanised | 12 | 1 |

a) Length x Width x Height


HB flat shearing angle with pressure plate for fixing a wall to the concrete foundation.


| Lood direction F2/F3; F4 |  |  |
| :---: | :---: | :---: |
| Comection Timber-Concrete |  |  |
| Vericial leg connection | $\begin{aligned} & \text { Angle-fracketescrew } 05 \times 25 n=3 \\ & \text { Panelwisisec CH } 45 \times 120 n=12 \end{aligned}$ |  |
| Horizontiol leg comnection | Rock concrete screws $012,5 \times 120 \mathrm{n}=2$ | Boltanchor $912 \times 110 \mathrm{n}=2$ |
|  | ind. pressure plat $230 \times 68 \times 12$ |  |
| Char. Sherr carrying capacity $\mathrm{F}_{23}[\mathrm{KN}]$ | 40,0 | 23,9 |
| Char. bearing capacity $\mathrm{F}_{4}[\mathrm{KN}]$ | 40,0 | 40,0 |



Please note: Verify the assumpions made. The stated values, and type and number of joining devices are based on preiminary measurements. Projects are to be dimensioned excusively by authorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.


## Note

All values given refer to the drilling pattern shown. We recommend using this as it has a considerably higher shear carrying capacity compared to the rear holes.


HB flat shearing angle with Paneltwistec CH

## Gurotec

## HH FLAT SHEARING ANGLE

CONNECTOR DEVELOPED FOR MODERN TIMBER CONSTRUCTION TO ABSORB SHEAR FORCES

ADVANTAGES

- For assembly on timber
- Very high shear load-bearing capacity
- Fewer connectors required
- Especially high tensile forces can be absorbed in combination with the KonstruX


## DESCRIPTION

The HH flat shearing angle (wood-wood) is a bracket connector for absorbing shearing forces that was specifically developed for modern timber construction. Its low height means it is ideally suited to use in timber frame construction.

$\left.\begin{array}{l|l|l|l|c|}\hline \text { Art. no. } & \text { Name } & \text { Dimensions }[\mathrm{mm}]^{0]} & \text { Material } & \text { Material thickness }[\mathrm{mm}]\end{array}\right]$ PU
a) Length $x$ Width


HH flat shearing angle for fixing a wall to the wooden floor of the upper level.

| Lood direction F2/F3; F4 |  |
| :---: | :---: |
| Connection Wood-Wood |  |
| Vericall leg connection | $\begin{gathered} \text { ABS } 05 \times 25 n=3 \\ \text { Peneltwistec CH } 05 \times 120 n=12 \end{gathered}$ |
| Horizonitiol leg comnection | $\begin{gathered} \text { ABS } \varnothing 5 \times 25 \mathrm{n}=3 \\ \text { Paneltwistec CH } 05 \times 120 \mathrm{n}=12 \end{gathered}$ |
| Char:shearing capacity $\mathrm{F}_{23}[\mathrm{KN}]$ | 40,0 |
| Char:Shearing capacity $\mathrm{F}_{23}[\mathrm{KNJ}$ ( (sse Sonotes SYO4) | 36,0 |
| Chor:- lood.bearing capacity $\mathrm{F}_{4}[\mathbf{k}]$ | 40,0 |
| Char: Oood.bearing capacity $\mathrm{F}_{4}[\mathrm{KNV}$ (use Sonoer SKO4) | 36,0 |



Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary meassurements. Projects are to be dimensioned exclusively by authorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.


HH flat shearing angle with Paneltwistec CH

## Eurotec

## SHEARING PLATE

CONNECTOR DEVELOPED FOR MODERN TIMBER CONSTRUCTION TO ABSORB SHEAR FORCES

## ADVANTAGES

- Very high shear load-bearing capacity
- Many different fields of application
- For installation in wood-concrete, and wood-wood connections

Fewer connectors required

## INSTRUCTIONS FOR USE

6 slanted screw connection holes and 41 holes each side, which are optionally intended for angle-bracket screws (ABSs) or anchor nails, are provided for anchoring in wood. Depending on the application, we have provided two additional partial utilisations of the fixing holes which are also available as static-type calculations. Anchoring in concrete is carried out using the holes $(\varnothing 14 \mathrm{~mm})$ provided for this purpose with our Rock concrete screw $\varnothing$ 12,5 mm or bolt anchors $\varnothing 12 \mathrm{~mm}$.


| Art. no. | Name | Dimensions $[\mathrm{mm}]$ | Material | Material thickness $[\mathrm{mm}]$ | PU |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 954113 | Shearing plate | $230 \times 240$ | S250 Gavanised | 3 | 1 |



## SHEARING PLATE - STATIC FULL UTILISATION VALUES



| Lood direction F2/3 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Timber-Timber | Fixing in the sole plate and solid timber ceiling |  |  |  |  |  |  | Steel |
|  | Joining devices |  |  |  |  |  |  |  |
|  | Anchor noils |  |  | Angle-bracket screw |  |  | Paneltwistec 대 | 5250 |
| Dimensions [mm] | $4 \times 40$ | $4 \times 50$ | $4 \times 60$ | $5 \times 40$ | $5 \times 50$ | $5 \times 60$ | $5 \times 120$ |  |
| Quantity ( n ) |  | 41 |  |  | 41 |  | 6 |  |
| Char. shearing capacity [KN] | 30,5 | 36 | 37,2 | 41,9 | 44,6 | 47,6 | . | 156 |


|  |  |  |  | Load |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Timber-Concrete | Fixing in the sole plate |  |  |  |  |  |  | Fixing in the con | crete ceiling | Steel |
|  | Joining devices |  |  |  |  |  |  |  |  |  |
|  | Anchor nails |  |  | Angle-hracket screw |  |  | Paneltwistec (H | Rock concrete screws | Bolt anchor | 5250 |
| Dimensions [mm] | $4 \times 40$ | 4×50 | $4 \times 60$ | $5 \times 40$ | $5 \times 50$ | $5 \times 60$ | $5 \times 120$ | 012,5 | 012 |  |
| Quantity (n) |  | 41 |  |  | 41 |  | 6 | 2 | 2 |  |
| Char. Shearing capacity [kN] | 30,5 | 36 | 37,2 | 41,9 | 44,6 | 47,6 | - | 21,8 | 12,2 | 156 |

The lood-bearing capacities were determined on the basis of ETA-19/0020. Characterisici lood-bearing capacity in kN , wood strength class $350 \mathrm{~kg} / \mathrm{m}^{3}$ char. gross density.
The minimum edge distances for joining devices according to EC 5 must be observed.
Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned extusively by authorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

| Anchor nails | CE | Art. no. | Dimensions | Material | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| With flat head | (1) | 20024 | 4,0 40 | Galvanised | 250 |
|  |  | 20024 | 4,0×50 | Galvanised | 250 |
|  |  | 20022 | $4,0 \times 60$ | Galvanised | 250 |

## Suitable for use wih:

Shearing angle (p. 28), Shearing plate (p. 36)
Shearing angle HB flat (p. 32)
Shrearing angle HH flat (p. 34)
Tension strap $\mathrm{HB} / \mathrm{HH}(\mathrm{p} .40,42)$

## Eurotec

## PARTIAL UTLISATION 1



|  |  |  | direction |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Timber-Timber | Fixing in the sole plate and solid dimber ceiling |  |  |  |  |  |  | Steel |
|  | Joining devices |  |  |  |  |  |  |  |
|  | Anchor nails |  |  | Angle-rracket screw |  |  | Paneltwistec <br> CH | 5250 |
| Dimensions [mm] | $4 \times 40$ | $4 \times 50$ | $4 \times 60$ | $5 \times 40$ | $5 \times 50$ | $5 \times 60$ | $5 \times 120$ |  |
| Quantity ( $n$ ) |  | 34 |  |  | 34 |  | 6 |  |
| Char. Shearing capacity [kN] | 23,9 | 28,1 | 29,1 | 32,7 | 34,9 | 37,2 | - | 156 |


|  |  |  |  | Loodd | F2/3 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Timber-Concrete | Fixing in the sole plate |  |  |  |  |  |  | Fixing in the concrete ceiling |  | Steel |
|  | Joining devices |  |  |  |  |  |  |  |  |  |
|  | Anchor nails |  |  | Angle-bracket screw |  |  | Paneltwistec CH | Rock-concrete screws | Bolt anchor | 5250 |
| Dimensions [mm] | $4 \times 40$ | $4 \times 50$ | $4 \times 60$ | $5 \times 40$ | $5 \times 50$ | $5 \times 60$ | $5 \times 120$ | 012,5 | 012 |  |
| Quantity (n) |  | 34 |  |  | 34 |  | 6 | 2 | 2 |  |
| Char. shearing capacity [KN] | 23,9 | 28,1 | 29,1 | 32,7 | 34,9 | 37,2 | - | 20,5 | 11,6 | 156 |

The lood-bearing capacities were determined on the basis of ETA-19/0020. Characterisicic load-bearing capacity in kN , wood strength class $350 \mathrm{~kg} / \mathrm{m}^{3}$ char. gross density. The minimum edge distances for joining devices according to E( 5 must be observed.

## PARTIAL UTILISATION 2



| Looddirection F2/3 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Timber-Timber | Fixing in the sole plate and solid dimber ceiling |  |  |  |  |  |  | Steel |
|  | Joining devices |  |  |  |  |  |  |  |
|  | Anchor nails |  |  | Angle-rracket screw |  |  | Paneltwistec CH | 5250 |
| Dimensions [mm] | $4 \times 40$ | $4 \times 50$ | $4 \times 60$ | $5 \times 40$ | $5 \times 50$ | $5 \times 60$ | $5 \times 120$ |  |
| Quantity ( n ) |  | 29 |  |  | 29 |  | 4 |  |
| Char. shearing capacity [kN] | 19,3 | 22,8 | 23,6 | 26,5 | 28,3 | 30,1 |  | 156 |


| Load direction F2/3 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Timber-Concrete | Fixing in the sole plate |  |  |  |  |  |  | Fixing in the concrete ceiling |  | Steel |
|  | Joining devices |  |  |  |  |  |  |  |  |  |
|  | Anchor nails |  |  | Angle-bracket screw |  |  | Paneltwistec CH | Rockconcrete screws | Bolt anchor | 5250 |
| Dimensions [mm) | $4 \times 40$ | $4 \times 50$ | $4 \times 60$ | $5 \times 40$ | $5 \times 50$ | $5 \times 60$ | $5 \times 120$ | 012,5 | 012 |  |
| Quantity (n) |  | 29 |  |  | 9 |  | 4 | 2 | 2 |  |
| Char. shearing capacity [kN] | 19,3 | 22,8 | 23,6 | 26,5 | 28,3 | 30,1 | - | 14,4 | 11,2 | 156 |

The lood-bearing capacities were determined on the basis of ETA-19/0020. Characteristic lood-bearing capacity in kN , wood strength class $350 \mathrm{~kg} / \mathrm{m}^{3}$ char. gross density.
The minimum edge distances for joining devices according to EC 5 must be observed.
Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by authorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

## Gurotec

## TENSION STRAP HB60 / HB70

## CONNECTOR DEVELOPED FOR MODERN TMBER CONSTRUCTION TO ABSORB

## TENSILE- AND SHEAR FORCES.

## ADVANTAGES

- Very high shear load-bearing capacity
- Many different fields of application
- For installation in wood and concrete
- Fewer connectors required
- Can be used with or without a sill plate


## INSTRUCTIONS FOR USE

Anchoring in wood is carried out using $5 \times 120 \mathrm{~mm}$ countersunk-head screws at an angle of $45^{\circ}$. Thanks to the holes specially provided for this purpose, which also serve as screw guides, a non-positive connection is created between the screw head and the tension strap. The anchoring in the concrete is achieved through the holes provided ( $\varnothing 14 \mathrm{~mm}$ ) with our Rock concrete screw or Bolt anchor. The minimum distance of the concrete connector to the top edge of the foundation is 65 mm . Tension straps $\mathrm{HH} 7 \mathrm{O}(\mathrm{p} .42)$ and HB70 have two Ø 5 mm holes for $90^{\circ}$ screw connection.


Suitable for use with:
Paneliwistec CH (p. 110), Bolt anchor (p. 168)
Anchor nails (p. 37), Rock concrete screw (p. 76)
Angle-bracket screw (p. 108)

| Art. no. | Name | Dimensions [mm] | Material | Material thickness [mm] | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 954095 | Tension strap HB6O | $506 \times 60$ | S250 Gavanised | 3 | 1 |
| 954097 | Tension strap HB7O | $506 \times 70$ | S250 Gavanised | 3 | 1 |



## TENSION STRAP HB60 - STATIC VALUES



| Lood direction Fl |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Connection Timber-Concrete |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Wood side connection | Paneltwistec CH $05 \times 120 \mathrm{n}=9$ |  |  |  | Anchor nails $04 \times 40 \mathrm{n}=6$ |  |  |  | Anchor nails $04 \times 50 \mathrm{n}=6$ |  |  |  | Anchor nails $04 \times 60 \mathrm{n}=6$ |  |
| Concrete side connection | Rock concrete screws $012,5 \times 120$ $\mathrm{n}=1$ | Rock concrete screws $012,5 \times 120$ $\mathrm{n}=2$ | $\begin{aligned} & \text { Bolt anchor } \\ & 012 \times 110 \\ & n=1 \end{aligned}$ | $\begin{gathered} \text { Bolt anchor } \\ 012 \times 110 \\ n=2 \end{gathered}$ | Rock concrete screws $012,5 \times 120$ $\mathrm{n}=1$ | Rock concrete screws $012,5 \times 120$ $\mathrm{n}=2$ | $\begin{gathered} \text { Bolt anchor } \\ 012 \times 110 \\ n=1 \end{gathered}$ | Bolt anchor $012 \times 110$ $n=2$ | Rock concrete screws $012,5 \times 120$ | Rock concrete screws $012,5 \times 120$ $\mathrm{n}=2$ | $\begin{aligned} & \text { Bolt anchor } \\ & 012 \times 110 \\ & n=1 \end{aligned}$ | $\begin{gathered} \text { Bolt anchor } \\ 012 \times 110 \\ n=2 \end{gathered}$ | Rock concrete screws $\underset{\substack{0 \\ n=1 \\ n=1}}{ }$ | Rock concrete screws $012,5 \times 120$ $\mathrm{n}=2$ |
| Char. Shear carrying capacity [kN] | 20,8* | 20, ${ }^{\text {* }}$ | 12,6 | 20,8* | 9,3 | 9,3 | 9,3 | 9,3 | 11,0 | 11,0 | 11,0 | 11,0 | 11,4 | 11,4 |


| Lood direction Fl |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Connection Timber-Concrete |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Wood side connection | Anchor nails $04 \times 60 \mathrm{n}=6$ |  | Angle-hracket screw $05 \times 40 n=6$ |  |  |  | Angle-bracket screw $05 \times 50 \mathrm{n}=6$ |  |  |  | Angle-hracket screw $05 \times 60 \mathrm{n}=6$ |  |  |  |
| Concrete side connection | $\begin{gathered} \text { Bolt anchor } \\ 012 \times 110 \\ n=1 \end{gathered}$ | $\begin{gathered} \text { Bolt anchor } \\ 012 \times 110 \\ n=2 \end{gathered}$ | Rock concrete screws $012,5 \times 120$ $\mathrm{n}=1$ | Rock concrete screws $012,5 \times 120$ $\mathrm{n}=2$ | $\begin{gathered} \text { Bolt anchor } \\ 012 \times 110 \\ n=1 \end{gathered}$ | $\begin{gathered} \text { Bolt anchor } \\ 012 \times 110 \\ n=2 \end{gathered}$ | Rock concrete screws $\substack{012,5 \times 120 \\ n=1}$ | Rock concrete screws $012,5 \times 120$ | $\begin{gathered} \text { Bolt anchor } \\ 012 \times 110 \\ n=1 \end{gathered}$ | $\begin{gathered} \text { Bolt anchor } \\ 012 \times 110 \\ n=2 \end{gathered}$ | Rock concrete screws $012,5 \times 120$ $\mathrm{n}=1$ | Rock concrete screws $012,5 \times 120$ $\mathrm{n}=2$ | $\begin{gathered} \text { Bolt anchor } \\ 012 \times 110 \\ n=1 \end{gathered}$ | $\begin{gathered} \text { Bolt anchor } \\ 012 \times 110 \\ n=2 \end{gathered}$ |
| Char. Shear carrying capacity [kN] | 11,4 | 11,4 | 10,9 | 10,9 | 10,9 | 10,9 | 12,0 | 12,0 | 12,0 | 12,0 | 13,1 | 13,1 | 12,6 | 13,1 |

* Concrete edge breakout for cracked concrete

The load-bearing capacities were determined based on EAA-19/0020 Characterisic load-bearing capacity in kN , wood strenght class $350 \mathrm{~kg} / \mathrm{m}^{3}$ char. Gross density.
The minimum distances between the connectors and the edges according to EC 5 must be complied with.
Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by cuthorised persons in accordance with the State Building Code.
As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

TENSION STRAP HB70 - STATIC VALUES


The lood-bearing capacities were determined based on ETA-19/0020 Characterisic load-bearing capacity in kN , wood strength dass $350 \mathrm{~kg} / \mathrm{m}^{3}$ char. Gross density.
The minimum distances between the connectors and the edges according to EC5 must be complied with.
Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by authorised persons in accordance with the State Building Code.
As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

## Gurotec

## TENSION STRAP HH60/HH70

## FOR ABSORBING TENSIIE FORCES AND TENSILE AND SHEARING FORCES DEVELOPED FOR

## MODERN TIMBER CONSTRUCTION

## ADVANTAGES

- Many different fields of application
- For installation in wood and concrete
- Very high shear load-bearing capacity thanks to a new fixing concept
- Fewer connectors required
- Thanks to its angled hole pattern, the tension strap can also absorb shear forces.

Inter-storey connector

## INSTRUCTIONS FOR USE

The Tension strap HH 60 with its width of 60 mm is perfect for conventional timber frame construction, whereas the Tension strap HH70 with a width of 70 mm and its angled screw pattern was specially developed for solid wood construction. Anchoring in wood is carried out using $5 \times 120 \mathrm{~mm}$ countersunk-head screws at an angle of $45^{\circ}$. A forcefit connection is created between the screw head and the tension strap, thanks to the holes specially provided for this purpose, which also serve as screw guides. The Tension strap HH7O has two additional holes $\varnothing 5 \mathrm{~mm}$ which are intended for $90^{\circ}$ screw connection.


Suitroble for use with: Paneltwistec $\mathrm{CH}(\mathrm{p} .110)$ Angle-bracket screw (p. 108), Anchor noils (p. 37)

| Properties | HH60 | HH70 |
| :--- | :---: | :---: |
| Min. Wall/frame width: | 60 mm | 120 mm |
| Max. Ceiling thickness: | 240 mm | 260 mm |


| Art. no. | Name | Dimensions [mm] | Material | Material thickness [mm] | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 954096 | Tension strap HH60 | $680 \times 60$ | 5250 Galvanised | 3 | 1 |
| 954098 | Tension strap HH7O | $740 \times 70$ | S250 Galvanised | 3 | 1 |



Tension straps $\mathrm{HH} 60 / \mathrm{HH} 70$ for fastening wall- and ceiling elements.

## TENSION STRAP HH6O - STATIC VALUES



| Load direction Fl |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Connection Timber-Timber |  |  |  |  |  |  |  |  |
| Leg connection 1 | $\begin{gathered} \text { Paneltwistec } \mathrm{CH} \varnothing 5 \times 120 \\ \mathrm{n}=9 \end{gathered}$ | $\operatorname{Anchor~nails~} \wp 4 \times 40_{n=6}$ | $\text { Anchor nails } \wp 4 \times 50$ | $\begin{gathered} \text { Anchor noils } \wp 4 \times 60 \\ n=6 \end{gathered}$ | $\begin{gathered} \text { Angle-bracket screw } 05 \times 40 \\ n=6 \end{gathered}$ | $\begin{gathered} \text { Angle-bracket screw } 05 \times 50 \\ n=6 \end{gathered}$ | $\begin{gathered} \text { Angle-brackets scew } 05 \times 60 \\ n=6 \end{gathered}$ | Steel |
| Leg connection 2 | $\begin{gathered} \text { Paneltwistec } \mathrm{CH} \subset 5 \times 120 \\ n=9 \end{gathered}$ | Anchor nails $04 \times 40$ $\mathrm{n}=6$ | $\begin{gathered} \text { Anchor nails } \varnothing 4 \times 50 \\ n=6 \end{gathered}$ | Anchor noils $04 \times 60$ $n=6$ | Angle-bracketscrew $05 \times 40$ $\mathrm{n}=6$ | $\begin{gathered} \text { Angle-bracketscrew } 05 \times 50 \\ n=6 \end{gathered}$ | Angle-brackets screw $05 \times 60$ $\mathrm{n}=6$ | S250 |
| Char. tensile capacity [kN] | 27 | 9,4 | 11 | 11,4 | 10,9 | 12 | 13,1 | 28,5 |

The load-bearing capaciies were determined based on ETA-19/0020 Characterisicic load-bearing capacity in KN , wood strength class $350 \mathrm{~kg} / \mathrm{m}^{3}$ char. Gross density.
The minimum distances between the connectors and the edges according to EC 5 must be complied with.
Please note: Verity the assumptions made. The stated values, and type and number of joining devices are based on preliminary meassurements. Projects are to be dimensioned exclusively by authorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

TENSION STRAP HH70 - STATIC VALUES


| Load direction Fl |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Connection Timber-Timber |  |  |  |  |  |  |  |  |
| Leg connection I | $\begin{gathered} \text { Paneltwistec CH } \varnothing 5 \times 120 \\ n=12 \end{gathered}$ | Anchor nails $\emptyset 4 \times 40$ $\mathrm{n}=8$ | $\begin{gathered} \text { Anchor nails } \varnothing 4 \times 50 \\ n=8 \end{gathered}$ | $\begin{gathered} \text { Anchor nails } \varnothing 4 \times 60 \\ n=8 \end{gathered}$ | Angle-bracket screw $05 \times 40$ $\mathrm{n}=8$ | Angle-bracketscrew $05 \times 50$ $n=8$ | Angle-bracketscrew $05 \times 60$ $\mathrm{n}=8$ | Steel |
| Leg connection 2 | $\begin{gathered} \text { Paneltwistec } \mathrm{CH} \cap 5 \times 120 \\ n=12 \end{gathered}$ | Anchor nails $04 \times 40$ $\mathrm{n}=8$ | $\text { Anchor nails } \varnothing 4 \times 50$ | $\begin{gathered} \text { Anchor nails } \varnothing 4 \times 60 \\ n=8 \end{gathered}$ | Angle-bracketscrew $05 \times 40$ $\mathrm{n}=8$ | Angle-bracketscrew $05 \times 50$ $\mathrm{n}=8$ | Angle-bracketscrew $05 \times 60$ $\mathrm{n}=8$ | 5250 |
| Char. tensile capacity [kN] | 35 | 12,5 | 14,7 | 15,2 | 17,1 | 18,2 | 19,4 | 37,4 |

The load-bearing capacities were determined based on ETA-19/0020 Characterisicic load-bearing capacity in kN , wood strength class $350 \mathrm{~kg} / \mathrm{m}^{3}$ char. Gross density.
The minimum distances between the connectors and the edges according to EC5 must be complied with.
Please note: Verity the assumptions made. The stated values, and type and number of joining devices are based on preliminary meassurements. Projects are to be dimensioned exclusively by outhorised persons in accordance with the State Building Code.
As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

## Gurotec

## SHEAR WALL CONNECTOR

FOR THE COMPENSATION OF UNEVENNESS IN CONSTRUCTION ELEMENTS

## ADVANTAGES

- Allows high shear force transmission between the wall elements
- Compensates for unevenness between building elements
- Does not protrude from the wall


## INSTRUCTIONS FOR USE

To install the shear wall connector, first cut a groove in each wall at the same height. The shear wall connector is then inserted into the milling and fixed with two screws. The flatness of the connector helps compensate for slight differences in height between the walls. The screw connection also pulls both walls horizontally to the connector, thus straightening out slight unevenness here as well.

Suitable for use with:
KonstruX ST CH Ø 8,0 mm
Scope of delivery includes screws

| Art. no. | Name | Dimensions [mm] ${ }^{\text {a/ }}$ | Pu* |
| :---: | :---: | :---: | :---: |
| Onreverst | Sher Vall (ometor | 100 $19 \times 80$ | Onreupes |
|  |  |  |  |




Unevenness compensation through screws and edges


## Gurotec

## ASSEMBIY CONNECTOR

## FOR CONNECTING TWO TIMBER CONSTRUCTION ELEMENTS IN SYSTEMS BUULDING

## ADVANTAGES

- Can be used regardless of weather conditions
- Easy assembly
- Quick and easy element positioning


## DESCRIPTION

The Eurotec assembly connector consists of two individual components that interlock during assembly. It serves as a preparatory element in system construction.

## INSTRUCTIONS FOR USE

We recommend our Paneltwistec $\mathrm{AGCH} 6 \times 80 \mathrm{~mm}$ for the use of the assembly connector. It is flush-mounted in a groove positioned at any chosen location on the construction elements. Once the elements have been inserted, the assembly connector is hidden inside the wall. The assembly connector must have a screw inserted in every screw hole. Our assembly connector is designed purely for guidance purposes. It cannot be used to absorb forces.

| Art. no. | Name | Dimensions $[\mathrm{mm}]^{0}$ | PU* |
| :--- | :--- | :--- | ---: |
| 800272 | Assembly conector | $32,7 \times 175 \times 29,7$ | 50 |


a) Height $x$ Length $x$ Width
*incl. 150 screws per PU




Step 1


Note
The assembly connector is not a connector that should be exposed to large, permanent load it is only a mounting tool!

## Gurotec

## MAGNUS HOOK CONNECTOR

## TIMBER CONNCTOR FOR MAIN-SECONDARY BEAM JOINTS

## ADVANTAGES

- Easy assembly
- High level of prefabrication
- Suitable for high joints
- Visible and hidden loads
- Milling cutter and milling and assembly iig available

ECS calculation soffware for free preliminary calculation

## INSTRUCTIONS FOR USE



The Magnus should always be fully unscrewed to ensure an easy and safe installation. Whether surface-mounted or recessed, the milling and mounting iig shows the connector where to fit. Sides and end grain surfaces must be flat to avoid any deformation of the connector during the assembly.


1 Insert $90^{\circ}$ fully threaded screws and fix Magnus to the wood


3
use fixing screws to secure the joint against lifting out


4
Joint complete


Connector


Fixing screws


## Gurotec

## OVERVIEW OF MAGNUS HOOK CONNECTORS



| Art. no. | Name | Dimensions | PU* | Fully threaded screws ${ }^{\text {b }}$ |  | Fixing screws ${ }^{\text {b }}$ ) |  | Main beam |  | Secondary beam sufface-mounted |  | Secondary beam flush-mounted |  |  |  | characteristic load-bearing capacity FRke |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx D ${ }^{\text {a }}$ |  | Dimension | $\mathrm{n}_{\text {per }}$connector | Dimension | nper connector | min. <br> WMB | min. <br> Нмв | min. <br> WSB | min. <br> Hsb | $\min _{W_{S B^{C}}}$ | min. <br> HsB | $W_{F}$ | DM ${ }^{\text {d) }}$ | Fl,Rk | F2,Rk | F3,Rk | F4,Rk |
|  |  | [mm] |  | [mm] |  | [mm] |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [kN] | [kN] | [kN] | [kN] |
| 94887 | Magus XS 30 30 | $30 \times 30 \times 9$ | 20 | 4,0 $\times 30$ | 6 | $4,2 \times 26$ | 1 | 40 | 40 | 40 | 40 | 40 | 40 | 30 | 9 | 1,2 | 1,57 | 1,70 | 1,19 |
| 94887 | Magnus $50 \times 60$ | $50 \times 60 \times 13$ | 10 | $4,0 \times 60$ | 8 | $4,2 \times 26$ | 2 | 60 | 80 | 60 | 80 | 80 | 80 | 50 | 13 | 3,73 | 7,25 | 5,00 | 1,92 |
| 948876 | Magnus $50 \times 80$ | $50 \times 80 \times 13$ | 10 | $4,0 \times 60$ | 12 | $4,2 \times 26$ | 2 | 60 | 100 | 60 | 100 | 80 | 100 | 50 | 13 | 3,73 | 14,50 | 5,00 | 2,80 |
| 94887 | Magus $50 \times 100$ | $50 \times 100 \times 13$ | 10 | $4,0 \times 60$ | 18 | $4,2 \times 26$ | 2 | 60 | 120 | 60 | 120 | 80 | 120 | 50 | 13 | 7,46 | 21,75 | 5,00 | 4,41 |
| 944878 | Magus M70 120 | $70 \times 120 \times 17$ | 10 | $5,0 \times 80$ | 13 | $4,8 \times 60$ | 2 | 80 | 140 | 80 | 140 | 100 | 140 | 70 | 17 | 5,49 | 21,34 | 13,00 | 5,17 |
| 948879 | Magus M70 140 | $70 \times 140 \times 17$ | 10 | $5,0 \times 80$ | 16 | $4,8 \times 60$ | 2 | 80 | 160 | 80 | 160 | 100 | 160 | 70 | 17 | 5,49 | 32,00 | 13,00 | 6,09 |
| 94488 | Magnus M70 160 | $70 \times 160 \times 17$ | 10 | 5,0×80 | 21 | $4,8 \times 60$ | 2 | 80 | 180 | 80 | 180 | 100 | 180 | 70 | 17 | 10,98 | 37,34 | 13,00 | 8,27 |
| 94488 | Magus M70 180 | $70 \times 180 \times 17$ | 10 | 5,0×80 | 24 | $4,8 \times 60$ | 2 | 80 | 200 | 80 | 200 | 100 | 200 | 70 | 17 | 10,98 | 42,67 | 13,00 | 9,32 |
| 94488 | Magnus $1110 \times 220$ | $110 \times 220 \times 19$ | 4 | $8,0 \times 120$ | 13 | $4,8 \times 60$ | 2 | 120 | 240 | 120 | 240 | 140 | 240 | 110 | 19 | 9,29 | 36,10 | 23,00 | 13,96 |
| 94888 | Magnus $1110 \times 260$ | $110 \times 260 \times 19$ | 4 | $8,0 \times 120$ | 17 | $4,8 \times 60$ | 2 | 120 | 280 | 120 | 280 | 140 | 280 | 110 | 19 | 13,93 | 45,13 | 23,00 | 17,98 |
| 944884 | Magnus $1110 \times 300$ | $110 \times 300 \times 19$ | 4 | $8,0 \times 120$ | 20 | $4,8 \times 60$ | 2 | 120 | 320 | 120 | 320 | 140 | 320 | 110 | 19 | 13,93 | 54,15 | 23,00 | 20,56 |
| 944887 | Magnus $110 \times 340$ | $110 \times 340 \times 19$ | 4 | $8,0 \times 120$ | 22 | $4,8 \times 60$ | 2 | 120 | 360 | 120 | 360 | 140 | 360 | 110 | 19 | 13,93 | 63,18 | 23,00 | 24,67 |
| 944888 | Magnus $110 \times 380$ | $110 \times 380 \times 19$ | 4 | $8,0 \times 120$ | 25 | $4,8 \times 60$ | 2 | 120 | 400 | 120 | 400 | 140 | 400 | 110 | 19 | 9,29 | 72,20 | 23,00 | 26,96 |
| 948889 | Magnus $110 \times 580$ | $110 \times 580 \times 19$ | 4 | $8,0 \times 120$ | 38 | $4,8 \times 60$ | 2 | 120 | 600 | 120 | 600 | 140 | 600 | 110 | 19 | 9,29 | 126,35 | 23,00 | 43,29 |

${ }^{*} 1$ connector consists of 2 individual parts
a) $D=$ assembly thickness
b) Incuded in delivery
c) Recommended minimum width of the secondary beam with the connector flush-mounted
d) To make installation easier, it is advantageous to reduce the milling depth slightly, especially for larger wood dimensions.
e) Both beams softwood with a gross density of $\rho \mathrm{k}=380 \mathrm{~kg} / \mathrm{m}^{3}$.

The specified characterisic values of the load-bearing capacity FRk apply to the specified fimber cross-sections, centred force application along the respective beam axis as well as connector installation flush with the top edge of the main and secondary beams. Calculation according to EAA $15 / 0761$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typoographical and printing errors.
The characterisic values of the load-bearing capacity FFks should not be treated as equivalent to the max. possible load (the max. force). The characterisici values of the load-bearing capacity Frk should be reduced to the design values Frd in terms of the service class and the load duration class: Frd= FRk x kmod $/ \gamma \mathrm{M}$.
Please note: These are planning aids. Projects must only be calculated by authorised persons.

## INSTALLATION ACCESSORIES

| Milling and assembly jig | Art. no. | Suitable for | PU |
| :---: | :---: | :---: | :---: |
| For Magnus hook connector | 94867 | Magnus XS | 1 |
|  | 94889 | Magus 5 | 1 |
|  | 94889 | Magnus M | 1 |
|  | 944870 | Magnus L200/260/300 | 1 |
|  | 94903 | Magnus L340/380/420 | 1 |
|  | 949904 | Magnus 460//50//40/580 | 1 |
|  | DESCRIP |  |  |
|  | - Insertio |  |  |
|  | - Milling |  |  |

Milling cutter
For Magnus hook connector


| Art. no. | Suitable for | Shaff diameter [mm] | PU |
| :--- | :--- | :--- | ---: |
| 949336 | Magnus XS | 6,35 | 1 |
| 29686 | Magnus S | 8 | 1 |
| 2966 | Magnus M und L | 8 | 1 |

THE FOLLOWING MUST BE OBSERVED IN THE EVENT OF FLUSH-MOUNTED INSTALLATION IN THE SECONDARY BEAM

- The beam's minimum width must be increased so that there is enough surrounding wood remaining at the side for the milling work
- The beam must be milled out at full height

THE FOLLOWING MUST BE OBSERVED IN THE EVENT OF FLUSH-MOUNTED INSTALLATION
IN THE MAIN BEAM

- The main beam's load-bearing cross-section is reduced by the connector's assembly thickness
- The beam's minimum width must be adjusted (screw length)



## Eurotec



| Art. no. | Name | Dimensions | PU* | Fully threaded screws ${ }^{\text {b }}$ ) |  |  |  |  |  | Fixing screws ${ }^{\text {b }}$ ) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx Da) |  | Dimensions | ntotal | In the main beam |  | In the secondary beam |  | Dimensions | n |
|  |  | [mm] |  | [mm] |  | n90 ${ }^{\circ}$ | 1445 | n90 ${ }^{\circ}$ | 145 ${ }^{\circ}$ | [mm] |  |
| 94877 | Magnus XS $30 \times 30$ | $30 \times 30 \times 9$ | 20 | 4,0×30 | 6 | 3 | - | 3 | - | $4,2 \times 26$ | 1 |

${ }^{*} 1$ connector consists of 2 individual parts
a) $D=$ assembly thickness
b) Incuded in delivery

| Art. no. | Name | Dimensions | Main beam |  | Secondary beam sufface-mounted |  | Secondary beam flush-mounted |  |  |  | characterisicic lood-bearing (cppacity FRk ${ }^{\text {d }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{\text {dol }}$ |  |  | min. WSB | min. Hs | min. WS ${ }_{\text {b }}{ }^{\text {b }}$ | min. Hsb | WM | DM ${ }^{\text {c }}$ | $\mathrm{F}_{1, \mathrm{Rk}}$ | F2,Rk | ,Rk | F4,Rk |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] |  | [mm] | [kN] | [kN] | [kN] | [kN] |
| 14874 | Magus $\times 530 \mathrm{x}$ | 0x30x9 | 40 | 40 | 40 | 40 | 40 | 40 | 30 | 9 | 1,12 | 1,57 | 1,0 | 1,19 |

a) $D=$ assembly thickness
b) Incuded in delivery
c) Recommended minimum width of the secondary beam with the connector flush-mounted
d) To make installation eassier, it is advantageous to reduce the milling depth slightly, especially for larger wood dimensions.
e) Both beams softwood with a gross density of $\mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$.

The specified characterisicic values of the load-bearing capacity FRk apply to the specified timber cross-sections, centred force application along the respective beam axis as well as connector installation flush with the top edge of the main and secondary beams.
Calculation according to ETA $15 / 0761$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculctions.
All values are calculated minimum values and are subject to typographical and printing errors.
The characterisicic values of the load-bearing capacity FRk should not be treated as equivalent to the max. possible load (the max. force). The charocterisicic values of the lood-bearing capacity FRk should be redveed to the design values FRd in terms of the service class and the lood duration class: FRd $=$ FRk $\mathrm{x} \mathrm{mod} / \gamma \mathrm{M}$.
Please note: These are planning aids. Projects must only be calculated by authorised persons.


| Art. no. | Name | Dimensions | PU* | Fully threaded screws ${ }^{\text {b }}$ ) |  |  |  |  |  | Fixing screws ${ }^{\text {b }}$ ) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{\text {a) }}$ |  | Dimensions | ntotal | In the main beam |  | In the secondary beam |  | Dimensions | n |
|  |  | [mm] |  | [mm] |  | n90 ${ }^{\circ}$ | n44 ${ }^{\circ}$ | n90 ${ }^{\circ}$ | 145 ${ }^{\circ}$ | [mm] |  |
| 94875 | Magus $50 \times 60$ | $50 \times 60 \times 13$ | 10 | 4,0×60 | 8 | 2 | 2 | 2 | 2 | $4,2 \times 26$ | 2 |

${ }^{*} 1$ connector consists of 2 individual parts
a) $D=$ assembly thickness
b) Incuded in delivery

| Art. no. | Name | Dimensions | Main beam |  | Secondary beam surface-mounted |  | Secondary beam flush-mounted |  |  |  | characteristic lood-bearing c cpacity $F$ Fk ${ }^{\text {d) }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{\text {a }}$ |  |  | min. WSB | min. Hsb | min. W(Sb ${ }^{\text {b }}$ | min. HSB | WM | DM ${ }^{\text {c }}$ | $\mathrm{F}_{1, \mathrm{lk}}$ | F2,Rk | $\mathrm{F}_{3, \mathrm{Rk}}$ | F4,Rk |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] |  |  | [kN] | [kN] | [kN] | [kN] |
| 4875 | Magus 550 | $50 \times 60 \times 13$ | 60 | 80 | 60 | 80 | 80 | 80 | 50 | 13 | 3,73 | 7,25 | 5,00 | 192 |

a) $D=$ assembly thickness
b) Incuded in delivery
c) Recommended minimum width of the secondary beam with the connector flush-mounted
d) To make installation eassier, it is advantageous to reduce the milling depth slightly, especially for larger wood dimensions.
e) Both heams softwood with a gross density of $\mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$.

The specified characterisicic valves of the lood-bearing capacity FRk apply to the specified fimber cross-sections, centred force application along the respective beam axis as well as connector installation flush with the top edge of the main and secondary beams.
Calculation according to ETA $15 / 0761$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
The characteristic values of the load-bearing capacity Frk should not be treated as equivalent to the max. possible lood (the max. force). The characterisicic values of the load-bearing capacity FRk should be reduced to the design values Frd in terms of the service class and the load duration class: $\mathrm{Frd}=\mathrm{FRk} \mathrm{x}$ kod $/ \gamma \mathrm{M}$.
Please note: These are planning ciids. Projects must only be calculated by outhorised persons.

## Eurotec

MAGNUS S $50 \times 80$

${ }^{*} 1$ connector consists of 2 individual ports
a) $D=$ assembly thickness
b) Incuded in delivery

| Art. no. | Name | Dimensions | Main beam |  | Secondary beam surface-mounted |  | Secondary beam flush-mounted |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{\text {a }}$ |  |  | min. WSB | min. HSB | min. WSS ${ }^{\text {b }}$ | min. HSB | WM $\mathrm{DM}^{\text {c }}$ | F1,Rk | F2,Rk | $\mathrm{F}_{3, \mathrm{Rk}}$ | F4,Rk |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] [mm] | [kN] | [kN] | [kN] | [kN] |
| 94876 | nurs $50 \times 80$ | $5 \times 80 \times 13$ | 60 | 100 | 60 | 100 | 80 | 100 | 50 | 3,73 | 14,50 | 5,00 | 280 |

a) $D=$ assembly thickness

## b) Incuded in delivery

c) Recommended minimum width of the secondary beam with the connector flush-mounted
d) To make installataion easier, it is advantageous to reduce the milling depth slightly, especially for larger wood dimensions.
e) Both beams softwood with a gross density of $\mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$.

The specified characterisic values of the load-bearing capacity FRk apply to the specified fimber cross-sections, centred force application along the respective heam axis as well as connector installation flush with the top edge of the main and secondary beams.
Calculation according to EAA $15 / 0761$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typoographical and printing errors.
The characterisicic values of the lood-bearing capacity Frk should not be treated as equivalent to the max. possible load (the max. force). The characterisicic values of the lood-bearing capacity FRk should be recuced to the design values FRd in terms of the service class and the load duration class: Frd= FRk x kmod $/ \gamma \mathrm{M}$.
Please note: These are planning cids. Projects must only be calculated by authorised persons.


| Art. no. | Name | Dimensions | PU* | Fully threaded screws ${ }^{\text {b }}$ ) |  |  |  |  |  | Fixing screws ${ }^{\text {b }}$ ) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx Da) |  | Dimensions | ntotal | In the main beam |  | In the secondary beam |  | Dimensions | n |
|  |  | [mm] |  | [mm] |  | n90 ${ }^{\circ}$ | n45 ${ }^{\circ}$ | n90 | n45 ${ }^{\circ}$ | [mm] |  |
| 94887 | Magnus $550 \times 100$ | $50 \times 100 \times 13$ | 10 | 4,0×60 | 18 | 2 | 6 | 4 | 6 | $4,2 \times 26$ | 2 |

* 1 connector consists of 2 individual parts
a) $D=$ assembly thickness
b) Incuded in delivery

| Art. no. | Name | Dimensions | Main beammin. WMB min. HMB |  | Secondary beam sufface-mounted |  | Secondory beam flush-mounted |  |  |  | characterisisic lood bearing (capacity F. $\mathrm{Rk}^{(l)}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{\text {a }}$ |  |  | min. WSB | min. Hsb | min. Ws ${ }^{\text {b }}$ ) | min. HSB | WM | DM ${ }^{\text {c }}$ | Fl,Rk | F2,Rk | $\mathrm{F}_{3, \mathrm{k} k}$ | F4,kk |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] |  | [kN] | [kN] | [kN] | [kN] |
| 94887 | S50x 100 | $50 \times 100 \times 13$ | 60 | 120 | 60 | 120 | 80 | 120 | 50 | 13 | 7,46 | 21,5 | 5,00 | 441 |

a) $D=$ assembly thickness
b) Incuded in delivery
c) Recommended minimum width of the secondary beam with the connector flush-mounted
d) To make installation easier, it is advantageous to reduce the milling depth slightly, especially for larger wood dimensions.
e) Both beams softwood with a gross density of $\mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$.

The specified characterisicic values of the load-bearing capacity FRk apply to the specified timber cross-sections, centred force application dong the respective beam axis as well as connector installation flush with the top edge of the main and secondary beams.
Calculation according to ETA $15 / 0761$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
The characteristic values of the load-bearing capacity Frk should not be trected as equivalent to the max. possible lood (the max. force). The characterisicic values of the load-bearing capacity FRk should be recuved to the design values Frd in terms of the service class and the load duration class: $\mathrm{Frd}=\mathrm{Frk} \mathrm{x} \mathrm{kmod}^{\operatorname{man}} / \gamma \mathrm{M}$.
Please note: These are planning aids. Projects must only be calculated by authorised persons.

## Gurotec



Symbolic illustrations: f.l.t.r. Main beam, secondary beam surface-mounted, secondary beam flush-mounted, connector dimensions


| Art. no. | Name | Dimensions | PU* | Fully threaded screws ${ }^{\text {b }}$ ) |  |  |  |  |  | Fixing screws ${ }^{\text {b }}$ ) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{\text {a) }}$ |  | Dimensions | ntotal | In the main beam |  | In the secondary beam |  | Dimensions | n |
|  |  | [mm] |  | [mm] |  | n90 ${ }^{\circ}$ | n45 ${ }^{\circ}$ | n90 ${ }^{\circ}$ | 145 ${ }^{\circ}$ | [mm] |  |
| 944878 | Magus M $70 \times 120$ | $70 \times 120 \times 17$ | 10 | $5,0 \times 80$ | 13 | 2 | 4 | 2 | 5 | 4,8×60 | 2 |

${ }^{*} 1$ connector consists of 2 individual parts
a) $D=$ assembly thickness
b) Incuded in delivery

| Art. no. | Name | Dimensions | Moin beam |  | Secondory beam suffac--mounted |  | Secondary beum flush-mounted |  |  |  | characteristic lood-bearing (cpacity FRk ${ }^{\text {d }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{\text {al }}$ |  |  | min. Wsb | min. HSB | min. WSs ${ }^{\text {b/ }}$ | min. HSB | WM | DM ${ }^{\text {c }}$ | Fl,Rk | F2,Rk | $\mathrm{F}_{3, \mathrm{Rk}}$ | F4,Rk |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [kN] | [kN] | [kN] | [kN] |
| 4487 | $1770 \times 120$ | 10x120x 17 | 80 | 140 | 80 | 140 | 100 | 140 | 70 | 17 | 5,49 | 21,34 | 13,0 | 5.17 |

a) $D=$ assembly thickness

## b) Incuded in delivery

c) Recommended minimum width of the secondary beam with the connector flush-mounted
d) To make installation easier, it is advantageous to reduce the milling depth slightly, especially for larger wood dimensions.
e) Both beams softwood with a gross density of $\mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$.

The specified characterisic values of the load-bearing capacity FRk apply to the specified fimber cross-sections, centred force application along the respective heam axis as well as connector installation flush with the top edge of the main and secondary beams.
Calculation according to EAA $15 / 0761$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
The characterisic values of the load-bearing capacity FFks should not be treated as equivalent to the max. possible load (the max. force). The characterisici values of the load-bearing capacity Frk should be reduced to the design values Frd in terms of the service class and the load duration class: FRd= FRk x $\mathrm{kmod}^{\mathrm{m}} / \gamma \mathrm{M}$.
Please note: These are planning aids. Projects must only be calculated by authorised persons.


| Art. no. | Name | Dimensions | PU* | Fully threaded screws ${ }^{\text {b }}$ ) |  |  |  |  |  | Fixing screws ${ }^{\text {b }}$ ) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx Da) |  | Dimensions | $n_{\text {notal }}$ | In the main beam |  | In the secondory beam |  | Dimensions | n |
|  |  | [mm] |  | [mm] |  | n90 ${ }^{\circ}$ | n45 ${ }^{\circ}$ | n90 ${ }^{\circ}$ | 145 ${ }^{\circ}$ | [mm] |  |
| 948879 | Magnus M $70 \times 140$ | $70 \times 140 \times 17$ | 10 | 5,0×80 | 16 | 2 | 6 | 2 | 6 | 4,8×60 | 2 |

${ }^{*} 1$ connector consists of 2 individual parts
a) $D=$ assembly thickness
b) Incuded in delivery

| Art. no. | Name | Dimensions | Moin beam |  | Secondory beam sufface-mounted |  | Secondary beam flush-mounted |  |  |  | characterisicic lood-bearing capacity FRK ${ }^{\text {d }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{\text {al }}$ |  |  | min. Wsb | min. HSB | min. Wsb ${ }^{\text {b }}$ | min. HSB | WM | DM ${ }^{\text {c }}$ | Fl,Rk | F2,Rk | $\mathrm{F}_{3, \mathrm{k} k}$ | F4,Rk |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [kN] | [kN] | [kN] | [kN] |
| 1879 | 1170 140 | $\times 10 \times 17$ | 80 | 160 | 80 | 160 | 100 | 160 | 70 | 17 | 5,49 | 3200 | 13,00 | 609 |

a) $D=$ assembly thickness
b) Incuded in delivery
c) Recommended minimum width of the secondary beam with the connector flush-mounted
d) To make installation eassier, it is advantageous to reduce the milling depth slightly, especially for larger wood dimensions.
e) Both beams softwood with a gross density of $\mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$.

The specified characterisicic values of the load-bearing capacity FRk apply to the specified fimber cross-sections, centred force application along the respective beam axis as well as connector installation flush with the top edge of the main and secondary beams.
Calculation according to ETA $15 / 0761$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
The characterisicic values of the load-bearing capacity Frk should not be trected as equivalent to the max. possible load (the max. force). The characterisicic values of the lood-bearing capacity FRk should be reduced to the design values Frd in terms of the service class and the load duration class: Frd= Frk x kmod $/ \gamma \mathrm{M}$.
Please note: These are planning aids. Projects must only be calculated by authorised persons.

## Eurotec



| Art. no. | Name | Dimensions | PU* | Fully threaded screws ${ }^{\text {b }}$ |  |  |  |  |  | Fixing screws ${ }^{\text {b }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx D ${ }^{\text {a) }}$ |  | Dimensions | ntotal | In the main beam |  | In the secondary beam |  | Dimensions | n |
|  |  | [mm] |  | [mm] |  | n90 ${ }^{\circ}$ | 145 ${ }^{\circ}$ | n90 ${ }^{\circ}$ | n45 ${ }^{\circ}$ | [mm] |  |
| 94888 | Mognus M $70 \times 160$ | $70 \times 160 \times 17$ | 10 | 5,0×80 | 21 | 2 | 8 | 4 | 7 | $4,8 \times 60$ | 2 |

${ }^{*} 1$ connector consists of 2 individual parts
a) $D=$ assembly thickness
b) Incuded in delivery

| Art. no. | Name | Dimensions | Main beammin. WMB min. HMB |  | Secondary beam sufface-mounted |  | Secondary beam fush-mounted |  |  |  | characterisitil lood -bearing (cppcity $\mathrm{FRk}^{\text {d) }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{0}$ ) |  |  | min. WSB | min. HSB | min. W( S $^{\text {b }}$ ) | min. HSB | WM | DM ${ }^{\text {c }}$ | F1,Rk | F2,Rk | , Rk | F4,Rk |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [kN] | [kN] | [kN] | [kN] |
| 4888 | mus $770 \times 160$ | $70 \times 160 \times 17$ | 80 | 180 | 80 | 180 | 100 | 180 | 70 | 17 | 10,98 | 37,34 | 13,00 | 8,7 |

a) $D=$ assembly thickness

## b) Incuded in delivery

c) Recommended minimum width of the secondary beam with the connector flush-mounted
d) To make installation easier, it is advantageous to reduce the milling depth slightly, especially for larger wood dimensions.
e) Both beams softwood with a gross density of $\mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$.

The specified characterisicic values of the load-bearing capacity FRk apply to the specified fimber cross-sections, centred force application along the respective beam axis as well as connector installation flush with the top edge of the main and secondary beams.
Calculation according to ETA $15 / 0761$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
The characcerisitic values of the lood-bearing capacity Frk should not be treated as equivalent to the max. possible load (the max. force). The characterisicic values of the lood-bearing capacity FRk should be reduced to the design values FRd in terms of the
service class and the load duration class: Frd $=$ FRk x mod $/ \gamma \mathrm{m}$.
Please note: These are planning aids. Projects must only be calculated by authorised persons.

${ }^{*} 1$ connector consists of 2 individual parts
a) $D=$ assembly thickness
b) Included in delivery

| Art. no. | Name | Dimensions | Main beam |  | Secondary beam surface-mounted |  | Secondary beam flush-mounted |  |  |  | characterisicil load-bearing capacity FRk ${ }^{\text {d }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{\text {a }}$ |  |  | min. Wsb | min. HSB | min. WS ${ }^{\text {b }}{ }^{\text {b }}$ | min. HSB | WM | DM ${ }^{\text {c }}$ | F\|,Rk | F2,Rk | $\mathrm{F}_{3, \mathrm{Rk}}$ | F4,R1k |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [kN] | [kN] | [kN] | [kN] |
| 94881 | mans $770 \times 180$ | $70 \times 180 \times 17$ | 80 | 200 | 80 | 200 | 100 | 200 | 70 | 17 | 10,98 | 42,67 | 13,00 | 9,32 |

a) $D=$ assembly thickness
b) Incuded in delivery
c) Recommended minimum width of the secondary beam with the connector flush-mounted
d) To make installotion eassier, it is advantageous to reduce the milling depth slightly, especially for larger wood dimensions.
e) Both beams softwood with a gross density of $\mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$.

The specified characteristic values of the load-bearing capacity FRk apply to the specified fimber cross-sections, centred force application along the respective beam axis as well as connector installation flush with the top edge of the main and secondary beams.
Calculation according to ETA 15/0761. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculacions.
All values are calculated minimum values and are subject to typographical and printing errors.
The characterisicic values of the load-bearing capacity FRk should not be treacted as equivalent to the max. possible load (the max. force). The characterisic values of the load-bearing capacity. FRk should be reduced to the design values Frd in terms of the service class and the load duration class: Frd= FRk x mod $/ \gamma \mathrm{M}$.
Please note: These are planning aids. Projects must only be calculated by authorised persons.

## Eurotec



Symbolic illustrations: f.l.t.r. Main beam, secondary beam surface-mounted, secondary beam flush-mounted, connector dimensions


| Art. no. | Name | Dimensions | PU* | Fully threaded screws ${ }^{\text {b }}$ ) |  |  |  |  |  | Fixing screws ${ }^{\text {b }}$ ) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx D ${ }^{\text {a) }}$ |  | Dimensions | ntotal | In the main beam |  | In the secondary beam |  | Dimensions | n |
|  |  | [mm] |  | [mm] |  | n90 ${ }^{\circ}$ | 145 ${ }^{\circ}$ | n90 ${ }^{\circ}$ | n45 ${ }^{\circ}$ | [mm] |  |
| 94882 | Magnus $1110 \times 220$ | $110 \times 220 \times 19$ | 4 | 8,0x 120 | 13 | 2 | 4 | 2 | 5 | 4,8×60 | 2 |

${ }^{*} 1$ connector consists of 2 individual parts
a) $D=$ assembly thickness
b) Incuded in delivery

| Art. no. | Name | Dimensions | Main heam |  | Secondary beam sufface-mounted |  | Secondary beam flush-mounted |  |  |  | characterisicil lood-bearing (cpacity Frk ${ }^{\text {d }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{\text {al }}$ |  |  | min. WSB | min. HSb | min. WSS ${ }^{\text {b }}$ | min. HSB | WM | DM ${ }^{\text {c }}$ | F1,Rk | F2,Rk | $\mathrm{F}_{3, \mathrm{Rk}}$ | F4,Rk |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] |  |  | [kN] | [kN] | [kN] | [kN] |
| 44882 | Magus $110 \times 220$ | 10x $220 \times 19$ | 120 | 240 | 120 | 240 | 140 | 240 | 110 | 19 | 9,29 | 36,10 | 23,00 | 13,6 |

a) $D=$ assembly thickness
b) Incuded in delivery
c) Recommended minimum width of the secondary beam with the connector flush-mounted
d) To make installation easier, it is advantageous to reduce the milling depth slightly, especially for larger wood dimensions.
e) Both beams softwood with a gross density of $\mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$.

The specified characteristic values of the load-bearing capacity FRk apply to the specified fimber cross-sections, centred force application along the respective beam axis as well as connector installation flush with the top edge of the main and secondary beams.
Calculation according to ETA $15 / 0761$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
The characteristic values of the load-bearing capacity FFks should not be treated as equivalent to the max. possible load (the max. force). The characterisic values of the lood-bearing capacity. FRk should be reduced to the design values Fed in terms of the
service class and the lood duration class: $\mathrm{Frd}=\mathrm{FRk} \mathrm{x} \mathrm{mod} / \gamma \mathrm{M}$.
The characterisicic load-bearing capacities for the L series were determined vsing $8 \times 120$ VG screws. Higher capacities can be achieved with longer screws (however, the minimum cross-sections of the supports also change)
Please note: These are planning aids. Projects must only be calculated by authorised persons.

## MAGNUS L $110 \times 260$



| Art. no. | Name | Dimensions | PU* | Fully threaded screws ${ }^{\text {b }}$ ) |  |  |  |  |  | Fixing screws ${ }^{\text {b }}$ ) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx D ${ }^{\text {a) }}$ |  | Dimensions | ntotal | In the main beam |  | In the secondory beam |  | Dimensions | n |
|  |  | [mm] |  | [mm] |  | n90 ${ }^{\circ}$ | n45 ${ }^{\circ}$ | n90 ${ }^{\circ}$ | 1445 | [mm] |  |
| 948883 | Magnus $1110 \times 260$ | $110 \times 260 \times 19$ | 4 | $8,0 \times 120$ | 17 | 3 | 5 | 5 | 6 | $4,8 \times 60$ | 2 |

${ }^{*} 1$ connector consists of 2 individual parts
a) $D=$ assembly thickness
b) Incuded in delivery

| Art. no. | Name | Dimensions | Main beam |  | Secondary beam sufface-mounted |  | Secondary beam flush-mounted |  |  |  | characterisicil load-bearing (cpacity Frk ${ }^{\text {d/ }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{\text {a }}$ | min. WMB | min. HMB | min. WSB | min. H SB | min. Wsb ${ }^{\text {b }}$ | min. HSB | WM | DM ${ }^{\text {c }}$ | $\mathrm{F}_{1, \mathrm{Rk}}$ | $\mathrm{F}_{2, \mathrm{Rk}}$ | $\mathrm{F}_{3, \mathrm{Rk}}$ | F4,Rk |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] |  | [mm] | [kN] | [kN] | [kN] | [kN] |
| 4883 | mus $110 \times 200$ | $110 \times 260 \times 19$ | 120 | 280 | 120 | 280 | 140 | 280 | 110 | 19 | 13,93 | 45,13 | 23,00 | 17,98 |

a) $D=$ assembly thickness
b) Incuded in delivery
c) Recommended minimum width of the secondary beam with the connector flush-mounted
d) To make installation easier, it is advantageous to reduce the milling depth slightly, especially for larger wood dimensions.
e) Both beams softwood with a gross density of $p \mathrm{k}=380 \mathrm{~kg} / \mathrm{m}^{3}$.

The specified characterisitic valves of the lood-bearing capacity FRk apply to the specified timber cross-sections, centred force application along the respective beam axis as well as connector installation flush with the top edge of the main and secondary beams. Calculation according to ETA $15 / 0761$. All mechanical values provided should be viewed as subject to the assumptions hat have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
The characcererstic values of the load-bearing capacity Frk should not be treated as equivalent to the max. possible load (the max. force). The characterisicic values of the load-bearing capacity FRk should be reduced to the design values Fre in terms of the service class and the load duration class: $\mathrm{Frd}=\mathrm{FRk} \mathrm{x} \mathrm{mod} / \gamma \mathrm{M}$.
The characterisic load-bearing capacities for the L series were determined using $8 \times 120$ VG screws. Higher capacities can be achieved with longer screws (however, the minimum cross-sections of the supports also change)
Please note: These are planning aids. Projects must only be calculated by authorised persons.

## Gurotec

MAGNUSLIIOX300


| Art. no. | Name | Dimensions | PU* | Fully threaded screws ${ }^{\text {b }}$ ) |  |  |  |  |  | Fixing screws ${ }^{\text {b }}$ ) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | W x H x D ${ }^{\text {a) }}$ |  | Dimensions | $n_{\text {total }}$ | In the main beam |  | In the secondary beam |  | Dimensions |  |
|  |  | [mm] |  | [mm] |  | n90 ${ }^{\circ}$ | n45 ${ }^{\circ}$ | n90 ${ }^{\circ}$ | n45 ${ }^{\circ}$ | [mm] | n |
| 94884 | Mognus L110 300 | $110 \times 300 \times 19$ | 4 | $8,0 \times 120$ | 20 | 4 | 6 | 3 | 7 | 4,8×60 | 2 |

* 1 connector consists of 2 individual parts
a) $D=$ assembly thickness
b) Included in delivery

| Art. no. | Name | Dimensions | Main beam |  | Secondory beam sufface-mounted |  | Secondary heam flush-mounted |  |  |  | characterisisic load-bearing capacity Frk ${ }^{\text {d }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{\text {a }}$ |  |  | min. WSB | min. Hsb | min. WS ${ }_{\text {S }}{ }^{\text {b }}$ | min. Hsb | WM | $\mathrm{DM}^{\text {c }}$ | $\mathrm{F}_{1, \mathrm{Rk}}$ | F2,Rk | F3,Rk | F4,Rk |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [kN] | [kN] | [kN] | [kN] |
| 944884 | Magus $110 \times 330$ | $110 \times 300 \times 19$ | 120 | 320 | 120 | 320 | 140 | 320 | 110 | 19 | 13,93 | 54,15 | 23,00 | 20,56 |

a) $D=$ assembly thickness
b) Incucted in delivery
c) Recommended minimum width of the secondary beam with the connector flush-mounted
d) To make installation easier, it is advantageous to reduce the milling depth slightly, especially for larger wood dimensions.
e) Both beams softwood with a gross density of $\rho \mathrm{k}=380 \mathrm{~kg} / \mathrm{m}^{3}$.

The specified characterisic valves of the load-bearing capacity FRk apply to the specified fimber cross-sections, centred force application along the respective beam axis as well as connector installation flush with the top edge of the main and secondary beams.
Calculation according to EAA $15 / 0761$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
The characteristic values of the load-bearing capacity FRks should not be treated as equivalent to the max. possible load (the max. force). The characteristic valves of the lood-bearing capacity Frks should be reduced to the design values Frd in terms of the
service class and the load duration class: $F R d=F R k x k_{\text {mod }} / \gamma \mathrm{M}$.
The characterisicic lood-bearing capacities for the L series were determined using $8 \times 120$ VG screws. Higher capacities can be achieved with longer screws (however, the minimum cross-sections of the supports also change)
Please note: These are planning aids. Projects must only be calculated by authorised persons.

## MAGNUSL $110 \times 340$



| Art. no. | Name | Dimensions | PU* | Fully threaded screws ${ }^{\text {b }}$ ) |  |  |  |  |  | Fixing screws ${ }^{\text {b }}$ ) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{\text {a) }}$ |  | Dimensions | ntotal | In the main beam |  | In the secondary beam |  | Dimensions | n |
|  |  | [mm] |  | [mm] |  | n90 ${ }^{\circ}$ | n45 ${ }^{\circ}$ | n90 ${ }^{\circ}$ | n45 ${ }^{\circ}$ | [mm] |  |
| 94887 | Magnus L110x 340 | $110 \times 340 \times 19$ | 4 | 8,0×120 | 22 | 3 | 7 | , |  | 4,8×60 | 2 |

* 1 connector consists of 2 individual parts
a) $D=$ assembly thickness
b) Incuded in delivery

| Art. no. | Name | Dimensions | Main beam |  | Secondary beam surface-mounted |  | Secondary beam flush-mounted |  |  |  | characterisisic lood-bearing (cppaciy $F_{\text {Rk }}{ }^{(l)}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{\text {a }}$ |  |  | min. WsB | min. ${ }^{\text {H }}$ | min. WS ${ }^{\text {b }}$ ) | min. HSB | WM | DM ${ }^{\text {(1) }}$ | Fl,kk | F2,Rk | $\mathrm{F}_{3,1 \mathrm{kl}}$ | F4,Rk |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] |  | [kN] | [kN] | [kN] | [kN] |
| 14887 | Magus 110 | $10 \times 300$ | 120 | 360 | 120 | 360 | 140 | 360 | 10 | 19 | 13,93 | 63,18 | 23,0 | 24,67 |

a) $D=$ assembly thickness
b) Incuded in delivery
c) Recommended minimum width of the secondary beam with the connector flush-mounted
d) To make installation easier, it is advantageous to reduce the milling depth slightly, especially for larger wood dimensions.
e) Both heams softwood with a gross density of $p \mathrm{k}=380 \mathrm{~kg} / \mathrm{m}^{3}$.

The specified characterisicic values of the load-bearing capacity Fpk apply to the specified fimber cross-sections, centred force application along the respective beam axis as well as connector installation flush with the top edge of the main and secondary beams.
Calculation according to ETA $15 / 0761$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
The characteristic values of the load-bearing capacity Frk should not be treated as equivalent to the max. possible load (the max. force). The characterisicic values of the load-bearing capacity FRk should be reduced to the design values Frd in terms of the
service class and the load duration class: $\mathrm{Frd}=\mathrm{Frk} \mathrm{x}$ mod $/ \gamma \mathrm{M}$.
The characteristic load-bearing capacities for the L series were determined using $8 \times 120$ VG screws. Higher capacities can be achieved with longer screws (however, the minimum cross-sections of the supports also change)
Please note: These are planning oids. Projects must only be calculcted by outhorised persons.

## Gurotec

MAGNUSLIIOX380


Symbolic illustrations: f.l.t.r. Main beam, secondary beam surface-mounted, secondary beam flush-mounted, connector dimensions


| Art. no. | Name | Dimensions | PU* | Fully threaded screws ${ }^{\text {b }}$ ) |  |  |  |  |  | Fixing screws ${ }^{\text {b }}$ ) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Wx $\mathrm{Hx}^{\text {da) }}$ |  | Dimensions | $n_{\text {total }}$ | In the main beam |  | In the secondary beam |  | Dimensions | n |
|  |  | [mm] |  | [mm] |  | n90 ${ }^{\circ}$ | n45 ${ }^{\circ}$ | n90 ${ }^{\circ}$ | n45 ${ }^{\circ}$ | [mm] |  |
| 94888 | Magnus L110x 380 | $110 \times 380 \times 19$ | 4 | 8,0× 120 | 25 | 4 | 8 | 2 | 11 | 4,8×60 | 2 |

${ }^{*} 1$ connector consists of 2 individual parts
a) $D=$ assembly thickness
b) Incuded in delivery

| Art. no. | Name | Dimensions | Main beam |  | Secondary beam sufface-movited |  | Secondary beam flush-mounted |  |  |  | characterisitil lood-bearing (cppaciy F Rk ${ }^{\text {d }}$ ) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx ${ }^{0}$ ) |  |  | min. WSB | min. Hs | min. WS ${ }_{\text {b }}{ }^{\text {b }}$ | min. H SB | WM | DM ${ }^{\text {c }}$ | Fl,Rk | F2,Rk | $\mathrm{F}_{3, \mathrm{Rk}}$ | F4,Rk |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] |  | [kN] | [kN] | [kN] | [kN] |
| 4488 | $10 x$ | $10 \times 380 \times 19$ | 120 | 400 | 120 | 400 | 140 | 400 | 110 | 19 | 9,29 | 12,20 | 23,00 | 26,66 |

a) $D=$ assembly thickness
b) Included in delivery
c) Recommended minimum width of the secondary beam with the connector flush-mounted
d) To make installation easier, it is advantageous to reduce the milling depth slightly, especially for larger wood dimensions.
e) Both beams softwood with a gross density of $\rho \mathrm{k}=380 \mathrm{~kg} / \mathrm{m}^{3}$.

The specified characterisic valves of the load-bearing capacity FRk apply to the specified fimber cross-sections, centred force application along the respective beam axis as well as connector installation flush with the top edge of the main and secondary beams.
Calculation according to EAA $15 / 0761$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
The characteristic values of the load-bearing capacity FRks should not be treated as equivalent to the max. possible load (the max. force). The characteristic valves of the lood-bearing capacity Frks should be reduced to the design values Frd in terms of the
service class and the load duration class: $F R d=F R k x k_{\text {mod }} / \gamma \mathrm{M}$.
The characterisicic lood-bearing capacities for the L series were determined using $8 \times 120$ VG screws. Higher capacities can be achieved with longer screws (however, the minimum cross-sections of the supports also change)
Please note: These are planning aids. Projects must only be calculated by authorised persons.


| Art. no. | Name | Dimensions | PU* | Fully threaded screws ${ }^{\text {b }}$ ) |  |  |  |  |  | Fixing screws ${ }^{\text {b }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | W x $\mathrm{x} \times \mathrm{D}^{\text {a) }}$ |  | Dimensions | $n_{\text {notal }}$ | In the main beam |  | In the secondary beam |  | Dimensions | n |
|  |  | [mm] |  | [mm] |  | n90 ${ }^{\circ}$ | n45 ${ }^{\circ}$ | n90 ${ }^{\circ}$ | 1445 | [mm] |  |
| 948889 | Magnus $1110 \times 580$ | 110 $\times 580 \times 19$ | 4 | $8,0 \times 120$ | 38 | 4 | 14 | 2 | 18 | 4,8×60 | 2 |

${ }^{*} 1$ connector consists of 2 individual parts
a) $D=$ assembly thickness
b) Included in delivery

| Art. no. | Name | Dimensions | Main beam |  | Secondary beam surface-mounted |  | Secondary beam flush-mounted |  |  |  | characteristic load-bearing (apacity Frkd) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | WxHx $\mathrm{D}^{\text {a }}$ | min. WMB | min. НMB | min. WSB | min. HsB | min. Wsb ${ }^{\text {b }}$ ) | min. HSB | WM | DM ${ }^{(1)}$ | Fl,Rk | F2,Rk | F3,Rk | F4,Rk |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [kN] | [kN] | [kN] | kN] |
| 948889 | Magus $1110 \times 580$ | $110 \times 580 \times 19$ | 120 | 600 | 120 | 600 | 140 | 600 | 110 | 19 | 9,29 | 126,35 | 23,00 | 43,29 |

a) $D=$ assembly thickness
b) Incuded in delivery
c) Recommended minimum width of the secondary beam with the connector flush-mounted
d) To make installation easier, itis advantageous to reduce the milling depth slightly, especially for larger wood dimensions.
e) Both beams softwood with a gross density of $\mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$.

The specified characteristic values of the load-bearing capacity FRk apply to the specified fimber cross-sections, centred force application along the respective beam axis as well as connector installation flush with the top edge of the main and secondary beams.
Calculation according to ETA $15 / 0761$. All mechanical values provided should be viewed as subject to the assumptions hat have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
The characterisicic values of the load-hearing capacity Frk should not be treated as equivalent to the max. possible lood (the max. force). The characterisicic values of the lood-bearing capacity FRk should be reduced to the design values Frd in terms of the service class and the load duration class: $\operatorname{Frd}=$ Frk $\times \operatorname{kmod} / \gamma \mathrm{M}$.
The characteristic load-bearing capacities for the L series were determined using $8 \times 120$ VG screws. Higher capacties can be achieved with longer screws (however, the minimum cross-sections of the supports also change)
Please note: These are planning ciids. Projects must only be calculated by outhorised persons.

## Eurotec



## EuroTec calculation service

## Magnus Hook Connector according to ETA-15/0761

by phone 02331 6245-444• by fax 02331 6245-200 • by e-mail technik@eurotec.team

Please contact our technical department or use the free calculation services in the service section of our website.
Contact

Trader:

Contact Person: $\qquad$
email: $\qquad$

Project: $\qquad$

## Project details

Main Beam
Width:
Height: $\qquad$ mm

Strength class: (e.g. C24, G124h etc.)

## Secondary Beam

| Width: | $\square$ |
| :--- | :--- |
| Height: | mm |
| Strength class: |  |
| (e.g. C24, G124h etc.) | mm |

## Loads (Characteristic values)

Load duration classPermanentLong
$\square$ MediumShort

## Installation

$\square \quad$ Surface assembly
$\square \quad$ Embedded in secondary beam
$\square \quad$ Embedded in main beam

Contractor:

Contact Person: $\qquad$

Phone:
email:
$\qquad$

## Gurotec

## T-PROFILE

## FOR HIDDEN ALUMINUM CONNECTIONS

## ADVANTAGES

- Hole pattern specially for Angle-bracket screw $\varnothing 5,0 \times 50 \mathrm{~mm}$
- Ideal for the timber-concrete connection with the Rock concrete screw $\varnothing 7,5$
- Creates a hidden connection
- No need of predrilling in combination with the EST dowel bar


## DESCRIPTION

The self-drilling EST-Dowel bar $\varnothing 7,5$ can be connected to the T-profile without predrilling. The T-profile has a hole pattern for the Angle-bracket screw 5,0 $\times 5,0 \mathrm{~mm}$. It can also be used together with the Rock concrete screw $\varnothing 7,5$ for the timber-concrete connection. Can be used in service classes 1 and 2 according to DIN EN 1995.


Suitable for use with:
KonstruX (p. 80), Angle-bracket screw (p. 108)
Panelwistec (p. 110), Rock concrete screw (p. 76)
EST dowel bar (p.70), Dowel bar (p.71)

| Art. no. | Name | Dimensions [mm] ${ }^{\text {a/ }}$ | Material | Material thickness [mm] | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 97652 | T-profile | $115 \times 2000 \times 80$ | Aluninum | 6 | 1 |
| a) Height $x$ Length $x$ Width |  |  |  |  |  |




[^0]

No need of predrilling with the EST dowel bar


Hole pattern with the Rock concrete screw

## Gurotec

## EST DOWEL BAR

## DOUBLE-THREADED SCREW WITH CYLINDER HEAD

Eurotec's self-drilling EST dowel bar is a double-threaded screw with an innovative arrow drill and a specifically developed chip-removing groove. Ideally suited for hidden connections in combination with our T-profile. The double-threaded screw has a cylinder head with TX drive. The special geometry of the arrow drill ensures a lower splitting effect when screwing in. The chip-removing groove ensures optimised screwing-in behaviour.

EST dowel bar | Suitable |
| :---: |
| for |
| $T$-profile |

ADVANTAGES / PROPERTIES

- Corrosion resistance
- Can be used in service classes 1 and 2 according to DIN EN 1991

Good resistance to mechanical stresses
No pilot-drilling necessary
With innovative arrow drill
No hammering of the screws thanks to TX-drive
Optimum chip-removing groove in the thread

- Suitable for timber and aluminum

| Art. no. | Dimensions [mm] | Thread length [mm] | Drive | PU |
| :---: | :---: | :---: | :---: | :---: |
| 80304 | 7,5 $\times 73$ | 27/0 | TX40 - | 50 |
| 800291 | 7,5993 | 27/8,5 | TX40 | 50 |
| 800305 | 7,5x113 | 36/12,5 | TX40 - | 50 |
| 800306 | 7,5×133 | 36/12,5 | TX40 - | 50 |
| 800307 | 7,5×153 | 36/12,5 | TX40 | 50 |
| 80027 | 7,5x 173 | 36/12,5 | TX40 | 50 |
| 800288 | 7,5x 193 | 36/12,5 | TX40 | 50 |
| 80028 | 7,5×213 | 36/12,5 | Tx40 - | 50 |
| 80020 | 7,5×233 | 36/12,5 | TX40 - | 50 |

TECHNICAL DRAWING


APPILCATION COMBINATION EST DOWEL BAR AND T.PROFILE


## DOWEL BAR

The rod dowel is a cylindrical bolt that has a phase at both ends for easier insertion. The rod dowel is suitable for both timber-timber joints and timber-steel joints. It is ideal for combination with our T-profile. The rod dowel is available in different diameters and lengths for an extremely wide range of applications. Please note the product table for this purpose.


## APPLICATION COMBINATION DOWEL BAR AND T-PROFILE



## Gurotec

## HIDDEN GROUND ANCHOR

## ADVANTAGES

- After installation of the floor, the hidden ground anchor is no longer visible - Dowel bar can easily be covered with thin wooden plates
- Easy insertion of the dowels, as the ground anchor is easy to drill through


## INSTRUCTIONS FOR USE

The later fastening point for the hidden ground anchor is prefabricated in the factory. The hidden ground anchor is screwed onto the wooden floor at the appropriate place. Then the wall can be placed over it. Through the groove in the wall, the hidden ground anchor can still be seen exactly as far as necessary. In the assembled state, the holes for the Dowel bar are drilled to ensure troublefree assembly. After the installation of the floor covering, the hidden ground anchor is no longer visible.

Suitable for use with:
KonstruX (S. 80), Dowel bar (p. 71)
SonoTec Angular Decoupler (p. 156)

6 dowel bars are required for fastening



One of our new products is the hidden ground anchor. As the name suggests, this connector is no longer visible after the floor covering has been installed, because it is fully recessed into the wall.



## Gurotec

## ROCK CONCRETE SCREW

## FOR FASTENING TO CONCRETE WTHOUT PLUGS

## ADVANTAGES

- No spreading effect due to small center and edge distances
- Immediately loadable - therefore no waiting times
- Small borehole depths and small drill hole diameters
- Can be used for components that are constantly exposed to weathering in outdoor areas


PROPERTIES

- Highest power transmission
- High-strength screw steel
- Extremely complex annealing process
- Special thread


## INSTRUCTIONS FOR USE

To insert the screw, the core hole is drilled first. The drill hole has to be cleaned, the chips have to be removed and finally the attachment part has to be fixed with the screw in the drill hole. The Rock concrete screw is developed for use in wood, concrete and stone.


| Rock concrete screw | 国: (E) | Art. no. | Dimensions [mm] | Head | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Hexagonal with flange, galvanised steel |  | 110227* | 7,5440 | SW13 | 100 |
|  |  | 110228* | 7,5450 | SW13 | 100 |
|  |  | 110229 | 7,5×60 | SW13 | 100 |
|  |  | 110230 | 7,5x80 | SW13 | 100 |
|  |  | 110231 | 7,5x 100 | SW13 | 100 |
|  |  | 110233* | 10,5 50 | SW15 | 100 |
|  |  | 110233* | 10,5 60 | SW15 | 100 |
|  |  | 110234 | $10,5 \times 80$ | SW15 | 100 |
|  |  | 110235 | 10,5 $\times 100$ | SW15 | 100 |
|  |  | 110236 | 10,5 $\times 120$ | SW15 | 100 |
|  |  | 11023 | 10,5 140 | SW15 | 100 |
|  |  | 110238 | 10,5 $\times 160$ | SW15 | 100 |
|  |  | *Scews |  |  |  |


| Rock concrete screw | 通: (E | Art. no. | Dimensions [mm] | Head | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Hexagonal with flange, special coated |  | 110253 | $16,5 \times 115$ | SW18 | 25 |
|  |  | 110254 | $16,5 \times 135$ | SW18 | 25 |
| $\triangle-$ |  | 110255 | $16,5 \times 160$ | SW18 | 25 |


| Rock concrete screw | Art. no. | Dimensions [mm] | Head | PU |
| :---: | :---: | :---: | :---: | :---: |
| Hexagonal, galvanised steel | 11033** | 7,5440 | SW13 | 100 |
|  | 110339* | 7,5,50 | SW13 | 100 |
|  | 110340 | 7,5660 | SW13 | 100 |
|  | 110341 | 7,5880 | SW13 | 100 |
|  | 11034* | 10,5 $\times 60$ | SW15 | 100 |
| - | 110343 | 10,5 88 | SW15 | 100 |
|  | 110344 | $10,5 \times 100$ | SW15 | 100 |
|  | 110345 | $10,5 \times 120$ | SW15 | 100 |
|  | 110346 | 10,5 $\times 140$ | SW15 | 100 |
|  | 11034 | $10,5 \times 160$ | SW15 | 100 |
|  | 110336* | 12,5 $\times 60$ | SW17 | 100 |
|  | 110337 | $12,5 \times 80$ | SW17 | 100 |
|  | 110327 | $12,5 \times 100$ | SW17 | 100 |
|  | 110328 | $12,5 \times 120$ | SW17 | 100 |
|  | 110329 | $12,5 \times 140$ | Sw17 | 100 |
|  | 110330 | $12,5 \times 160$ | SW17 | 50 |
|  | 110331 | $12,5 \times 180$ | SW17 | 50 |
|  | 110332 | $12,5 \times 200$ | SW17 | 50 |
|  | 110333 | $12,5 \times 240$ | SW17 | 50 |
|  | 110334 | $12,5 \times 280$ | Sw17 | 50 |
|  | 110335 | $12,5 \times 320$ | SW17 | 50 |
|  | *Scews $n$ |  |  |  |


| Rock concrete screw | \% C | Art. no. | Dimensions [mm] | Drive | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Countersunk head, galvanised steel |  | 110348* | 7,5440 | TX40 | 100 |
|  |  | 110349 | 7,5,60 | TX40 - | 100 |
|  |  | 110350 | 7,5, 80 | TX40 | 100 |
|  | \%em | 110351 | 1,5x 100 | TX40 | 100 |
|  |  | 110352 | 1,5 120 | TX40 | 100 |
|  |  | 110353 | 7,5x 140 | TX40 | 100 |
|  |  | 110354 | 7,5 160 | TX40 | 100 |
|  |  | *Screws no |  |  |  |

## Eurotec

## TECHNICAL INFORMATION ROCK CONCRETE SCREW



Rock, hexagonal with flange

| $\begin{aligned} & 7,5 \times 60 \\ & 1,5 \times 80 \end{aligned}$ | SW13 | 16,5 | 100 | 5 25 | 55 | 6,0 | 3,0 | 11,0 | 19,0 | 6 | 70 | 9 | 40 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10,5x80 |  |  |  | 5 |  |  |  |  |  |  |  |  |  |
| $10,5 \times 100$ |  |  |  | 25 |  |  |  |  |  |  |  |  |  |
| 10,5 120 | SW15 | 17,5 | 160 | 45 | 75 | 6,0 | 3,0 | 22,0 | 51,0 | 9 | 90 | 12 | 55 |
| 10,5 140 |  |  |  | 65 |  |  |  |  |  |  |  |  |  |
| $10,5 \times 160$ |  |  |  | 85 |  |  |  |  |  |  |  |  |  |
| $16,5 \times 115$ |  |  |  | 5 |  |  |  |  |  |  |  |  |  |
| $16,5 \times 135$ | Sw18 | 30,5 | 175 | 25 | 110 | 40,0 | 30,0 | 57,9 | 235,9 | 14 | 130 | 18 | 100 |
| $16,5 \times 160$ |  |  |  | 50 |  |  |  |  |  |  |  |  |  |
| Rock, hexagonal |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $7,5 \times 60$ | SW13 | n/a | 100 | 5 | 55 | 6,0 | 3,0 | 11,0 | 19,0 | 6 | 70 | 9 | 40 |
| $1,5 \times 80$ $10,5 \times 80$ |  |  |  | 25 5 |  |  |  |  |  |  |  |  |  |
| $10,5 \times 100$ |  |  |  | 25 |  |  |  |  |  |  |  |  |  |
| $10,5 \times 120$ | SW15 | n/a | 160 | 45 | 75 | 6,0 | 3,0 | 22,0 | 51,0 | 9 | 90 | 12 | 55 |
| 10,5 $\times 140$ |  |  |  | 65 |  |  |  |  |  |  |  |  |  |
| 10,5 $\times 160$ |  |  |  | 85 |  |  |  |  |  |  |  |  |  |
| 12,5x 80 | SW17 | n/a | 200 | 5 | 75 | 25,0 | 12,0 | 35,0 | 98,0 | 10 | 90 | 14 | 65 |
| $12,5 \times 100$ | SW17 | n/a | 200 | 5 | 95 | 25,0 | 12,0 | 35,0 | 98,0 | 10 | 110 | 14 | 65 |
| $12,5 \times 120$ |  |  |  | 25 |  |  |  |  |  |  |  |  |  |
| $12,5 \times 140$ |  |  |  | 45 |  |  |  |  |  |  |  |  |  |
| $12,5 \times 160$ |  |  |  | 65 |  |  |  |  |  |  |  |  |  |
| $12,5 \times 180$ |  |  |  | 85 |  |  |  |  |  |  |  |  |  |
| $12,5 \times 200$ |  |  |  | 105 |  |  |  |  |  |  |  |  |  |
| $12,5 \times 240$ |  |  |  | 145 |  |  |  |  |  |  |  |  |  |
| $12,5 \times 280$ |  |  |  | 185 |  |  |  |  |  |  |  |  |  |
| 12,5 320 |  |  |  | 225 |  |  |  |  |  |  |  |  |  |

Rock, countersunk head

| $7,5 \times 60$ |  |  |  | 5 |
| :--- | :--- | :--- | :--- | :--- |
| $7,5 \times 80$ |  |  |  | 25 |
| $7,5 \times 100$ | 14,0 | $n / a$ | 100 | 45 |
| $7,5 \times 120$ |  |  |  | 65 |
| $7,5 \times 140$ |  |  |  | 85 |
| $7,5 \times 160$ |  |  |  | 105 |

Setting tool: Electrical tangential impact wrench, max. power rating $T_{\text {max }}$ according to manufacturer's data, recommended $\mathrm{T}_{\text {max }}: 250 \mathrm{Nm}$ for Rock $7,5 \times \mathrm{L} ; 450 \mathrm{Nm}$ for Rock $10,5 \times \mathrm{L}$. and $12,5 \mathrm{LL}$. and $16,5 \mathrm{~L}$.
Note: A higher max. torque of the setting tool can lead to destruction of the drilling hole or damage to the screw.
Assembly with torque wrench: Recommended installation torque Tinst: 20 Nm for Rock $7,5 \mathrm{xL} ; 40 \mathrm{Nm}$ for Rock $10,5 \times \mathrm{L} .60 \mathrm{Nm}$ for Rock $12,5 \times \mathrm{L}$. and 120 Nm for $16,5 \mathrm{LL}$.
a) The calculation for a joint is to be performed according to EAAG-001 Annex C. b) Partial safety factors: $\gamma \mathrm{Ms}, \nu=1,5 ; \gamma M s, M=1,5$.

Please note: These are planning aids. Projects must only be calculated by authorised persons.

EuroTec calculation service

## Rock concrete screw according to ETA-15/0886

by phone 02331 6245-444 • by fax 02331 6245-200 • by e-mail technik@eurotec.team

Please contact our technical department or use the free calculation services in the service section of our website.

## Contact

Trader:

## Contact Person:

$\qquad$
e-mail: $\qquad$

Project: $\qquad$

## Contractor:

Contact Person: $\qquad$
Phone: $\qquad$
e-mail: $\qquad$

A detailed sketch of the joint must be enclosed with the inquiry, stating the following details:

- Geometry of concrete and attachment
- Edge and centre distances $C$ and $S$
- Position of attachment relative to concrete component
- Position (and angle, where applicable) of force application point on the attachment




## Screw selection

$\square \quad \varnothing 7,5 \mathrm{~mm}$ countersunk head
$\square \quad \varnothing 7,5 \mathrm{~mm}$ hex head, flange $\square$ $\varnothing 7,5 \mathrm{~mm}$ hex head
$\varnothing 10,5 \mathrm{~mm}$ hex head
$\varnothing 10,5 \mathrm{~mm}$ hex head, flange
$\varnothing 12,5$ mm hex, flange
$\varnothing 12,5$ hex head, flange

## Gurotec

## KONSTRUX FULLY THREADED SCREW

THE HIGH-PERFORMANCE SOLUTION FOR NEW CONSTRUCTION AND REFURBISHMENT

## ADVANTAGES

- High extraction resistance
- Strong joints
- Maximisation of the load-bearing capacity
- A time- and cost-saving alternative
- Hidden connections
- No pre-drilling required according to approval / ETA (recommended from screw lengths $\geq 245 \mathrm{~mm}$ )


## PROPERTIES

- Maximum load transmission
- High fire-resistance
- No thermal bridges


## INSTRUCTIONS FOR USE

KonstruX fully threaded screws maximize the load-bearing capacity of a connection due to the high thread extraction resistance in both components. When using partially threaded screws, the significantly lower head pull-through resistance in the attachment part limits the load-bearing capacity of the connection. KonstruX fully threaded screwn provide a cost-saving alternative to traditional connectors or timber connectors such as joist shoes and joist girders.






KonstruX in order to connect a wall with a sill plate.


## Gurotec



Connection of a wall and a support for the ceiling joist.


## Gurotec



Connection of ceiling elements through internal push board.


Connection of ceiling elements through upper push board.

## Gurotec




Mitred roof panels, screw connection with ridge purlin.


Mitred roof panels, diagonal screw connection.


Roof panels on butt joint, diagonal screw connection.

## Eurotec

## STARCASE CONSTRUCTION WITH CLT AND KONSTRUX




Attach the tier end frontal to the tier support.


Attach steps on top of the tier support.


## Gurotec

| KonstruX ST fully threaded screw \% C \% | Art. no. | Dimensions [mm] | Drive | PU |
| :---: | :---: | :---: | :---: | :---: |
| Cylinder head, galvanised | 908808 | 6,5 $\times 80$ | TX30 | 100 |
|  | 908809 | 6,5x 100 | TX30- | 100 |
|  | 908810 | $6,5 \times 120$ | TX30 - | 100 |
|  | 904811 | 6,5×140 | TX30 - | 100 |
|  | 908812 | 6,5×160 | TX30 - | 100 |
| BENEFITS OF DRILL POINT | 908813 | 6,5x 195 | TX30 - | 100 |
| Reduced screwing torque | 908825 | $8,0 \times 155$ | TX40 | 50 |
| High extraction resistance | 908826 | $8,0 \times 195$ | TX40 | 50 |
| , | 90882 | 8,0x 220 | TX40 | 50 |
| , | 908828 | 8,0x 245 | TX40 - | 50 |
|  | 908834 | 8,0 270 | TX40 - | 50 |
|  | 908829 | $8,0 \times 295$ | TX40 | 50 |
| , | 908830 | 8,0x 330 | TX40 | 50 |
|  | 908831 | $8,0 \times 375$ | TX40 | 50 |
| ) | 908832 | $8,0 \times 400$ | TX40 | 50 |
|  | 948804 | $8,0 \times 430$ | TX40 - | 50 |
|  | 948805 | $8,0 \times 480$ | TX40 | 50 |
|  | 948806 | 8,0x530 | TX40 - | 50 |
|  | 94880 | 8,0x580 | TX40 | 50 |
|  | 908815 | $10,0 \times 300$ | TX50 - | 25 |
|  | 908816 | $10,0 \times 330$ | TX50 - | 25 |
|  | 908817 | 10,0 $\times 360$ | TX50 - | 25 |
|  | 908818 | 10,0 $\times 400$ | TX50 - | 25 |
|  | 908819 | $10,0 \times 450$ | TX50 | 25 |
|  | 908820 | $10,0 \times 500$ | TX50 - | 25 |
|  | 908821 | 10,0 $\times 550$ | TX50 - | 25 |
|  | 908822 | $10,0 \times 600$ | TX50 - | 25 |



BENEFITS OF DRILL POINT

- Reduced screwing torque
- High extraction resistance


| Art. no. | Dimensions [mm] | Drive | PU |
| :---: | :---: | :---: | :---: |
| 908857 | 6,5x80 | TX30 - | 100 |
| 908858 | 6,5×100 | TX30 - | 100 |
| 908859 | 6,5×120 | TX30 | 100 |
| 908860 | 6,5x 140 | TX30 | 100 |
| 90779 | 8,0×95 | TX40 - | 50 |
| 90791 | $8,0 \times 125$ | TX40 | 50 |
| 90792 | $8,0 \times 155$ | Tx40 - | 50 |
| 90793 | $8,0 \times 195$ | TX40 - | 50 |
| 90779 | 8,0x 220 | TX40 - | 50 |
| 907795 | 8,0x 245 | TX40 - | 50 |
| 90776 | $8,0 \times 270$ | TX40 - | 50 |
| 90779 | $8,0 \times 295$ | TX40 - | 50 |
| 90779 | 8,0x330 | TX40 - | 50 |
| 907799 | 8,0x375 | TX40 - | 50 |
| 90880 | $8,0 \times 400$ | TX40 - | 50 |
| 908801 | $8,0 \times 430$ | TX40 - | 50 |
| 908802 | $8,0 \times 480$ | TX40 - | 50 |
| 908803 | 8,0x 545 | TX40 - | 50 |
| 90470 | $10,0 \times 125$ | TX50 - | 25 |
| 90471 | $10,0 \times 155$ | TX50 - | 25 |
| 90472 | $10,0 \times 195$ | TX50 - | 25 |
| 90473 | $10,0 \times 220$ | TX50 | 25 |
| 90774 | 10,0 $\times 245$ | TX50 | 25 |
| 90775 | $10,0 \times 270$ | TX50 | 25 |
| 904776 | $10,0 \times 300$ | TX50 | 25 |
| 90477 | 10,0×330 | TX50 - | 25 |
| 90478 | 10,0 $\times 360$ | TX50 | 25 |
| 90479 | $10,0 \times 400$ | TX50 - | 25 |
| 90778 | $10,0 \times 450$ | TX50 - | 25 |
| 904781 | $10,0 \times 500$ | TX50 - | 25 |
| 90778 | 10,0 $\times 550$ | TX50 - | 25 |
| 90478 | $10,0 \times 600$ | TX50 | 25 |


| KonstruX threaded screw 滑: (E | Art. no. | Dimensions [mm] | Drive | PU |
| :---: | :---: | :---: | :---: | :---: |
| Countersunk head, galvanised | 905737 | 11,3x300 | TX50 - | 20 |
|  | 905738 | 11,3x340 | TX50 - | 20 |
| $\cdots$ 为 | 905739 | 11,3x 380 | TX50 - | 20 |
|  | 905740 | 11,3x420 | TX50 - | 20 |
| ADVANTAGES SCREW TIP | 905741 | $11,3 \times 460$ | TX50 - | 20 |
|  | 90572 | 11,3x500 | TX50 - | 20 |
| Faster and easier screwing | 90574 | 11,3x540 | TX50 | 20 |
| Reduced spliting effect | 90574 | 11,3x580 | TX50 - | 20 |
|  | 905745 | 11,3x620 | TX50 - | 20 |
|  | 905746 | 11,3x660 | TX50 - | 20 |
|  | 90574 | 11,3x700 | TX50 - | 20 |
|  | 905748 | 11,3x750 | TX50 | 20 |
|  | 905749 | 11,3x800 | TX50 - | 20 |
|  | 904750 | 11,3x900 | TK50 - | 20 |
|  | 90475 | $11,3 \times 1000$ | TX50 - | 20 |


| KonstruX threaded screw ${ }_{\text {a }}$ | Art. no. | Dimensions [mm] | Drive | PU |
| :---: | :---: | :---: | :---: | :---: |
| Countersunk head, Stainless steel A4 | 905750 | 10,0 160 | TX50 | 25 |
|  | 905751 | $10,0 \times 200$ | TX50 | 25 |
|  | 905752 | 10,0 $\times 220$ | TX50 - | 25 |
|  | 905753 | 10,0 $\times 240$ | TX50 - | 25 |
|  | 905754 | 10,0 $\times 260$ | TX50 - | 25 |
|  | 905755 | $10,0 \times 280$ | TX50 - | 25 |
|  | 905756 | 10,0x 300 | TX50 - | 25 |
|  | 905757 | $10,0 \times 350$ | TX50 - | 25 |
|  | 905758 | $10,0 \times 400$ | TX50 | 25 |

## Eurotec



THE FAST AND SECURE TIMBERJOINT SYSTEM KONSTRUX CYLINDER-HEAD/COUNTERSUNK-HEAD SCREWS

| Application examples | Cylinder head |  |  | Countersunk head |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & 06,5 \\ & {[\mathrm{~mm}]} \end{aligned}$ | $\begin{aligned} & 08,0 \\ & {[\mathrm{~mm}]} \end{aligned}$ | $\begin{aligned} & 010,0 \\ & {[\mathrm{~mm}]} \end{aligned}$ | $\begin{aligned} & 06,5 \\ & {[\mathrm{~mm}]} \end{aligned}$ | $\begin{aligned} & 08,0 \\ & {[\mathrm{~mm}]} \end{aligned}$ | $\begin{aligned} & 010,0 \\ & {[\mathrm{~mm}]} \end{aligned}$ | $\begin{gathered} 011,3 \\ {[\mathrm{~mm}]} \end{gathered}$ |
|  | $X$ | X | X | X | X | X | $\mathbf{X}$ |
| Timber-timber under tension ot $45^{\circ}$ <br> Timber-timber under tension at $45^{\circ}$ | $\mathbf{X}$ | X | $\mathbf{X}$ | $\mathbf{X}$ | X | X | $\mathbf{X}$ |
| Steel-timber tensile loading <br> Steel-timber shearing <br> a | - | - | - | X | X | X | $\mathbf{X}$ |
| Steel-timber under tension ot $45^{\circ}$ <br> Steel-timber under tension at $45^{\circ}$ | - | - | - | $\mathbf{X}$ | X | X | $\mathbf{X}$ |
| Main-secondary beam connection <br> Post-crosspiece connection | X | $\mathbf{X}$ | X | X | X | $\mathbf{X}$ | - |
|  | X | X | X | X | X | $\mathbf{X}$ | $\mathbf{X}$ |
| Transverse-shear reinforcement at notch <br> Transverse-shear reinforcement at hole | $\mathbf{X}$ | X | $\mathbf{X}$ | X | X | X | X |
|  | - | X | $\mathbf{X}$ | - | X | X | X |
| Transverse-shear reinforcement of building trusses | - | - | X | - | - | X | X |

## Eurotec

## KONSTRUX FULLY THREADED SCREW

TECHNICAL INFORMATION

## KONSTRUX ST WITH CYLINDER HEAD AND DRILL POINT 6,5 TO 10,0 MM: TIMBER-TIMBER JOINTS



Calculation according to $\mathrm{EA}-11 / 0024$. Wood density $\rho \mathrm{k}=380 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
a) The characteristic valves of the lood-bearing capacity Rk cannot be treated as equivalent to the max. possible load (the max. force). Characterisici values of the lood-bearing capacity Rk should be reduced to dimensioning values Rd
with regard to the usage class and class of the load duration: $R_{d}=R_{k} \cdot \mathrm{kmod}_{\mathrm{m}} / \gamma \mathrm{\gamma}$. The dimensioning values of the lood-bearing capacity $\mathrm{R}_{\mathrm{d}}$ should be contrasted with the dimensioning values of the loads ( $\mathrm{R}_{\mathrm{d}} \geq \mathrm{Ed}$ ).
Example:
Characterisic value for constant load (dead weight) $G_{k}=2,00 \mathrm{kN}$ and variable load (e. g. snow lood) $Q_{k}=3,00 \mathrm{kN} . \mathrm{kmod}^{2}=0,9 . \gamma \mathrm{m}=1,3$.
$\rightarrow$ Dimensioning value of the lood $\mathrm{Ed}=2,00 \cdot 1,35+3,00 \cdot 1,5=7,20 \mathrm{kN}$.
The load-bearing capacity of the joint is therefore considered to have been demonstrated if $\mathrm{R}_{\mathrm{d}} \geq \mathrm{Ed}_{\mathrm{d}} \rightarrow \min \mathrm{R}_{\mathrm{k}}=\mathrm{R}_{\mathrm{d}} \cdot \gamma \mathrm{M} / \mathrm{kmod}$
i.e. the characteristic minimum value is calculated based on: $\min \mathrm{R}_{\mathrm{k}}=\mathrm{R}_{\mathrm{d}} \cdot \gamma_{\mathrm{M}} / \mathrm{kmod}_{\bmod } \rightarrow \mathrm{R}_{\mathrm{k}}=7,20 \mathrm{kN} \cdot 1,3 / 0,9=10,40 \mathrm{kN} \rightarrow$ comparison with table values.

Please note: These are planning aids. Projects must only be calculated by authorised persons.

## KONSTRUX ST WITH CYLINDER HEAD AND DRILL POINT

6,5 TO 10,0 MM: TIMBER-TIMBER JOINTS


Characterisic value of the joint's lood-bearing capacity Rax,k or Rk acc. to EAA-11/0024

| dl xL [ mm$]$ | A[mm] | $B[\mathrm{~mm}]$ | $\mathrm{Raxa}^{(\mathrm{K}}{ }^{\mathrm{a}} \cdot[\mathrm{kN}]$ | $\mathrm{Rk}^{(0)} \cdot[\mathrm{kN}]$ | ${\mathrm{Rax}, \mathrm{k}^{\text {a) }} \text {-[kN] }}^{\text {a }}$ | $\mathrm{Rk}^{(0)} \cdot[\mathrm{kN}]$ | ${\mathrm{Rax}, \mathrm{K}^{\text {a }}}^{\text {a }} \cdot[\mathrm{kN}]$ | $\mathrm{Rk}^{\text {a) }} \cdot[[\mathrm{kN}]$ | ${\mathrm{Rax}, \mathrm{k}^{\text {a) }} \text { - [kN] }}^{\text {a }}$ | $\mathrm{Rk}^{\text {a) }}$-[kN] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\alpha=45^{\circ}$ |  | $\begin{aligned} & \alpha A=90^{\circ} \\ & \alpha B=45^{\circ} \end{aligned}$ |  | $\begin{aligned} & \alpha A=90^{\circ} \\ & \alpha B=90^{\circ} \end{aligned}$ |  | $\begin{aligned} & \alpha A=45^{\circ} \\ & \alpha B=90^{\circ} \end{aligned}$ |  |
| 6,5 5160 | 60 | 80 | 5,95 | 4,21 | 5,95 | 4,21 | 5,95 | 4,21 | 5,95 | 4,21 |
| 6,5x 195 | 80 | 80 | 6,48 | 4,58 | 6,48 | 4,58 | 6,48 | 4,58 | 6,48 | 4,58 |
| 8, $\times 155$ | 60 | 60 | 6,65 | 4,70 | 6,65 | 4,70 | 6,65 | 4,70 | 6,65 | 4,70 |
| 8, $\times 195$ | 80 | 80 | 7,76 | 5,49 | 7,76 | 5,49 | 7,76 | 5,49 | 7,76 | 5,49 |
| 8,0 220 | 80 | 100 | 10,13 | 7,17 | 10,13 | 7,17 | 10,13 | 7,17 | 10,13 | 7,17 |
| 8,0×245 | 100 | 100 | 9,82 | 6,95 | 9,82 | 6,95 | 9,82 | 6,95 | 9,82 | 6,95 |
| 8,0×295 | 120 | 100 | 11,88 | 8,40 | 11,88 | 8,40 | 11,88 | 8,40 | 11,88 | 8,40 |
| 8,0×330 | 120 | 140 | 15,20 | 10,75 | 15,20 | 10,75 | 15,20 | 10,75 | 15,20 | 10,75 |
| 8, $\times 375$ | 140 | 140 | 16,79 | 11,87 | 16,79 | 11,87 | 16,79 | 11,87 | 16,79 | 11,87 |
| 8,0x 400 | 160 | 140 | 16,48 | 11,65 | 16,48 | 11,65 | 16,48 | 11,65 | 16,48 | 11,65 |
| $8,0 \times 430$ | 160 | 160 | 19,32 | 13,66 | 19,32 | 13,66 | 19,32 | 13,66 | 19,32 | 13,66 |
| $8,0 \times 480$ | 180 | 180 | 21,38 | 15,12 | 21,38 | 15,12 | 21,38 | 15,12 | 21,38 | 15,12 |
| 10,0x 300 | 120 | 120 | 15,03 | 10,63 | 15,03 | 10,63 | 15,03 | 10,63 | 15,03 | 10,63 |
| $10,0 \times 330$ | 120 | 140 | 18,49 | 13,07 | 18,49 | 13,07 | 18,49 | 13,07 | 18,49 | 13,07 |
| $10,0 \times 360$ | 140 | 140 | 18,69 | 13,21 | 18,69 | 13,21 | 18,69 | 13,21 | 18,69 | 13,21 |
| $10,0 \times 400$ | 160 | 140 | 20,04 | 14,17 | 20,04 | 14,17 | 20,04 | 14,17 | 20,04 | 14,17 |
| $10,0 \times 450$ | 160 | 180 | 25,81 | 18,25 | 25,81 | 18,25 | 25,81 | 18,25 | 25,81 | 18,25 |
| 10,0 $\times 500$ | 180 | 200 | 28,31 | 20,02 | 28,31 | 20,02 | 28,31 | 20,02 | 28,31 | 20,02 |
| $10,0 \times 550$ | 200 | 200 | 30,82 | 21,79 | 30,82 | 21,79 | 30,82 | 21,79 | 30,82 | 21,79 |
| $10,0 \times 600$ | 220 | 220 | 33,00 | 23,33 | 33,00 | 23,33 | 33,00 | 23,33 | 33,00 | 23,33 |

Calculation according to $\mathrm{EA}-11 / 0024$. Wood density $\rho_{\mathrm{k}}=380 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
a) The characteristic values of the load-bearing capacity Rk cannot be treated as equivalent to the max. possible load (the max. force). Characteristic values of the load-bearing capacity Rks should be reduced to dimensioning values

Rd with regard to the usage class and class of the load duration: $R_{d}=R_{k} \cdot k_{m o d} / \gamma M$. The dimensioning values of the load-bearing capacity $R d s$ should be contrasted with the dimensioning values of the loads (Rd $\left.\geq E_{d}\right)$.
Example:
Characterisic value for constant load (dead weight) $G_{k}=2,00 \mathrm{kN}$ and variable load (e. g. snow load) $Q_{k}=3,00 \mathrm{kN}$. $\mathrm{kmod}^{2}=0,9 \cdot \gamma_{\mathrm{M}}=1,3$.
$\rightarrow$ Dimensioning value of the lood $\mathrm{E}_{\mathrm{d}}=2,00 \cdot 1,35+3,00 \cdot 1,5=7,20 \mathrm{kN}$.
The load-bearing capacity of the joint is therefore considered to have been demonstrated if $\mathrm{R}_{\mathrm{d}} \geq \mathrm{E}_{\mathrm{d}} \rightarrow \min \mathrm{R}_{\mathrm{k}}=\mathrm{R}_{\mathrm{d}} \cdot \gamma \mathrm{M} / \mathrm{kmod}$
i.e. the characteristic minimum value is calculated based on: $\min \mathrm{Rk}=\mathrm{Rd}_{\mathrm{d}} \cdot \gamma \mathrm{M} / \mathrm{kmod} \rightarrow \mathrm{R}_{\mathrm{k}}=7,20 \mathrm{kN} \cdot 1,3 / 0,9=10,40 \mathrm{kN} \rightarrow$ comparison with table values.

Please note: These are planning aids. Projects must only be calculated by authorised persons.
Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by authorised
persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

## Eurotec

## KONSTRUX ST WITH COUNTERSUNK HEAD AND DRILL POINT

6,5 TO 10,0 MM: TIMBER-TIMBER JOINTS

| Dimensions |  |  | Extraction resistance | Shearing |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Charocterisicic value of the joint's loadbearing capacity Rax, , acc. to ETA-11/0024 | $\begin{aligned} & \xrightarrow{V\left(\alpha=0^{\circ}\right)} \\ & V_{\left(\alpha=0^{\circ}\right)} \\ & \stackrel{V\left(\alpha=90^{\circ}\right)}{ } \\ & V\left(\alpha=90^{\circ}\right) \end{aligned}$ |  | $\mathrm{V}\left(\mathrm{a}=0^{\circ}\right)$ <br> $V\left(\alpha=90^{\circ}\right)$ <br> $\mathrm{V}\left(\mathrm{a}=90^{\circ}\right)$ <br> $V\left(\alpha=0^{\circ}\right)$ <br> of the join's <br> cr. to ETA-11/002 | B |
| dl xL [mm] | A [mm] | B [mm] |  | $\mathrm{Rk}^{\text {a) }} \cdot[\mathrm{kNW}]$ | $\mathrm{R}^{\text {a) }}$ - [kN] | $\mathrm{Rk}^{\text {a) }}$-[kN] | $\mathrm{Rk}^{\text {a) }}$ - [kN] |
|  |  |  |  | $\alpha=0^{\circ}$ | $\alpha=90^{\circ}$ | $\begin{aligned} \alpha_{A} & =0^{\circ} \\ \alpha, & =90^{\circ} \end{aligned}$ | $\begin{aligned} & \alpha A=90^{\circ} \\ & \alpha B=0^{\circ} \end{aligned}$ |
| 6,5 $\times 120$ | 60 | 80 | 4,75 | 3,93 | 3,47 | 3,93 | 3,47 |
| $6,5 \times 140$ | 80 | 80 | 4,75 | 3,93 | 3,47 | 3,47 | 3,93 |
| 8,0×95 | 40 | 60 | 3,08 | 4,61 | 3,57 | 4,61 | 3,57 |
| $8,0 \times 125$ | 60 | 80 | 4,61 | 5,05 | 4,37 | 5,05 | 4,37 |
| $8,0 \times 155$ | 80 | 80 | 7,11 | 5,67 | 4,99 | 4,99 | 5,67 |
| 8,0x 195 | 100 | 100 | 9,01 | 6,15 | 5,46 | 5,46 | 6,15 |
| 8,0x 220 | 120 | 120 | 9,48 | 6,27 | 5,58 | 5,58 | 6,27 |
| 8,0x 245 | 120 | 140 | 11,38 | 6,74 | 6,06 | 6,74 | 6,06 |
| 8, $\times 270$ | 140 | 140 | 12,33 | 6,98 | 6,29 | 6,29 | 6,98 |
| $8,0 \times 295$ | 140 | 160 | 13,28 | 7,21 | 6,42 | 7,21 | 6,42 |
| 8,0 $\times 330$ | 160 | 180 | 15,17 | 7,69 | 6,42 | 1,69 | 6,42 |
| 8,0x 375 | 180 | 200 | 17,07 | 7,79 | 6,42 | 7,79 | 6,42 |
| $8,0 \times 400$ | 200 | 220 | 18,97 | 7,79 | 6,42 | 7,79 | 6,42 |
| 8,0x 430 | 220 | 220 | 19,92 | 1,79 | 6,42 | 6,42 | 1,79 |
| $8,0 \times 480$ | 240 | 260 | 22,76 | 7,79 | 6,42 | 7,79 | 6,42 |
| $10,0 \times 125$ | 60 | 80 | 6,92 | 7,18 | 6,18 | 7,18 | 6,18 |
| $10,0 \times 155$ | 80 | 80 | 8,65 | 1,61 | 6,61 | 6,61 | 1,61 |
| 10,0 195 | 100 | 100 | 10,96 | 8,19 | 7,19 | 7,19 | 8,19 |
| 10,0 $\times 220$ | 120 | 120 | 11,53 | 8,33 | 1,33 | 1,33 | 8,33 |
| 10,0 245 | 120 | 140 | 13,84 | 8,91 | 1,91 | 8,91 | 1,91 |
| 10,0 270 | 140 | 140 | 14,99 | 9,20 | 8,20 | 8,20 | 9,20 |
| $10,0 \times 300$ | 160 | 160 | 16,15 | 9,48 | 8,48 | 8,48 | 9,48 |
| $10,0 \times 330$ | 160 | 180 | 18,46 | 10,06 | 8,90 | 10,06 | 8,90 |
| $10,0 \times 360$ | 180 | 200 | 20,76 | 10,64 | 8,90 | 10,64 | 8,90 |
| 10,0x 400 | 200 | 220 | 23,07 | 10,89 | 8,90 | 10,89 | 8,90 |
| 10,0x 450 | 220 | 240 | 25,38 | 10,89 | 8,90 | 10,89 | 8,90 |
| 10,0x 500 | 240 | 280 | 27,68 | 10,89 | 8,90 | 10,89 | 8,90 |
| $10,0 \times 550$ | 260 | 300 | 29,99 | 10,89 | 8,90 | 10,89 | 8,90 |
| $10,0 \times 600$ | 300 | 320 | 33,00 | 10,89 | 8,90 | 10,89 | 8,90 |


All values are calculcted minimum values and are subject to typographical and pirining errors.



## Example:



Plecse note: These cre planning aids. Projects must only be calculcted by authoised persons.

## KONSTRUX ST WITH COUNTERSUNK HEAD AND DRILL POINT 8,0 AND 10,0 MM: TIMBER-TMBER JOINTS

Dimensions
Tension connection


Characterisicic value of the joint's loadbearing capacity Rax,k bzw. Rk acc. to EAA-11/0024

| dl xL [mm] | A [mm] | $B[\mathrm{~mm}]$ | $\mathrm{Rax}_{\text {a }}\left(\mathrm{k}{ }^{\text {a) }}\right.$. [kN] | $\mathrm{Rk}^{(0)}$ - [kN] | ${\mathrm{Rax}, 1^{\text {a }}}^{\text {a) }}$ [kN] | $\mathrm{Rk}^{\text {a) }}$-[kN] | $R_{a x, 1}{ }^{\text {a) }}$-[kN] | $\mathrm{Rk}^{\text {a) }}$-[kN] | $\mathrm{R}_{\mathrm{ax}, \mathrm{k}} \mathrm{l}^{\text {a) }}$ [ [kN] | Rk ${ }^{\text {a) }}$-[kN] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\alpha=45^{\circ}$ |  | $\begin{aligned} & \alpha A=90^{\circ} \\ & \alpha B=45^{\circ} \end{aligned}$ |  | $\begin{aligned} & \alpha_{A}=90^{\circ} \\ & \alpha_{B}=90^{\circ} \end{aligned}$ |  | $\begin{aligned} & \alpha A=45^{\circ} \\ & \alpha, B=90^{\circ} \end{aligned}$ |  |
| 8, $\times 155$ | 60 | 60 | 6,65 | 4,70 | 6,65 | 4,70 | 6,65 | 4,70 | 6,65 | 4,70 |
| 8, $\times 195$ | 80 | 80 | 7,76 | 5,49 | 7,76 | 5,49 | 7,76 | 5,49 | 7,76 | 5,49 |
| 8, $\times 220$ | 80 | 100 | 10,13 | 7,17 | 10,13 | 7,17 | 10,13 | 7,17 | 10,13 | 7,17 |
| 8, $\times 245$ | 100 | 100 | 9,82 | 6,95 | 9,82 | 6,95 | 9,82 | 6,95 | 9,82 | 6,95 |
| 8, $\times 270$ | 100 | 120 | 12,19 | 8,62 | 12,19 | 8,62 | 12,19 | 8,62 | 12,19 | 8,62 |
| 8, $\times 295$ | 120 | 100 | 11,88 | 8,40 | 11,88 | 8,40 | 11,88 | 8,40 | 11,88 | 8,40 |
| 8, $\times 330$ | 120 | 140 | 15,20 | 10,75 | 15,20 | 10,75 | 15,20 | 10,75 | 15,20 | 10,75 |
| 8, $\times 375$ | 140 | 140 | 16,79 | 11,87 | 16,79 | 11,87 | 16,79 | 11,87 | 16,79 | 11,87 |
| 8,0 400 | 160 | 140 | 16,48 | 11,65 | 16,48 | 11,65 | 16,48 | 11,65 | 16,48 | 11,65 |
| 8, x 430 | 160 | 160 | 19,32 | 13,66 | 19,32 | 13,66 | 19,32 | 13,66 | 19,32 | 13,66 |
| 8,0 480 | 180 | 180 | 21,38 | 15,12 | 21,38 | 15,12 | 21,38 | 15,12 | 21,38 | 15,12 |
| 10,0x 220 | 80 | 100 | 12,33 | 8,72 | 12,33 | 8,72 | 12,33 | 8,72 | 12,33 | 8,72 |
| $10,0 \times 245$ | 100 | 100 | 11,95 | 8,45 | 11,95 | 8,45 | 11,95 | 8,45 | 11,95 | 8,45 |
| $10,0 \times 270$ | 100 | 120 | 14,83 | 10,49 | 14,83 | 10,49 | 14,83 | 10,49 | 14,83 | 10,49 |
| 10,0 300 | 120 | 120 | 15,03 | 10,63 | 15,03 | 10,63 | 15,03 | 10,63 | 15,03 | 10,63 |
| $10,0 \times 330$ | 120 | 140 | 18,49 | 13,07 | 18,49 | 13,07 | 18,49 | 13,07 | 18,49 | 13,07 |
| 10,0 $\times 360$ | 140 | 140 | 18,69 | 13,21 | 18,69 | 13,21 | 18,69 | 13,21 | 18,69 | 13,21 |
| $10,0 \times 400$ | 160 | 140 | 20,04 | 14,17 | 20,04 | 14,17 | 20,04 | 14,17 | 20,04 | 14,17 |
| $10,0 \times 450$ | 160 | 180 | 25,81 | 18,25 | 25,81 | 18,25 | 25,81 | 18,25 | 25,81 | 18,25 |
| 10,0x500 | 180 | 200 | 28,31 | 20,02 | 28,31 | 20,02 | 28,31 | 20,02 | 28,31 | 20,02 |
| 10,0 $\times 550$ | 200 | 200 | 30,82 | 21,79 | 30,82 | 21,79 | 30,82 | 21,79 | 30,82 | 21,79 |
| $10,0 \times 600$ | 220 | 220 | 33,00 | 23,33 | 33,00 | 23,33 | 33,00 | 23,33 | 33,00 | 23,33 |

Calculation according to EAA- $11 / 0024$. Wood density $\mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
a) The characteristic values of the load-bearing capacity Rk cannot be treated as equivalent to the max. possible lood (the max. force). Characterisicic values of the lood-bearing capacity Rk should be reduced to dimensioning values Rd
with regard to the usage class and dass of the load duration: $R_{d}=R_{k} \cdot k_{m o d} / \gamma \mathrm{M}$. The dimensioning values of the lood-bearing capacity $\mathrm{Rd}_{\mathrm{d}}$ should be contrasted with the dimensioning values of the loads ( $\mathrm{R}_{\mathrm{d}} \geq \mathrm{Ed}$ ).
Example:
Characterisic value for constant lood (dead weight) $G_{k}=2,00 \mathrm{kN}$ and variable lood (e. g. snow load) $Q_{k}=3,00 \mathrm{kN} . \mathrm{kmod}^{2}=0,9 \cdot \gamma_{\mathrm{M}}=1,3$.
$\rightarrow$ Dimensioning value of the load $\mathrm{E} d=2,00 \cdot 1,35+3,00 \cdot 1,5=7,20 \mathrm{kN}$.
The lood-bearing capacity of the joint is therefore considered to have been demonstrated if $\mathrm{R}_{\mathrm{d}} \geq \mathrm{Ed} . \rightarrow \min \mathrm{Rk}_{\mathrm{k}}=\mathrm{R}_{d} \cdot \gamma \mathrm{M} / \mathrm{kmod}$
i.e. the characterisicic minimum value is calculated based on: $\min \mathrm{R}_{\mathrm{k}}=\mathrm{Rd}_{\mathrm{d}} \cdot \gamma_{\mathrm{M}} / \mathrm{kmod}_{\operatorname{mol}} \rightarrow \mathrm{R}_{k}=7,20 \mathrm{kN} \cdot 1,3 / 0,9=10,40 \mathrm{kN} \rightarrow$ comparison with table values.

Please note: These are planning aids. Projects must only be calculated by authorised persons.

## Gurotec

## KONSTRUX WITH COUNTERSUNK HEAD AND DRILL POINT OR AG TIP 11,3 MM: TIMBER-TIMBER CONNECTION

| Dimensions |  |  | Extraction resistance | Shearing |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Characterisicic value of the joint's loadbearing capacity Rax,k acc. to ETA-11/0024 | $\xrightarrow[V\left(\alpha=0^{\circ}\right)]{V\left(\alpha=0^{\circ}\right)}$ $V\left(\alpha=90^{\circ}\right)$ $V\left(\alpha=90^{\circ}\right)$ | A <br> Charocter <br> loadbearing ca | $V\left(\alpha=90^{\circ}\right)$ $V\left(\alpha=90^{\circ}\right)$ $V_{\left(\alpha=0^{\circ}\right)}$ <br> of the join's c. to ETA-11/0024 |  |
| dl x L [mm $]$ | A [mm] | $B[\mathrm{~mm}$ ] | ${\mathrm{Rax}, 1^{\text {a }}}^{\text {a) }}$ [ [kN] | $R_{k}{ }^{\text {a) }} \cdot[\mathrm{kN}]$ | $\mathrm{Rk}^{\text {a) }}$-[kN] | $\mathrm{R}^{(1)}$ ) [ [kN] | $\mathrm{Rk}^{\text {a) }}$. [kN] |
|  |  |  |  | $\alpha=0^{\circ}$ | $\alpha=90^{\circ}$ | $\begin{aligned} \alpha_{A} & =0^{\circ} \\ \alpha_{B} & =90^{\circ} \end{aligned}$ | $\begin{aligned} & \alpha A=90^{\circ} \\ & \alpha B=0^{\circ} \end{aligned}$ |
| 11,3x 300 | 160 | 160 | 18,25 | 12,17 | 10,73 | 10,73 | 12,17 |
| $11,3 \times 340$ | 180 | 180 | 20,85 | 12,82 | 11,38 | 11,38 | 12,82 |
| 11,3x 380 | 200 | 200 | 23,46 | 13,47 | 12,03 | 12,03 | 13,47 |
| 11,3x420 | 220 | 220 | 26,07 | 14,12 | 12,34 | 12,34 | 14,12 |
| $11,3 \times 460$ | 240 | 240 | 26,67 | 14,77 | 12,34 | 12,34 | 14,77 |
| 11,3x500 | 260 | 260 | 31,28 | 15,21 | 12,34 | 12,34 | 15,21 |
| 11,3x540 | 280 | 280 | 33,89 | 15,21 | 12,34 | 12,34 | 15,21 |
| 11,3x580 | 300 | 300 | 36,49 | 15,21 | 12,34 | 12,34 | 15,21 |
| 11,3×620 | 320 | 320 | 39,10 | 15,21 | 12,34 | 12,34 | 15,21 |
| $11,3 \times 660$ | 340 | 340 | 41,71 | 15,21 | 12,34 | 12,34 | 15,21 |
| 11,3x700 | 360 | 360 | 44,32 | 15,21 | 12,34 | 12,34 | 15,21 |
| 11,3x750 | 380 | 380 | 48,23 | 15,21 | 12,34 | 12,34 | 15,21 |
| 11,3x800 | 400 | 420 | 50,00 | 15,21 | 12,34 | 15,21 | 12,34 |
| 11,3×900 | 460 | 460 | 50,00 | 15,21 | 12,34 | 12,34 | 15,21 |
| $11,3 \times 1000$ | 500 | 520 | 50,0 | 15,21 | 12,34 | 15,21 | 12,34 |

Calculation according to $\mathrm{FTA}-\mathrm{Il} / \mathrm{O} 224$. Wood density $\mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical valves provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
a) The characteristic values of the load-bearing capacity Rk cannot be treated os equivalent to the max. possible load (the max. force). Characterisicic values of the load-bearing capacity Rk should be reduced to dimensioning valves Rd
with regard to the usage class and class of the load duration: $R_{d}=R_{k} \cdot k_{m o d} / \gamma m$. The dimensioning values of the load-bearing capacity $R_{d}$ should be contrassed with the dimensioning values of the loads ( $\left.R_{d} \geq E_{d}\right)$.
Example:
Characterisic value for constant load (dead weight) $G_{k}=2,00 \mathrm{kN}$ and variable load (e. g. snow lood) $Q_{k}=3,00 \mathrm{kN} . \mathrm{kmod}^{2}=0,9 \cdot \gamma_{\mathrm{M}}=1,3$.
$\rightarrow$ Dimensioning value of the load $\mathrm{Ed}=2,00 \cdot 1,35+3,00 \cdot 1,5=7,20 \mathrm{kN}$.
The load-bearing capacity of the joint is therefore considered to have been demonstrated if $R_{d} \geq E_{d} . \rightarrow \min R_{k}=R_{d} \cdot \gamma M / k_{m o d}$
i.e. the characterissic minimum value is calculated based on: $\min \mathrm{R}_{k}=\mathrm{R}_{\mathrm{d}} \cdot \gamma_{\mathrm{M}} / \mathrm{kmod}_{\bmod } \rightarrow \mathrm{R}_{k}=7,20 \mathrm{kN} \cdot 1,3 / 0,9=10,40 \mathrm{kN} \rightarrow$ comparison with table values.

Please note: These are planning aids. Projects must only be calculated by authorised persons.

## KONSTRUX WITH COUNTERSUNK HEAD AND DRILL POINT OR AG TIP 11,3 MM: TIMBER-TIMBER CONNECTION

| Dimensions |  |  | Tension connection |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Characterisicic value of the joint's lood-bearing capacity Rax, or Rk occ. to ETA-11/0024 |  |  |  |  |  |  |  |
| dl $\mathrm{xL}[\mathrm{mm}]$ | A [mm] | $B[\mathrm{~mm}]$ | $\mathrm{Rax}_{\text {a }} \mathrm{k}^{\text {a) }}$-[kN] | $\mathrm{Rk}^{\text {a) }}$-[kN] | $\mathrm{Rax}_{\text {a }}, \mathrm{k}^{\mathrm{a}}$. [kN] | $\mathrm{Rk}^{\text {a) }}$. [kN] | ${\mathrm{Rax}, \mathrm{k}^{\text {a }}}^{\text {) }}$ [ KN$]$ | $\mathrm{R}_{\mathrm{k}}{ }^{\text {) }}$. [kN] | $\mathrm{Raxax}^{(1)} \mathrm{k}^{\mathrm{a}} .[\mathrm{kN}]$ | $\mathrm{Rk}^{\text {a) }} \cdot[\mathrm{kN}]$ |
|  |  |  | $\alpha=45^{\circ}$ |  | $\begin{aligned} & \alpha A=90^{\circ} \\ & \alpha_{B}=45^{\circ} \end{aligned}$ |  | $\begin{aligned} & \alpha_{A}=90^{\circ} \\ & \alpha B=90^{\circ} \end{aligned}$ |  | $\begin{aligned} & \alpha A=45^{\circ} \\ & \alpha B=90^{\circ} \end{aligned}$ |  |
| 11,3x300 | 120 | 120 | 16,98 | 12,01 | 16,98 | 12,01 | 16,98 | 12,01 | 16,98 | 12,01 |
| 11,3x340 | 140 | 120 | 18,51 | 13,09 | 18,51 | 13,09 | 18,51 | 13,09 | 18,51 | 13,09 |
| 11,3x380 | 140 | 140 | 23,72 | 16,77 | 23,72 | 16,77 | 23,72 | 16,77 | 23,72 | 16,77 |
| 11,3x420 | 160 | 160 | 25,25 | 17,85 | 25,25 | 17,85 | 25,25 | 17,85 | 25,25 | 17,85 |
| 11,3x460 | 180 | 160 | 26,78 | 18,93 | 26,78 | 18,93 | 26,78 | 18,93 | 26,78 | 18,93 |
| 11,3x500 | 180 | 200 | 31,99 | 22,62 | 31,99 | 22,62 | 31,99 | 22,62 | 31,99 | 22,62 |
| 11,3x540 | 200 | 200 | 33,52 | 23,70 | 33,52 | 23,70 | 33,52 | 23,70 | 33,52 | 23,70 |
| 11,3x580 | 220 | 220 | 35,04 | 24,78 | 35,04 | 24,78 | 35,04 | 24,78 | 35,04 | 24,78 |
| 11,3x620 | 220 | 240 | 40,26 | 28,47 | 40,26 | 28,47 | 40,26 | 28,47 | 40,26 | 28,47 |
| 11,3x660 | 240 | 240 | 41,79 | 29,55 | 41,79 | 29,55 | 41,79 | 29,55 | 41,79 | 29,55 |
| 11,3x700 | 260 | 260 | 43,31 | 30,63 | 43,31 | 30,63 | 43,31 | 30,63 | 43,31 | 30,63 |
| 11,3x750 | 280 | 280 | 46,14 | 32,63 | 46,14 | 32,63 | 46,14 | 32,63 | 46,14 | 32,63 |
| 11,3x800 | 300 | 280 | 48,97 | 34,63 | 48,97 | 34,63 | 48,97 | 34,63 | 48,97 | 34,63 |
| $11,3 \times 900$ | 320 | 340 | 50,00 | 35,36 | 50,0 | 35,36 | 50,00 | 35,36 | 50,00 | 35,36 |
| 11,3x 1000 | 360 | 360 | 50,00 | 35,36 | 50,00 | 35,36 | 50,00 | 35,36 | 50,00 | 35,36 |

Calculation according to $\mathrm{ETA}-11 / 0024$. Wood density $\rho \mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculcted minimum values and are subject to typographical and printing errors.
a) The characteristic values of the load-bearing capacity Rk cannot be treated as equivalent to the max. possible load (the max. force). Characterisici values of the load-bearing capacity Rk should be reduced to dimensioning values Rd with regard to the usage class and class of the load duration: $\mathrm{Rd}_{\mathrm{d}}=\mathrm{Rk}_{\mathrm{k}} \cdot \mathrm{kmod}_{\mathrm{m}} / \gamma \mathrm{M}$. The dimensioning values of the load-bearing capacity Rd should be contrasted with the dimensioning values of the loads $\left(\mathrm{Rd}_{d} \geq\right.$ Ed).

## Example:

Characterisic value for constant load (dead weight) $G_{k}=2,00 \mathrm{kN}$ and variable load (e. g. snow lood) $\mathrm{Q}_{\mathrm{k}}=3,00 \mathrm{kN}$. $\mathrm{kmod}_{\mathrm{m}}=0,9 . \gamma_{\mathrm{M}}=1,3$.
$\rightarrow$ Dimensioning value of the load $\mathrm{Ed}=2,00 \cdot 1,35+3,00 \cdot 1,5=7,20 \mathrm{kN}$.
The load-bearing capacity of the joint is therefore considered to have been demonssrated if $\mathrm{R}_{\mathrm{d}} \geq \mathrm{Ed} . \rightarrow \min \mathrm{R}_{\mathrm{k}}=\mathrm{R}_{d} \cdot \gamma \mathrm{M} / \mathrm{kmod}$
i.e. the characterisicic minimum value is calculated based on: $\min \mathrm{R}_{k}=\mathrm{R}_{\mathrm{d}} \cdot \gamma_{\mathrm{M}} / \mathrm{k}_{\mathrm{mod}} \rightarrow \mathrm{R}_{\mathrm{k}}=7,20 \mathrm{kN} \cdot 1,3 / 0,9=10,40 \mathrm{kN} \rightarrow$ comparison with table values.

Please note: These are planning aids. Projects must only be calculated by authorised persons.

## KONSTRUX ST WITH COUNTERSUNK HEAD AND DRILL POINT 6,5 TO 10,0 MM: STEEL-TIMBER JOINTS

| Dimensions |  |  |  | Extraction resistance | Tension connection |  |  |  | Shearing |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  <br> Charactersisic value of the join's looctbearing capaciy Rax, a acc. 10 EAA- $\mathrm{II} / 0024$ |  |  | $\qquad$ <br> $\operatorname{Rk}\left(\alpha=90^{\circ}\right)$ <br> of the join's loadbe Rk acc. to ETA-II/O | ng |  | 3 t <br> ve of the joint's <br> Rk acc. toEIA-11/002 |
| $\mathrm{dl} \mathrm{xL}[\mathrm{mm}]$ | t[mm] | $B[\mathrm{~mm}]$ | $\mathrm{B} 45^{\circ}$ [mm] | $\mathrm{R}_{\mathrm{ax}, 1} \mathrm{l}^{\text {a) }}$-[kN] | $\mathrm{R}_{\mathrm{ax}, \mathrm{k}} \mathrm{K}^{\text {a) }} \cdot[\mathrm{KkN}]$ | $\mathrm{R}_{\mathrm{ax}, 1} \mathrm{l}^{\text {a) }}$-[kN] | $\mathrm{R}_{\mathrm{k}}{ }^{\text {a) }} \cdot[\mathrm{kN}]$ | $\mathrm{Rk}^{\text {a) }}$-[kN] | Rk ${ }^{\text {a) }}$. [kN] | $\mathrm{Rk}^{\text {a) }}$-[kN] |
|  |  |  |  |  | $\alpha=45^{\circ}$ | $\alpha=90^{\circ}$ | $\alpha=45^{\circ}$ | $\alpha=90^{\circ}$ | $\alpha=0^{\circ}$ | $\alpha=90^{\circ}$ |
| 6,5x 80 | 15 | 80 | 60 | 5,14 | 4,65 | 4,65 | 3,29 | 3,29 | 4,17 | 3,52 |
| 6,5x 100 | 15 | 100 | 80 | 6,73 | 6,24 | 6,24 | 4,41 | 4,41 | 4,17 | 3,52 |
| 6,5x 120 | 15 | 120 | 80 | 8,31 | 7,82 | 1,82 | 5,53 | 5,53 | 4,17 | 3,52 |
| 6,5×140 | 15 | 140 | 100 | 9,89 | 9,40 | 9,40 | 6,65 | 6,65 | 4,17 | 3,52 |
| 8,0x95 | 15 | 100 | 80 | 1,59 | 7,00 | 1,00 | 4,95 | 4,95 | 6,18 | 5,22 |
| 8, $\times 125$ | 15 | 120 | 100 | 10,43 | 9,84 | 9,84 | 6,96 | 6,96 | 6,18 | 5,22 |
| $8,0 \times 155$ | 15 | 160 | 120 | 13,28 | 12,69 | 12,69 | 8,97 | 8,97 | 6,18 | 5,22 |
| $8,8 \times 195$ | 15 | 200 | 140 | 17,07 | 16,48 | 16,48 | 11,65 | 11,65 | 6,18 | 5,22 |
| 8,0 220 | 15 | 220 | 160 | 19,44 | 18,85 | 18,85 | 13,33 | 13,33 | 6,18 | 5,22 |
| 8, $\times 245$ | 15 | 240 | 180 | 21,81 | 21,22 | 21,22 | 15,01 | 15,01 | 6,18 | 5,22 |
| 8,0 270 | 15 | 280 | 200 | 24,18 | 23,59 | 23,59 | 16,68 | 16,68 | 6,18 | 5,22 |
| 8,0x 295 | 15 | 300 | 220 | 25,00 | 25,00 | 25,00 | 17,68 | 17,68 | 6,18 | 5,22 |
| 8,0x 330 | 15 | 340 | 240 | 25,00 | 25,00 | 25,00 | 17,68 | 17,68 | 6,18 | 5,22 |
| 8,0x 375 | 15 | 380 | 280 | 25,00 | 25,00 | 25,00 | 17,68 | 17,68 | 6,18 | 5,22 |
| 8,0x 400 | 15 | 400 | 280 | 25,00 | 25,00 | 25,00 | 17,68 | 17,68 | 6,18 | 5,22 |
| $8,0 \times 430$ | 15 | 440 | 300 | 25,00 | 25,00 | 25,00 | 17,68 | 17,68 | 6,18 | 5,22 |
| $8,0 \times 480$ | 15 | 480 | 340 | 25,00 | 25,00 | 25,00 | 17,68 | 17,68 | 6,18 | 5,22 |
| $10,0 \times 125$ | 15 | 120 | 100 | 12,69 | 11,97 | 11,97 | 8,46 | 8,46 | 8,72 | 1,30 |
| 10,0 $\times 155$ | 15 | 160 | 120 | 16,15 | 15,43 | 15,43 | 10,91 | 10,91 | 8,72 | 1,30 |
| 10,0 $\times 195$ | 15 | 200 | 140 | 20,76 | 20,05 | 20,05 | 14,17 | 14,17 | 8,72 | 1,30 |
| $10,0 \times 220$ | 15 | 220 | 160 | 23,65 | 22,93 | 22,93 | 16,21 | 16,21 | 8,72 | 1,30 |
| 10,0 245 | 15 | 240 | 180 | 26,53 | 25,81 | 25,81 | 18,25 | 18,25 | 8,72 | 1,30 |
| 10,0 270 | 15 | 280 | 200 | 29,41 | 28,70 | 28,70 | 20,29 | 20,29 | 8,72 | 1,30 |
| 10,0x 300 | 15 | 300 | 220 | 32,87 | 32,16 | 32,16 | 22,74 | 22,74 | 8,72 | 1,30 |
| 10,0×330 | 15 | 340 | 240 | 33,00 | 33,00 | 33,00 | 23,33 | 23,33 | 8,72 | 1,30 |
| 10,0x 360 | 15 | 360 | 260 | 33,00 | 33,00 | 33,00 | 23,33 | 23,33 | 8,72 | 1,30 |
| 10,0x400 | 15 | 400 | 280 | 33,00 | 33,00 | 33,00 | 23,33 | 23,33 | 8,72 | 1,30 |
| $10,0 \times 450$ | 15 | 460 | 320 | 33,00 | 33,00 | 33,00 | 23,33 | 23,33 | 8,72 | 1,30 |
| 10,0x 500 | 15 | 500 | 360 | 33,00 | 33,00 | 33,00 | 23,33 | 23,33 | 8,72 | 1,30 |
| 10,0x 550 | 15 | 560 | 400 | 33,00 | 33,00 | 33,00 | 23,33 | 23,33 | 8,72 | 1,30 |
| $10,0 \times 600$ | 15 | 600 | 420 | 33,00 | 33,00 | 33,00 | 23,33 | 23,33 | 8,72 | 1,30 |

Calculation according to ETA-11/0024. Wood density $\mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
a) The characteristic values of the load-bearing capacity Rk cannot be treated as equivalent to the max. possible load (the max. force). Characterisic values of the load-bearing capacity Rk should be reduced to dimensioning values Rd
with regard to the usage class and class of the load duration: $\operatorname{Rd}=\mathrm{Rk}_{\mathrm{k}} \cdot \mathrm{kmod}^{2} / \gamma \mathrm{M}$. The dimensioning values of the load-bearing capacity $\operatorname{Rd}$ should be contrassed with the dimensioning values of the loads ( $\left.\mathrm{R}_{d} \geq \mathrm{Ed}\right)$.
Example:
Characterisicic value for constant load (dead weight) $G_{k}=2,00 \mathrm{kN}$ and variable load (e. g. snow load) $\mathrm{Q}_{\mathrm{k}}=3,00 \mathrm{kN}$. $\mathrm{kmod}=0,9 \cdot \gamma \mathrm{M}=1,3 . \rightarrow$ Dimensioning valve of the load $\mathrm{E} d=2,00 \cdot 1,35+3,00 \cdot 1,5=7,20 \mathrm{kN}$. The load-bearing capacity of the joint is therefore considered to have been demonstrated if $\mathrm{R}_{\mathrm{d}} \geq \mathrm{E}_{\mathrm{d}} \rightarrow \min \mathrm{R}_{\mathrm{k}}=\mathrm{R}_{\mathrm{d}} \cdot \gamma_{\mathrm{M}} / \mathrm{kmod}_{\text {mi.e. }}$. the characterisicic minimum value is calculated based on: min $\mathrm{R}_{\mathrm{k}}=\mathrm{R}_{\mathrm{d}} \cdot \gamma_{\mathrm{M}} / \mathrm{kmod}_{\bmod } \rightarrow \mathrm{R}_{\mathrm{k}}=7,20 \mathrm{kN} \cdot 1,3 / 0,9=10,40 \mathrm{kN} \rightarrow$ comparison with table values.
Please note: These are planning vids. Projects must only be calculated by authorised persons.

## KONSTRUX WITH COUNTERSUNK HEAD AND DRILL POINT OR AG TIP 11,3 MM: STEEL-TMBER CONNECTION

| Dimensions |  |  |  | Extraction resistance | Tension connection |  |  |  | Shearing |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  <br> Charactersisic value of the join's loocthearing capacity Rax, , acc. 10 ETA-II/0024 |  | Characterersici value o capacity Rax,k bzw. | the jinit's loadberim Rk acc. to EA-11/002 | $\stackrel{v}{-}$ |  | $\square$ <br> B <br> ve of the join's Rk acc. to EA-11/0024 |
| $\mathrm{dl} \mathrm{xL}[\mathrm{mm}]$ | t[mm] | B [mm] | $B 45^{\circ}$ [mm] | $\mathrm{R}_{\text {ax, }},{ }^{\text {a) }}$. [KN] | $\left.\mathrm{Rax}_{\mathrm{ax}} \mathrm{k}^{\mathrm{a}}\right) \cdot[\mathrm{KN}]$ | $R_{\text {ax, }} \mathrm{l}^{\text {a) }}$. [kN] | $\mathrm{Rk}^{\text {a) }}$. [kN] | $\mathrm{Rk}^{\text {a) }}$-[kN] | $\mathrm{R}^{(0)}$. [kN] | Rk ${ }^{\text {a) }}$. [kN] |
|  |  |  |  |  | $\alpha=45^{\circ}$ | $\alpha=90^{\circ}$ | $\alpha=45^{\circ}$ | $\alpha=90^{\circ}$ | $\alpha=0^{\circ}$ | $\alpha=90^{\circ}$ |
| 11,3x300 | 20 | 300 | 220 | 36,49 | 35,42 | 35,42 | 25,04 | 25,04 | 11,79 | 9,76 |
| $11,3 \times 340$ | 20 | 340 | 240 | 41,71 | 40,63 | 40,63 | 28,73 | 28,73 | 11,79 | 9,76 |
| 11,3x 380 | 20 | 380 | 260 | 46,92 | 45,84 | 45,84 | 32,42 | 32,42 | 11,79 | 9,76 |
| $11,3 \times 420$ | 20 | 420 | 300 | 50,0 | 50,0 | 50,0 | 35,36 | 35,36 | 11,79 | 9,76 |
| $11,3 \times 460$ | 20 | 460 | 320 | 50,00 | 50,00 | 50,00 | 35,36 | 35,36 | 11,79 | 9,76 |
| 11,3x500 | 20 | 500 | 360 | 50,0 | 50,00 | 50,00 | 35,36 | 35,36 | 11,79 | 9,76 |
| 11,3x540 | 20 | 540 | 380 | 50,0 | 50,0 | 50,0 | 35,36 | 35,36 | 11,79 | 9,76 |
| 11,3x580 | 20 | 580 | 420 | 50,0 | 50,0 | 50,0 | 35,36 | 35,36 | 11,79 | 9,76 |
| 11,3x620 | 20 | 620 | 440 | 50,0 | 50,00 | 50,0 | 35,36 | 35,36 | 11,79 | 9,76 |
| 11,3×660 | 20 | 660 | 460 | 50,0 | 50,0 | 50,00 | 35,36 | 35,36 | 11,79 | 9,76 |
| 11,3x700 | 20 | 700 | 500 | 50,00 | 50,00 | 50,00 | 35,36 | 35,36 | 11,79 | 9,76 |
| 11,3x750 | 20 | 740 | 540 | 50,00 | 50,00 | 50,0 | 35,36 | 35,36 | 11,79 | 9,76 |
| 11,3x800 | 20 | 800 | 560 | 50,00 | 50,00 | 50,00 | 35,36 | 35,36 | 11,79 | 9,76 |
| 11,3x900 | 20 | 900 | 640 | 50,00 | 50,0 | 50,0 | 35,36 | 35,36 | 11,79 | 9,76 |
| 11,3x 1000 | 20 | 1000 | 700 | 50,00 | 50,00 | 50,00 | 35,36 | 35,36 | 11,79 | 9,76 |

Calculation according to $E T-11 / 0024$. Wood density $\rho \mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All valves are calculated minimum values and are subject to typographical and printing errors.
a) The characterisicic values of the lood-bearing capacity Rk cannot be treated as equivalent to the max. possible lood (the max. force). Characteristic valves of the load-bearing capacity Rk should be reaveced to dimensioning values Rd
with regard to the usage class and dass of the lood duration: $R_{d}=R_{k} \cdot K_{\text {mod }} / \gamma$ M. The dimensioning values of the lood-bearing capacity $R_{d}$ should be contrasted with the dimensioning values of the loads ( $\left.R_{d} \geq E_{d}\right)$.
Example:
Characterisic value for constant load (dead weight) $G_{k}=2,00 \mathrm{kN}$ and variable lood (e. g. snow load) $Q_{k}=3,00 \mathrm{kN} . \mathrm{kmod}=0,9 \cdot \gamma \mathrm{M}=1,3$.
$\rightarrow$ Dimensioning value of the lood $\mathrm{Ed}=2,00 \cdot 1,35+3,00 \cdot 1,5=7,20 \mathrm{kN}$.
The load-bearing capacity of the joint is therefore considered to have been demonstrated if $\mathrm{Rd} \geq \mathrm{Ed}_{\mathrm{d}} \rightarrow \mathrm{min} \mathrm{Rk}=\mathrm{Rd}_{\mathrm{d}} \cdot \gamma \mathrm{M} / \mathrm{kmod}$
i.e. the characteristic minimum value is calculated based on: $\min \mathrm{R}_{\mathrm{k}}=\mathrm{R}_{d} \cdot \gamma_{\mathrm{M}} / \mathrm{k}_{\mathrm{mod}} \rightarrow \mathrm{R}_{\mathrm{k}}=7,20 \mathrm{kN} \cdot 1,3 / 0,9=10,40 \mathrm{kN} \rightarrow$ comparison with table values.

Please note: These are planning aids. Projects must only be calculated by outhorised persons.

## Eurotec

## KONSTRUX ST WITH CYLINDER HEAD AND DRILL POINT 6,5 MM: MAIN-SECONDARY BEAM JOINTS



Calculation according to EAA-11/0024. Wood density $\mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations. All values are calculated minimum values and are subject to typographical and printing errors.
a) The characterisic valves of the lood-bearing capacity Rk cannot be treated as equivalent to the max. possible load (the max. force). Characteristic values of the lood-bearing capacity Rk should be reduced to dimensioning values Rd with regard to the usage class and class of the load duration: $R_{d}=R_{k} \cdot k_{\text {mod }} / \gamma \mathrm{M}$. The dimensioning values of the load-bearing capacity $R d$ should be contrasted with the dimensioning values of the loads ( $\left.R_{d} \geq E_{d}\right)$.

Example:
Characterisic value for constant lood (dead weight) $G_{k}=2,00 \mathrm{kN}$ and variable load (e. g. snow lood) $Q_{k}=3,00 \mathrm{kN} . \mathrm{kmod}^{2}=0,9 \cdot \gamma_{\mathrm{M}}=1,3$.
$\rightarrow$ Dimensioning value of the load $\mathrm{Ed}=2,00 \cdot 1,35+3,00 \cdot 1,5=7,20 \mathrm{kN}$.
The load-bearing capacity of the joint is therefore considered to have been demonstrated if $\mathrm{Rd} \geq \mathrm{Ed} . \rightarrow \mathrm{min} \mathrm{Rk}=\mathrm{Rd} \cdot \gamma \mathrm{M} / \mathrm{kmod}$
i.e. the characteristic minimum value is calculated based on: $\min \mathrm{R}_{\mathrm{k}}=\mathrm{R}_{d} \cdot \gamma_{\mathrm{M}} / \mathrm{kmod} \rightarrow \mathrm{R}_{k}=7,20 \mathrm{kN} \cdot \mathrm{I}, 3 / 0,0=10,40 \mathrm{kN} \rightarrow$ comparison with table values.
b) estimated with an efficient quantity of pairs of screws: 0,9 .

Please note: These are planning aids. Projects must only be calculated by authorised persons.

## KONSTRUX ST WITH CYLINDER HEAD AND DRILL POINT 8,0 MM: MAIN-SECONDARY BEAM JOINTS

Dimensions Main/secondary beam connection
$\mathrm{a}_{2}=\min .40 \mathrm{~mm}, \mathrm{a}_{2},=\min .24 \mathrm{~mm}, \mathrm{k}=\min .12 \mathrm{~mm}$
Charactersisic value of the joint's loachbearing capacity $\mathrm{R}_{k}$ occ. to EA- $11 / 0024$

| $\mathrm{dl} \times \mathrm{L}$ [mm] | min . WSB [mm] | min. HSB [mm] | $\min$. WMB [mm] | min . $\mathrm{H} M \mathrm{BB}$ [mm] | $\mathrm{m}[\mathrm{mm}$ ] | $\beta^{\circ}$ | $\left.\left.R_{v, 1}, \mathrm{a}\right) \mathrm{b}\right)$-[kN] | Pair (n) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8,0x 245 | 80 | 200 | 100 | 200 | 87 | 45 | 16,43 | 1 |
|  | 100 |  |  |  |  |  | 30,66 | 2 |
|  | 140 |  |  |  |  |  | 44,16 | 3 |
|  | 180 |  |  |  |  |  | 57,21 | 4 |
| $8,0 \times 295$ | 80 | 220 | 120 | 220 | 104 | 45 | 17,44 | 1 |
|  | 100 |  |  |  |  |  | 32,55 | 2 |
|  | 140 |  |  |  |  |  | 46,88 | 3 |
|  | 180 |  |  |  |  |  | 60,74 | 4 |
| $8,0 \times 330$ | 80 | 260 | 140 | 260 | 117 | 45 | 17,44 | 1 |
|  | 100 |  |  |  |  |  | 32,55 | 2 |
|  | 140 |  |  |  |  |  | 46,88 | 3 |
|  | 180 |  |  |  |  |  | 60,74 | 4 |
| $8,0 \times 375$ | 80 | 280 | 160 | 280 | 133 | 45 | 17,44 | 1 |
|  | 100 |  |  |  |  |  | 32,55 | 2 |
|  | 140 |  |  |  |  |  | 46,88 | 3 |
|  | 180 |  |  |  |  |  | 60,74 | 4 |
| $8,0 \times 400$ | 80 | 300 | 160 | 300 | 141 | 45 | 17,44 | 1 |
|  | 100 |  |  |  |  |  | 32,55 | 2 |
|  | 140 |  |  |  |  |  | 46,88 | 3 |
|  | 180 |  |  |  |  |  | 60,74 | 4 |
| $8,0 \times 430$ | 80 | 320 | 180 | 320 | 152 | 45 | 17,44 | 1 |
|  | 100 |  |  |  |  |  | 32,55 | 2 |
|  | 140 |  |  |  |  |  | 46,88 | 3 |
|  | 180 |  |  |  |  |  | 60,74 | 4 |
| $8,0 \times 480$ | 80 | 360 | 180 | 360 | 170 | 45 | 17,44 | 1 |
|  | 100 |  |  |  |  |  | 32,55 | 2 |
|  | 140 |  |  |  |  |  | 46,88 | 3 |
|  | 180 |  |  |  |  |  | 60,74 | 4 |

Calculation according to $\mathrm{EA}-\mathrm{Il} / 0024$. Wood density $\rho \mathrm{k}=380 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should be viewed as subject to the assumpions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
a) The characterisisic valves of the load-bearing capacity Rk cannot be treated as equivalent to the max. possible load (the max. force). Characterisic values of the load-bearing capacity Rk should be reduced to dimensioning values Rd with regard to the usage class and class of the load duration: $\mathrm{Rd}=\mathrm{Rk} \cdot \mathrm{Kmod} / \gamma \mathrm{m}$. The dimensioning values of the load-bearing capacity Rd should be contrasted with the dimensioning values of the loads ( $\mathrm{Rd} \geq \mathrm{Ed}$ ).
Example:
Characterisic value for constant lood (dead weight) $G_{k}=2,00 \mathrm{kN}$ and variable load (e. g. snow load) $Q_{k}=3,00 \mathrm{kN} . \mathrm{kmod}=0,9 . \gamma_{\mathrm{M}}=1,3$.
$\rightarrow$ Dimensioning value of the lood $\mathrm{E}_{\mathrm{d}}=2,00 \cdot 1,35+3,00 \cdot 1,5=7,20 \mathrm{kN}$.
The load-bearing capacity of the joint is therefore considered to have been demonstrated if $\mathrm{R}_{\mathrm{d}} \geq \mathrm{E}_{\mathrm{d}} \rightarrow \min \mathrm{R}_{\mathrm{k}}=\mathrm{R}_{\mathrm{d}} \cdot \gamma \mathrm{M} / \mathrm{kmod}$
i.e. the characteristic minimum value is calculcted based on: $\min \mathrm{Rk}_{\mathrm{k}}=\mathrm{Rd}_{\mathrm{d}} \cdot \gamma_{\mathrm{M}} / \mathrm{kmod} \rightarrow \mathrm{Rk}=7,20 \mathrm{kN} \cdot 1,3 / 0,9=10,40 \mathrm{kN} \rightarrow$ comparison with table values.
b) estimated with on efficient quantity of pairs of screws: $n, 9$.

Please note: These are planning viids. Projects must only be caluluated by authorised persons.

## Gurotec

## KONSTRUX ST WITH CYLINDER HEAD AND DRILL POINT 10,0 MM: MAIN-SECONDARY BEAM JOINTS



All values cre caluclated minimum volues and rer stbiect to typographical and piniting eroros.



## Example:


$\rightarrow$ Dimensioning value of the lood $\mathrm{E}_{\mathrm{d}}=2,00 \cdot 1,35+3,00 \cdot 1,5=1,20 \mathrm{kN}$.
The lood bearing capocity of the jointit is therefore considereded to have been demonstruted if $\mathrm{R}_{d} \geq \mathrm{E}_{d} \rightarrow \min \mathrm{R}_{\mathrm{K}}=\mathrm{R}_{d} \cdot \gamma_{M} / \mathrm{kmod}_{\mathrm{mod}}$

b) essimated with on efficient quantity of pais of screws: $n^{0,}$ ?

Please note: These cre planning idid. Projects must only be calculcied by wuthorised persons.

## KONSTRUX ST WITH CYLINDER HEAD 6,5 MM

## GEOMETRY AND MECHANICAL PROPERTIES



| KonstruX ST-ZK 06,5xL -TX30 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Art. no. | $\begin{gathered} \lfloor \\ {[\mathrm{mm}]} \end{gathered}$ | $\begin{aligned} & L_{g_{1,} \text { eff }} \\ & {[\mathrm{mm}]} \end{aligned}$ | PU | Pre-drilling diameter $\mathrm{Od}_{\mathrm{v}}[\mathrm{mm}]$ | Characteristic pull-out resistance value $\mathrm{f}_{\mathrm{ax}, \mathrm{k}}\left[\mathrm{N} / \mathrm{mm}^{2}\right]$ | Characteristic tensile strength value $f_{\text {tens, }, 1}[k N]$ | Characteristic yield moment $M_{y, k}[\mathrm{Nmm}]$ | Characteristic yield strength $f_{y, 1}\left[\mathrm{~N} / \mathrm{mm}^{2}\right]$ |
| 904808 | 80 | 71 | 100 | 4,5 | 11,4 | 17,0 | 15000 | 1000 |
| 904809 | 100 | 91 | 100 | 4,5 | 11,4 | 17,0 | 15000 | 1000 |
| 904810 | 120 | 111 | 100 | 4,5 | 11,4 | 17,0 | 15000 | 1000 |
| 904811 | 140 | 131 | 100 | 4,5 | 11,4 | 17,0 | 15000 | 1000 |
| 904812 | 160 | 151 | 100 | 4,5 | 11,4 | 17,0 | 15000 | 1000 |
| 904813 | 195 | 186 | 100 | 4,5 | 11,4 | 17,0 | 15000 | 1000 |

Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by authorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

## Gurotec

## Axial and edge distances

The minimum distances for KonstruX loaded exclusively in the axial direction in pre-drilled and non-pre-drilled holes in components measuring min. $t=65$ thick and min. 60 mm wide must be selected as follows

| Axial distance parallel to the direction of the grain | al | [mm] | 5.d | 33 |
| :---: | :---: | :---: | :---: | :---: |
| Axial distance perpendicular to the direction of the grain | 12 | [mm] | 5.d | 33 |
| Distance from the centre of gravity of the screw area driven into the wood from the end grain sufface | al, ${ }^{\text {a }}$ | [mm] | 5.d | 33 |
| Distance from the centre of gravity of the screw area driven into the wood from the side grain sufface | 02, 6 | [mm] | 3.d | 20 |
| Axial distance between a crossing pair of screws | 02,k | [mm] | 1,5•d | 10 |
| Reduced axial distance a2 perpendicular to the direction of the grain, if al $\cdot 02 \geq 25 \cdot \mathrm{~d}^{2}$ | a2,red | [mm] | 2,5•d | 16 |

## The axial and edge distances are minimum distances according to DIN EN 1995:2014 (EC5) and generally apply to fasteners subjected to transverse loads

al
Distance from the fasteners within a row in the direction of the grain

a2
Distance from the fasteners perpendicular to the direction of the grain

a3,
Distance between the fastener and the unloaded end of the end groin $90^{\circ} \leq \alpha \leq 270^{\circ}$


03,1
Distance between the fastener and the loaded end of the end grain $-90^{\circ} \leq \alpha \leq 90^{\circ}$
a4,
Distance between the fustener and the unloaded edge $180^{\circ} \leq \alpha \leq 360^{\circ}$
a4,



|  |  |  | Force $/$ fibre angle $\alpha=0^{\circ}$ |  | Force $/$ fibre angle $\alpha=90^{\circ}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Axial distance parallel to the direction of the grain | al | [mm] | 5.d | 33 | 4.d | 33 |
| Axial distance perpendicular to the direction of the grain | 02 | [mm] | 3.d | 20 | 4.d | 33 |
| Distance from the centre of gravity of the screw area driven into the wood from the unloaded end of the end grain | a3, | [mm] | 7.d | 46 | 7.d | 46 |
| Distance from the centre of gravity of the screw area driven into the wood from the loaded end of the end groin | a3, | [mm] | 12.d | 78 | 7.d | 46 |
| Axial distance perpendicular to the unlooded edge | 04, | [mm] | 3.d | 20 | 3.d | 20 |
| Axial distance from the loaded edge | 04, | [mm] | 3.d | 20 | 7.d | 46 |

When analysed, the minimum distances for KonstruX in non-pre-drilled holes, loaded in a crosswise direction, are as follows according to the position of the direction of the grain


[^1]
## Eurotec

## KONSTRUX ST WITH CYIINDER HEAD AND DRILL POINT <br> 6,5 MM: SHEARING STRENGTH RATIO WITHOUT PRE-DRILIING



Calculation according to ETA- $\mathrm{II} / 0024$. Wood density $\rho_{k}=380 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
a) The characterisicic valves of the lood-bearing capacity Rk cannot be treated as equivalent to the max. possible load (the max. force). Characteristic valves of the lood-bearing capacity Rk should be reduced to dimensioning values Rd with regard to the usage class and class of the load duration: $\operatorname{Rd}=\mathrm{Rk}_{\mathrm{k}} \cdot \mathrm{kmod}_{\mathrm{m}} / \gamma \mathrm{M}$. The dimensioning values of the load-bearing capacity $\operatorname{Rd}$ should be contrassed with the dimensioning values of the loads ( $\left.\mathrm{Rd}_{d} \geq \mathrm{Ed}\right)$.

## KONSTRUX ST WITH CYLINDER HEAD AND DRILL POINT 6,5 MM: AXIAL PULL-OUT LOAD CAPACITY WITHOUT PRE-DRILIING



| Odl xL[mm] | A [mm] | B [mm] | ${\mathrm{Rax}, 1^{\text {a }}}^{\text {a) }}$ [ [kN] | $\mathrm{Rk}^{\text {a) }}$-[kN] | $\mathrm{Rax}_{\mathrm{ax}} \mathrm{K}^{\text {a) }} \cdot[\mathrm{KN}]$ | $\mathrm{Rk}^{\text {a) }}$-[kN] | $\mathrm{Rax}_{\mathrm{ux}} \mathrm{k}^{\text {a) }}$.[kN] | $\mathrm{Rk}^{\text {a) }}$-[kN] | $\mathrm{Rax}_{\mathrm{ax}} \mathrm{K}^{\text {a) }} \cdot[\mathrm{KN}]$ | $\mathrm{Rk}^{\text {a) }} \cdot[\mathrm{lkN}]$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\alpha=45^{\circ}$ |  | $\begin{aligned} & \alpha A=90^{\circ} \\ & \alpha B=45^{\circ} \end{aligned}$ |  | $\begin{aligned} & \alpha A=90^{\circ} \\ & \alpha, B=90^{\circ} \end{aligned}$ |  | $\begin{aligned} & \alpha A=45^{\circ} \\ & \alpha B=90^{\circ} \end{aligned}$ |  |
| 6,5 $\times 160$ | 60 | 80 | 5,51 | 3,90 | 5,51 | 3,90 | 5,51 | 3,90 | 5,51 | 3,90 |
| $6,5 \times 195$ | 80 | 80 | 6,04 | 4,27 | 6,04 | 4,27 | 6,04 | 4,27 | 6,04 | 4,27 |

Calculation according to $\mathrm{ETA}-\mathrm{II} / 0024$. Wood density $\rho_{k}=380 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum valves and are subject to typographical and printing errors.
a) The characcteristic values of the load-bearing capacity Rk cannot be treated as equivalent to the max. possible load (the max. force). Characterisici values of the lood-bearing capacity Rk should be reduced to dimensioning values Rd with regard to the usage class and class of the load duration: $R_{d}=R_{k} \cdot k_{m o d} / \gamma \mathrm{M}$. The dimensioning values of the load-bearing capacity $R_{d}$ should be contrasted with the dimensioning values of the loads ( $\left.\mathrm{R}_{\mathrm{d}} \geq \mathrm{E} d\right)$.

## KONSTRUX ST WITH CYIINDER HEAD AND DRILL POINT 6,5 MM: MAIN-SECONDARY BEAM JOINTS

## Dimensions

## Main/secondary beam connection



Calculation according to $E A-11 / 0024$. Wood density $\rho \mathrm{pk}=380 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should he viewed as subject to the assumptions that have been made and represent example calculations. All values are calculated minimum values and are subject to typographical and printing errors.
a) The characteristic values of the load-bearing capacity Rk cannot be treated as equivalent to the max. possible lood (the max. force). Characterisici values of the lood-bearing capacity Rks should be reduced to dimensioning values Rd with regard to the usage class and dlass of the load duration: $\mathbb{R d}_{d}=R_{k} \cdot \mathrm{~K}_{\text {mod }} / \gamma \mathrm{M}$. The dimensioning values of the load-bearing capacity $\mathrm{R}_{\mathrm{d}}$ should be contrasted with the dimensioning values of the loads ( $\mathrm{R}_{d} \geq \mathrm{E}_{\mathrm{d}}$ ).

Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by authorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

## Gurotec

## ANGLE-BRACKET SCREW (ABS)



## ADVANTAGES

- Quick and easy screwing-in

Reduced spliting effect
National and international approvals

## DESCRIPTION

The Eurotec Angle-bracket screw (ABS) is made of hardened carbon steel and is specially designed for joints between steel sheet and wood. The spliting effect in the wood is reduced by the geometry of the screw tip. In addition, the screw is characterized, among other things, by the smooth shank under the head, which allows load transfer during shearing.


| Angle-bracket screw | (E) | Art. no. | Dimensions [mm] | Drive | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Blue galvanised |  | 945343 | $5,0 \times 25$ | TX20 | 250 |
|  |  | 945232 | $5,0 \times 35$ | TX20 | 250 |
|  |  | 945241 | $5,0 \times 40$ | TX20 | 250 |
|  |  | 945233 | $5,0 \times 50$ | TX20 | 250 |
|  |  | 945344 | $5,0 \times 60$ | TX20 | 250 |
|  |  | 945345 | $5,0 \times 70$ | TX20 | 250 |

## TECHNICAL INFORMATIONS <br> ANGLE-BRACKET SCREW, STEEL BLUE GALVANISED



Calculation according to $\mathrm{ETA}-\mathrm{Il} / 0024$. Wood density $\mathrm{\rho k}=350 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values. Typesetting and printing errors are excepted.
a) The characterisicic values of the load-bearing capacity Rk should not be treated os equivalent to the max. possible load (the max. force). Characteristic values of the load-bearing capacity Rk are to be reduced to the design valves Rd as regards the service class and class of the load duration: $R_{d}=R_{k} \cdot k_{m o d} / \gamma M$. The design values of the lood- bearing capacity $R d$ should be compared to the design values of the loads $\left(R_{d} \geq E_{d}\right)$.

## Example:

Characteristic value for constant load (dead load) $G_{k}=2,00 \mathrm{kN}$ and variable load (e.g. snow load) $Q_{k}=3,00 \mathrm{kN} . \mathrm{k}_{\mathrm{mod}}=0,9 . \gamma \mathrm{M}=1,3$.
$\rightarrow$ Rated value of the load $E_{d}=2,00 \cdot 1,35+3,00 \cdot 1,5=7,20 \mathrm{kN}$.
Load-bearing capacity of the connection is proved if $\mathrm{R}_{d} \geq \mathrm{Ed}_{\mathrm{d}} \rightarrow \mathrm{min} \mathrm{R}_{k}=\mathrm{R}_{d} \cdot \gamma \mathrm{M} / \mathrm{kmod}$
That is, the characterisic minimum value of the load-bearing capacity is calculated as: $\min \mathrm{R}_{\mathrm{k}}=\mathrm{Rd}_{\mathrm{d}} \cdot \gamma_{\mathrm{M}} / \mathrm{kmod}_{\bmod } \rightarrow \mathrm{Rk}_{\mathrm{k}}=7,20 \mathrm{kN} \cdot 1,3 / 0,9=10,40 \mathrm{kN} \rightarrow$ aligned with table values.
Please note: These are planning aids. Projects must only be calculated by authorised persons.
Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preiminary measurements. Projects are to be dimensioned exclusively by authorised persons in accordance wiht the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

## Gurotec

## PANELTWISTEC



## ADVANTAGES

- Quick and easy screwing-in

Reduced splitting effect

- National and international approvals
- Due to the special coating, the screw has a higher corrosion resistance than conventional galvanizing
- Can be used in service classes 1 and 2
- Free of chromium (VI) oxide
- Resistant to mechanical stress
- Prevents contact corrosion with attachments
- No hammering of the screws when screwing in due to TX-Drive


## DESCRIPTION

Paneltwistec wood construction screws may generally be installed in CLT without predrilling. The Paneltwistec is a wood construction screw with a special screw tip and milling ribs above the thread. The cutting notch on the screw tip ensures fast gripping and less splitting effect when screwing in. The Paneltwistec AG instead features a folded-down thread, which reduces the screw-in torque. Paneltwistec wood construction screws are available in both countersunk head and flanged button-head variants, as well as made of coated carbon steels and various stainless steels.



## Gurotec



TECHNICAL INFORMATION
PANELTWISTEC AG, COUNTERSUNK-HEAD, BLUE GALVANISED

| Dimensions |  |  |  | Extraction resistance | Head pull-through resistance | Wood-Wood shearing |  |  |  | Steel-Wood shearing |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | $\mathrm{V}\left(\mathrm{a}=0^{\circ}\right)$ <br> $V\left(\alpha=0^{\circ}\right)$ <br> $V\left(\alpha=0^{\circ}\right)$ <br> $\mathrm{V}\left(\alpha=90^{\circ}\right.$ |  |  |  |  |  |  |
| $\begin{aligned} & \mathrm{dl} \times \mathrm{L} \\ & {[\mathrm{~mm}]} \end{aligned}$ | $\begin{gathered} \mathrm{dk} \\ {[\mathrm{~mm}]} \end{gathered}$ | $\begin{gathered} A D \\ {[\mathrm{~mm}]} \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ {[\mathrm{~mm}]} \end{gathered}$ | $\mathrm{Fax}_{\mathrm{ax}}, 90, \mathrm{Rk}$ <br> [kN] | Fax,head, Rk [kN] | Fla,Rk <br> [kN] | Fla,Rk <br> [kN] | Fla,Rk [kN] | Fla,Rk <br> [kN] | $\begin{gathered} \dagger \\ {[\mathrm{mm}]} \end{gathered}$ | Fla,Rk [kN] | Fla,Rk <br> [kN] |
|  |  |  |  |  |  |  |  | $\alpha A D=0^{\circ}$ | $\angle A D=90^{\circ}$ |  |  |  |
|  |  |  |  |  |  | $\alpha=0^{\circ}$ | $\alpha=90^{\circ}$ | $\alpha \mathrm{EI}=90^{\circ}$ | aEI $=0^{\circ}$ |  | $\alpha=0^{\circ}$ | $\alpha=90^{\circ}$ |
| 3,5×30 | 7,0 | 12 | 18 | 0,84 | 0,59 |  |  |  |  | 1 |  | 86 |
| 3,5×35 | 7,0 | 14 | 21 | 0,98 | 0,59 |  |  |  |  | 1 |  | 92 |
| 3,5440 | 7,0 | 16 | 24 | 1,12 | 0,59 |  |  |  |  | 1 |  | 95 |
| 3,5445 | 7,0 | 18 | 27 | 1,26 | 0,59 |  |  |  |  | 1 |  | 99 |
| 3,5×50 | 7,0 | 20 | 30 | 1,40 | 0,59 |  |  |  |  | 1 |  | 02 |
| 4,0×30 | 8,0 | 12 | 18 | 0,93 | 0,7 |  |  |  |  | 2 |  | 91 |
| 4,0×35 | 8,0 | 14 | 21 | 1,08 | 0,71 |  |  |  |  | 2 |  | 107 |
| 4,0×40 | 8,0 | 16 | 24 | 1,24 | 0,7 |  |  |  |  | 2 |  | 15 |
| 4,0x45 | 8,0 | 18 | 27 | 1,39 | 0,71 |  |  |  |  | 2 |  | 19 |
| 4,0×50 | 8,0 | 20 | 30 | 1,55 | 0,71 |  |  |  |  | 2 |  | 23 |
| 4,0×60 | 8,0 | 24 | 36 | 1,86 | 0,7 |  |  |  |  | 2 |  | 31 |
| 4,0×70 | 8,0 | 28 | 42 | 2,17 | 0,71 |  |  |  |  | 2 |  | 138 |
| 4,0x80 | 8,0 | 32 | 48 | 2,48 | 0,71 |  |  |  |  | 2 |  | 46 |
| 4,540 | 9,0 | 16 | 24 | 1,35 | 0,97 |  |  |  |  | 2 |  | 34 |
| 4,5 45 | 9,0 | 18 | 27 | 1,52 | 0,97 |  |  |  |  | 2 |  | 40 |
| 4,5 $\times 50$ | 9,0 | 20 | 30 | 1,69 | 0,97 |  |  |  |  | 2 |  | 44 |
| 4,5 $\times 60$ | 9,0 | 24 | 36 | 2,03 | 0,97 |  |  |  |  | 2 |  | 53 |
| 4,5 $\times 70$ | 9,0 | 28 | 42 | 2,36 | 0,97 |  |  |  |  | 2 |  | 161 |
| 4,5×80 | 9,0 | 32 | 48 | 2,70 | 0,97 |  |  |  |  | 2 |  | 70 |
| 5,0×40 | 10,0 | 16 | 24 | 1,45 | 1,20 |  |  |  |  | 2 |  | 44 |
| 5,0×45 | 10,0 | 18 | 27 | 1,63 | 1,20 |  |  |  |  | 2 |  | 16 |
| 5,0×50 | 10,0 | 20 | 30 | 1,82 | 1,20 |  |  |  |  | 2 |  | 167 |
| $5,0 \times 60$ | 10,0 | 24 | 36 | 2,18 | 1,20 |  |  |  |  | 2 |  | ,76 |
| 5,0×70 | 10,0 | 28 | 42 | 2,54 | 1,20 |  |  |  |  | 2 |  | 185 |
| 5,0×80 | 10,0 | 32 | 48 | 2,90 | 1,20 |  |  |  |  | 2 |  | 94 |
| $5,0 \times 90$ | 10,0 | 36 | 54 | 3,27 | 1,20 |  |  |  |  | 2 |  | 03 |
| 5,0 100 | 10,0 | 40 | 60 | 3,63 | 1,20 |  |  |  |  | 2 |  | 12 |
| 5,0× 120 | 10,0 | 50 | 70 | 4,24 | 1,20 |  |  |  |  | 2 |  | 27 |

Calculation according to $\mathrm{ETA}-\mathrm{II} / 0024$. Wood density $\rho \mathrm{k}=350 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
a) The characteristic values of the load-bearing capacity Rk cannot be treated as equivalent to the max. possible lood (the max. force). Characterisicic values of the lood-bearing capacity Rk should be reduced to dimensioning values Rd with regard to the usage class and dass of the load duration: $\mathbb{R}_{d}=\mathbb{R}_{k} \cdot \mathcal{k}_{\bmod } / \gamma$. The dimensioning values of the load bearing capacity $\mathrm{R}_{d}$ should be contrasted with the dimensioning values of the loads ( $\left.\mathrm{R}_{d} \geq \mathrm{E}_{\mathrm{d}}\right)$.

## Example:

Characterisic valve for constant load (dead weight) $G_{k}=2,00 \mathrm{kN}$ and variable load (e. g. snow load) $Q_{k}=3,00 \mathrm{kN} . \mathrm{kmod}^{2}=0,9 \cdot \gamma \mathrm{M}=1,3$.
$\rightarrow$ Dimensioning value of the lood $\mathrm{E} d=2,00 \cdot 1,35+3,00 \cdot 1,5=7,20 \mathrm{kN}$.
The load-bearing capacity of the joint is therefore considered to have been demonstrated if $R_{d} \geq \mathrm{E}_{\mathrm{d}} \rightarrow \mathrm{min} \mathrm{R}_{\mathrm{k}}=\mathrm{R}_{\mathrm{d}} \cdot \gamma_{\mathrm{M}} / \mathrm{kmod}_{\mathrm{m}}$
i.e. the characteristic minimum value is calculated based on: $\min \mathrm{R}_{k}=\mathrm{R}_{\mathrm{d}} \cdot \gamma \mathrm{M} / \mathrm{kmod}_{\bmod } \rightarrow \mathrm{R}_{k}=7,20 \mathrm{kN} \cdot 1,3 / 0,9=10,40 \mathrm{kN} \rightarrow$ comparison with table values..

Please note: These are planning cids. Projects must only be calculated by authorised persons.
Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by authorised
persons in occordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

## Gurotec



Calculation according to $\mathrm{ETA}-\mathrm{Il} /$ /O024. Wood density $\rho_{\mathrm{k}}=350 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
a) The characteristic values of the load-bearing capacity Rk cannot be treated as equivalent to the max. possible load (the max. force). Characterisicic values of the load-bearing capacity Rk should be reduced to dimensioning values Rd with regard to the usage dlass and class of the load duration: $\mathbb{R d}_{d}=\mathbb{R}_{k} \cdot \operatorname{knod}_{\mathrm{mod}} / \gamma \mathrm{M}$. The dimensioning values of the load-bearing capacity $\mathbb{R}_{d}$ should be contrasted with the dimensioning values of the loads ( $\left.\mathbb{R}_{d} \geq \mathrm{E}_{d}\right)$.

## Example:

Characterisic value for constant load (dead weight) $G_{k}=2,00 \mathrm{kN}$ and variable load (e. g. snow lood) $Q_{k}=3,00 \mathrm{kN} . \mathrm{kmod}=0,9 . \gamma \mathrm{M}=1,3$.
$\rightarrow$ Dimensioning value of the lood $E d=2,00 \cdot 1,35+3,00 \cdot 1,5=7,20 \mathrm{kN}$.
The load-bearing capacity of the joint is therefore considered to have been demonstrated if $\mathrm{R}_{\mathrm{d}} \geq \mathrm{Ed}_{\mathrm{d}} \rightarrow \min \mathrm{R}_{\mathrm{k}}=\mathrm{Rd}_{\mathrm{d}} \cdot \gamma_{\mathrm{M}} / \mathrm{kmod}$
i.e. the characteristic minimum value is calculated based on: $\min \mathrm{R}_{\mathrm{k}}=\mathrm{R}_{\mathrm{d}} \cdot \gamma_{\mathrm{M}} / \mathrm{k}_{\bmod } \rightarrow \mathrm{R}_{k}=7,20 \mathrm{kN} \cdot 1,3 / 0,9=10,40 \mathrm{kN} \rightarrow$ comparison with table values.

Please note: These are planning aids. Projects must only be calculated by authorised persons.

## Gurotec



Please note: Verify the assumptions made. The stated values, and type and number of joining devices are bassed on preliminary measurements. Projects are to be dimensioned exclusively by authorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

## Gurotec

| Paneltwistec AG | Art. no. | Dimensions [mm] | Drive | PU |
| :---: | :---: | :---: | :---: | :---: |
| Flanged button-head screw, blue galvanised | 946158 | 4,0 40 | TX20 | 500 |
|  | 946159 | 4,0 $\times 50$ | TX20 | 500 |
|  | 946160 | 4,0×60 | TX20 | 500 |
|  | 946161 | 4,5 5 50 | TX20 | 200 |
| ,hinhthentrss | 946162 | 4,5 560 | TX20 | 200 |
|  | 946163 | 4,5x70 | TX20 | 200 |
| ADVANTAGES | 946037 | 5,0 $\times 50$ | TX25 | 200 |
|  | 946038 | $5,0 \times 60$ | TX25 | 200 |
| and head pull-hrough capacity | 946039 | $5,0 \times 70$ | TX25 | 200 |
|  | 946040 | 5,0×80 | TX25 | 200 |
| This makes for better use of the screw's tensile load-bearing strength | 946042 | 5,0× 100 | TX25 | 200 |
|  | 945947 | 6,0 $\times 30$ | TX30 - | 100 |
|  | 945948 | 6,0 $\times 40$ | TX30 - | 100 |
|  | 945712 | 6,0 $\times 50$ | TX30 - | 100 |
|  | 945713 | 6,0×60 | TX30- | 100 |
|  | 945716 | 6,0×70 | TX30- | 100 |
|  | 945717 | 6,0x80 | TX30 - | 100 |
|  | 945718 | 6,0×90 | TX30- | 100 |
|  | 945719 | 6,0× 100 | TX30- | 100 |
|  | 945720 | 6,0× 110 | TX30- | 100 |
|  | 945721 | $6,0 \times 120$ | TX30 - | 100 |
|  | 945722 | 6,0×130 | TX30 - | 100 |
|  | 945723 | 6,0×140 | TX30- | 100 |
|  | 945724 | $6,0 \times 150$ | TX30 - | 100 |
|  | 945725 | 6,0×160 | TX30- | 100 |
|  | 945726 | 6,0×180 | TX30 - | 100 |
|  | 945727 | 6,0×200 | TX30- | 100 |
|  | 945728 | 6,0x 220 | TX30 - | 100 |
|  | 945729 | 6,0×240 | TX30 - | 100 |
|  | 945730 | 6,0×260 | TX30 - | 100 |
|  | 945731 | 6,0x 280 | TX30 - | 100 |
|  | 945732 | 6,0×300 | TX30 - | 100 |


| Paneltwistec AG | Art. no. | Dimensions [mm] | Drive | PU |
| :---: | :---: | :---: | :---: | :---: |
| Flanged bution-head screw, blue galvanised | 945806 | 8,0×60 | TX40 | 50 |
|  | 944588 | $8,0 \times 80$ | TX40 - | 50 |
| $\rightarrow$ chathathatercer | 944589 | $8,0 \times 100$ | TX40 | 50 |
| Whenthethrses | 944590 | $8,0 \times 120$ | TX40 - | 50 |
|  | 94459 | $8,0 \times 140$ | TX40 - | 50 |
| ADVANTAGES | 94592 | $8,0 \times 160$ | TX40 | 50 |
|  | 94593 | $8,0 \times 180$ | TX40 | 50 |
| The larger head diameter allows for considerably higher torque and head pull-through capacity | 94459 | $8,0 \times 200$ | TX40 | 50 |
| and head puli-through capacity | 94595 | 8,0x 220 | TX40 | 50 |
| This makes for better use of the screw's tensile load-bearing strength | 944596 | 8,0×240 | TX40 - | 50 |
|  | 94459 | 8,0x 260 | TX40 - | 50 |
|  | 94459 | 8,0×280 | TX40 - | 50 |
|  | 944599 | 8,0x 300 | TX40 | 50 |
|  | 94660 | 8,0 $\times 320$ | TX40 - | 50 |
|  | 94601 | 8,0x 340 | TX40 | 50 |
|  | 94460 | 8,0×360 | TX40 - | 50 |
|  | 94603 | 8,0x 380 | TX40 - | 50 |
|  | 94604 | $8,0 \times 400$ | TX40 | 50 |
|  | 94605 | 8,0 420 | TX40 - | 25 |
|  | 946606 | $8,0 \times 440$ | TX40 | 25 |
|  | 94607 | 8,0 460 | TX40 | 25 |
|  | 944608 | $8,0 \times 480$ | TX40 - | 25 |
|  | 94609 | 8,0 500 | TX40 | 25 |
|  | 944610 | 8,0x550 | TX40 | 25 |
|  | 946611 | 8,0x600 | TX40 | 25 |



## Gurotec

## TECHNICAL INFORMATION <br> PANELTWISTEC AG, FLANGE BUTTON HEAD, BLUE GALVANISED

| Dimensions |  |  |  | Extraction resistance | Head pull-through resistance | Wood-Wood shearing |  |  |  | Steel-Wood shearing |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $-\stackrel{-}{-\frac{d k_{1}}{-}}$ |  |  |  |  |  | $\mathrm{V}\left(\mathrm{a}=0^{\circ}\right)$ <br> $V\left(\alpha=0^{\circ}\right)$ <br> $V\left(\alpha=0^{\circ}\right.$ <br> $V\left(\alpha=90^{\circ}\right)$ |  | $\begin{aligned} & V\left(\mathrm{a}=90^{\circ}\right) \\ & V\left(\mathrm{a}=90^{\circ}\right) \\ & V\left(\mathrm{a}=90^{\circ}\right) \\ & \square \\ & V_{\left(\alpha=0^{\circ}\right)} \end{aligned}$ |  |  |  |  |
| $\begin{aligned} & \mathrm{dl} \times \mathrm{L} \\ & {[\mathrm{~mm}]} \end{aligned}$ | $\begin{gathered} d k \\ {[\mathrm{~mm}]} \end{gathered}$ | $\begin{gathered} \mathrm{AD} \\ {[\mathrm{~mm}]} \end{gathered}$ | $\begin{gathered} \mathrm{El} \\ {[\mathrm{~mm}]} \end{gathered}$ | $F_{a x}, 90$,Rk <br> [kN] | Fox,head,Rk <br> [kN] | Fla, Rk <br> [kN] | Fla,Rk [kN] | Fla,Rk [kN] | Fla,Rk [kN] | $\begin{gathered} \dagger \\ {[\mathrm{mm}]} \end{gathered}$ | Fla,Rk <br> [kN] | Fla,Rk [kN] |
|  |  |  |  |  |  |  |  | $\alpha_{A D}=0^{\circ}$ | $\alpha_{A D}=90^{\circ}$ |  |  |  |
|  |  |  |  |  |  | $\alpha=0^{\circ}$ | $\alpha=90^{\circ}$ | $\alpha_{\text {EE }}=90^{\circ}$ | $\alpha_{E I}=0^{\circ}$ |  | $\alpha=0^{\circ}$ | $\alpha=90^{\circ}$ |
| 4,0x40 | 10,0 | 16 | 24 | 1,24 | 1,20 |  |  |  |  | 2 |  |  |
| $4,0 \times 50$ | 10,0 | 20 | 30 | 1,55 | 1,20 |  |  |  |  | 2 |  |  |
| $4,0 \times 60$ | 10,0 | 24 | 36 | 1,86 | 1,20 |  |  |  |  | 2 |  |  |
| 4,5x 50 | 11,0 | 20 | 30 | 1,69 | 1,45 |  |  |  |  | 2 |  | 44 |
| 4,5x60 | 11,0 | 24 | 36 | 2,03 | 1,45 |  |  |  |  | 2 |  |  |
| 4,5×70 | 11,0 | 28 | 42 | 2,36 | 1,45 |  |  |  |  | 2 |  |  |
| 5,0x50 | 12,0 | 20 | 30 | 1,82 | 1,73 |  |  |  |  | 2 |  |  |
| 5,0×60 | 12,0 | 24 | 36 | 2,18 | 1,73 |  |  |  |  | 2 |  |  |
| 5,0×70 | 12,0 | 28 | 42 | 2,54 | 1,73 |  |  |  |  | 2 |  |  |
| $5,0 \times 80$ | 12,0 | 32 | 48 | 2,90 | 1,73 |  |  |  |  | 2 |  |  |
| 5,0x 100 | 12,0 | 40 | 60 | 3,63 | 1,73 |  |  |  |  | 2 |  |  |
| 6,0×30 | 14,0 | 6 | 24 | 1,64 | 2,35 |  |  |  |  | 2 |  | 20 |
| $6,0 \times 40$ | 14,0 | 16 | 24 | 1,64 | 2,35 |  |  |  |  | 2 |  | 63 |
| 6,0x50 | 14,0 | 20 | 30 | 2,05 | 2,35 |  |  |  |  | 2 |  |  |
| 6,0×60 | 14,0 | 24 | 36 | 2,46 | 2,35 |  |  |  |  | 2 |  | 26 |
| $6,0 \times 70$ | 14,0 | 28 | 42 | 2,87 | 2,35 |  |  |  |  | 2 |  | 36 |
| $6,0 \times 80$ | 14,0 | 32 | 48 | 3,28 | 2,35 |  |  |  |  | 2 |  |  |
| 6,0×90 | 14,0 | 36 | 54 | 3,69 | 2,35 |  |  |  |  | 2 |  |  |
| $6,0 \times 100$ | 14,0 | 40 | 60 | 4,10 | 2,35 |  |  |  |  | 2 |  | 67 |
| 6,0× 110 | 14,0 | 44 | 66 | 4,79 | 2,35 |  |  |  |  | 2 |  | 77 |
| 6,0× 120 | 14,0 | 50 | 70 | 4,79 | 2,35 |  |  |  |  | 2 |  | 84 |
| 6,0×130 | 14,0 | 60 | 70 | 4,79 | 2,35 |  |  |  |  | 2 |  | 84 |
| $6,0 \times 140$ | 14,0 | 70 | 70 | 4,79 | 2,35 |  |  |  |  | 2 |  | 84 |
| 6,0 $\times 150$ | 14,0 | 80 | 70 | 4,79 | 2,35 |  |  |  |  | 2 |  | 84 |
| $6,0 \times 160$ | 14,0 | 90 | 70 | 4,79 | 2,35 |  |  |  |  | 2 |  | 84 |
| 6,0×180 | 14,0 | 110 | 70 | 4,79 | 2,35 |  |  |  |  | 2 |  | 84 |
| 6,0×200 | 14,0 | 130 | 70 | 4,79 | 2,35 |  |  |  |  | 2 |  | 84 |
| 6,0×220 | 14,0 | 150 | 70 | 4,79 | 2,35 |  |  |  |  | 2 |  | 84 |
| 6,0×240 | 14,0 | 170 | 70 | 4,79 | 2,35 |  |  |  |  | 2 |  | 84 |
| 6,0 $\times 260$ | 14,0 | 190 | 70 | 4,79 | 2,35 |  |  |  |  | 2 |  | 84 |
| 6,0×280 | 14,0 | 210 | 70 | 4,79 | 2,35 |  |  |  |  | 2 |  | 84 |
| 6, $0 \times 300$ | 14,0 | 230 | 70 | 4,79 | 2,35 |  |  |  |  | 2 |  | 84 |


All values rer caluclated minimum values and are slibect to typographical and piniting eroros.
a) The charocterisisic values of fhe load.bearing capacity Rk cannot be tereted os equivilent to the max. possible lood (the max. fore). Characterisic values of the lood-bearing capacity Rk should be reduved to dimensioning values Rd


## Example:


$\rightarrow$ Dimensioning value of the lood $\mathrm{E}_{\mathrm{d}}=2,00 \cdot 1,35+3,00 \cdot 1,5=1,20 \mathrm{kN}$

i.e. the characteristic minimum value is calculcted bosed on: min $\mathrm{R}_{k}=\mathrm{R}_{\mathrm{d}} \cdot \gamma_{M} / \mathrm{kmod}_{\bmod } \rightarrow \mathrm{R}_{k}=7,20 \mathrm{kN} \cdot 1,3 / 0,9=10,40 \mathrm{kN} \rightarrow$ comparison wiht hable values.

Please note: These are planning dids. Projects must only be calculcted by wuthorised persons.

| Dimensions |  |  |  | Extraction resistance | Head pull-through resistance | Wood-Wood shearing |  |  |  | Steel-Wood shearing |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | $F_{a x, \text { head, Rk }}$ | $V\left(\alpha=0^{\circ}\right)$ <br> $V\left(a=0^{\circ}\right)$ <br> $V\left(\alpha=0^{\circ}\right)$ <br> $V\left(\alpha=90^{\circ}\right)$ |  |  |  |  |  |  |
| $\begin{aligned} & d l \times l \\ & {[\mathrm{~mm}]} \end{aligned}$ | $\begin{gathered} \mathrm{dk} \\ {[\mathrm{~mm}]} \end{gathered}$ | $\begin{array}{r} \mathrm{AD} \\ {[\mathrm{~mm}} \end{array}$ | $\begin{gathered} \mathrm{ET} \\ {[\mathrm{~mm}]} \end{gathered}$ | $F_{\text {ax }}, 90$, Rk <br> [kN] | $\begin{gathered} \text { Fax head, Rk }_{[k N]} \end{gathered}$ | $F_{l a, R k}$ <br> [kN] | Fla,Rk <br> [kN] | Fla,Rk <br> [kN] | Fla,Rk <br> [kN] | $\begin{gathered} \dagger \\ {[\mathrm{mm}]} \end{gathered}$ | Fla,Rk <br> [kN] | Fla,Rk <br> [kN] |
|  |  |  |  |  |  |  |  | $\alpha A D=0^{\circ}$ | $\alpha A D=90^{\circ}$ |  |  |  |
|  |  |  |  |  |  | $\alpha=0^{\circ}$ | $\alpha=90^{\circ}$ | $\alpha \mathrm{ET}=90^{\circ}$ | $\alpha_{E T}=0^{\circ}$ |  | $\alpha=0^{\circ}$ | $\alpha=90^{\circ}$ |
| $8,0 \times 80$ | 22,0 | 30 | 50 | 4,26 | 5,81 | 4,14 | 3,34 | 4,14 | 3,34 | 3 | 4,56 | 3,94 |
| $8,0 \times 100$ | 22,0 | 40 | 60 | 5,33 | 5,81 | 4,83 | 4,01 | 4,83 | 4,01 | 3 | 4,83 | 4,20 |
| $8,0 \times 120$ | 22,0 | 50 | 70 | 5,86 | 5,81 | 4,95 | 4,32 | 4,95 | 4,32 | 3 | 4,96 | 4,34 |
| $8,0 \times 140$ | 22,0 | 40 | 100 | 8,44 | 5,81 | 4,95 | 4,13 | 4,95 | 4,13 | 3 | 5,60 | 4,98 |
| $8,0 \times 160$ | 22,0 | 60 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,95 | 4,32 | 3 | 5,60 | 4,98 |
| $8,0 \times 180$ | 22,0 | 80 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,95 | 4,32 | 3 | 5,60 | 4,98 |
| $8,0 \times 200$ | 22,0 | 100 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 220$ | 22,0 | 120 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 240$ | 22,0 | 140 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 260$ | 22,0 | 160 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 280$ | 22,0 | 180 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 300$ | 22,0 | 200 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 320$ | 22,0 | 220 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 340$ | 22,0 | 240 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 360$ | 22,0 | 260 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 380$ | 22,0 | 280 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 400$ | 22,0 | 300 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 420$ | 22,0 | 300 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 440$ | 22,0 | 300 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 460$ | 22,0 | 300 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 480$ | 22,0 | 300 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 500$ | 22,0 | 300 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 550$ | 22,0 | 300 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |
| $8,0 \times 600$ | 22,0 | 300 | 100 | 8,44 | 5,81 | 4,95 | 4,32 | 4,32 | 4,95 | 3 | 5,60 | 4,98 |

Calculation according to $\mathrm{EA}-11 / 0024$. Wood density $\rho \mathrm{pk}=350 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
a) The characteristic valves of the load-bearing capacity Rk cannot be treated as equivalent to the max. possible load (the max. force). Characterisicic values of the load-bearing capacity Rk should be reduced to dimensioning values Rd
with regard to the usage class and dlass of the load duration: $\mathrm{Rd}=\mathrm{Rk}_{\mathrm{R}} \cdot \mathrm{Kmod} / \gamma$ M. The dimensioning values of the load-bearing capacity Rd should be contrasted with the dimensioning values of the loads ( $\mathrm{Rd} \geq \mathrm{Ed}$ ).

## Example:

Characterisic value for constant load (dead weight) $G_{k}=2,00 \mathrm{kN}$ and variable load (e. g. snow load) $Q_{k}=3,00 \mathrm{kN} . \mathrm{kmod}^{2}=0,9 \cdot \gamma \mathrm{M}=1,3$.
$\rightarrow$ Dimensioning value of the lood $\mathrm{Ed}=2,00 \cdot 1,35+3,00 \cdot 1,5=7,20 \mathrm{kN}$.
The load-bearing capacity of the joint is therefore considered to have been demonstrated if $\mathrm{Rd} \geq \mathrm{Ed} . \rightarrow \mathrm{min} \mathrm{Rk}=\mathrm{Rd} \cdot \gamma \mathrm{M} / \mathrm{kmod}$
i.e. the characteristic minimum value is calculated based on: $\min \mathrm{R}_{k}=\mathrm{R}_{d} \cdot \gamma_{M} / \mathrm{kmod}_{\bmod } \rightarrow \mathrm{R}_{k}=7,20 \mathrm{kN} \cdot 1,3 / 0,9=10,40 \mathrm{kN} \rightarrow$ comparison with table values.

Please note: These are planning aids. Projects must only be calculated by authorised persons.

## Eurotec

| Dimensions |  |  |  | Extraction resistance | Head pull-through resistance | Wood-Wood shearing |  |  |  | Steel-Wood shearing |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & \mathrm{dl} \mathrm{xL} \\ & {[\mathrm{~mm}]} \end{aligned}$ | $\begin{gathered} \mathrm{dk} \\ {[\mathrm{~mm}]} \end{gathered}$ | $\begin{gathered} A D \\ {[\mathrm{~mm}]} \end{gathered}$ | $\begin{gathered} \mathrm{El} \\ {[\mathrm{~mm}]} \end{gathered}$ | $F_{a x}, 90$, Rk <br> [kN] | $\begin{gathered} \mathrm{Fax}_{\text {head, } \mathrm{Rk}} \\ {[\mathrm{kNN}]} \end{gathered}$ | Fla, Rk <br> [kN] | $F_{l a, R k}$ <br> [kN] | Fla,Rk <br> [kN] | Fla,Rk <br> [kN] | $\begin{array}{c\|c} t & F_{\text {la, Rk }} \\ {[\mathrm{mm}]} & {[\mathrm{kN}]} \end{array}$ | $F$ la, Rk <br> [kN] |
|  |  |  |  |  |  |  |  | $\alpha A D=0^{\circ}$ | $\angle A D=90^{\circ}$ |  |  |
|  |  |  |  |  |  | $\alpha=0^{\circ}$ | $\alpha=90^{\circ}$ | $\alpha \mathrm{ET}=90^{\circ}$ | $\alpha \mathrm{ET}=0^{\circ}$ | $\alpha=0^{\circ}$ | $\alpha=90^{\circ}$ |
| $10,0 \times 100$ | 25,0 | 40 | 60 | 6,48 | 7,50 | 6,44 | 5,08 | 6,44 | 5,08 | 6,78 | 5,81 |
| $10,0 \times 120$ | 25,0 | 50 | 70 | 7,13 | 7,50 | 6,94 | 5,74 | 6,94 | 5,74 | 6,94 | 5,97 |
| $10,0 \times 140$ | 25,0 | 40 | 100 | 10,26 | 1,50 | 6,70 | 5,34 | 6,70 | 5,34 | $3 \quad 7,72$ | 6,76 |
| $10,0 \times 160$ | 25,0 | 60 | 100 | 10,26 | 7,50 | 7,03 | 6,07 | 7,03 | 6,07 | 7,72 | 6,76 |
| $10,0 \times 180$ | 25,0 | 80 | 100 | 10,26 | 7,50 | 7,03 | 6,07 | 7,03 | 6,07 | 7,72 | 6,76 |
| $10,0 \times 200$ | 25,0 | 100 | 100 | 10,26 | 7,50 | 7,03 | 6,07 | 6,07 | 7,03 | 7,72 | 6,76 |
| $10,0 \times 220$ | 25,0 | 120 | 100 | 10,26 | 7,50 | 1,03 | 6,07 | 6,07 | 7,03 | $3 \quad 7,72$ | 6,76 |
| $10,0 \times 240$ | 25,0 | 140 | 100 | 10,26 | 7,50 | 7,03 | 6,07 | 6,07 | 7,03 | $3 \quad 7,72$ | 6,76 |
| $10,0 \times 260$ | 25,0 | 160 | 100 | 10,26 | 7,50 | 7,03 | 6,07 | 6,07 | 7,03 | $3 \quad 7,72$ | 6,76 |
| $10,0 \times 280$ | 25,0 | 180 | 100 | 10,26 | 7,50 | 7,03 | 6,07 | 6,07 | 7,03 | 7,72 | 6,76 |
| $10,0 \times 300$ | 25,0 | 200 | 100 | 10,26 | 1,50 | 1,03 | 6,07 | 6,07 | 7,03 | 7,72 | 6,76 |
| $10,0 \times 320$ | 25,0 | 220 | 100 | 10,26 | 1,50 | 7,03 | 6,07 | 6,07 | 7,03 | $3 \quad 7,72$ | 6,76 |
| $10,0 \times 340$ | 25,0 | 240 | 100 | 10,26 | 7,50 | 7,03 | 6,07 | 6,07 | 7,03 | 3 7,72 | 6,76 |
| $10,0 \times 360$ | 25,0 | 260 | 100 | 10,26 | 7,50 | 1,03 | 6,07 | 6,07 | 7,03 | $3 \quad 7,72$ | 6,76 |
| $10,0 \times 380$ | 25,0 | 280 | 100 | 10,26 | 7,50 | 7,03 | 6,07 | 6,07 | 7,03 | 7,72 | 6,76 |
| 10,0× 400 | 25,0 | 300 | 100 | 10,26 | 7,50 | 7,03 | 6,07 | 6,07 | 7,03 | $3 \quad 7,72$ | 6,76 |

Calculation according to EA- $11 / 0024$. Wood density $\mathrm{pk}=350 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical values provided should be viewed as subject to the assumptions that have been made and represent example calculations. All values are calculated minimum values and are subject to typographical and printing errors.
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## PANELTWISTEC, PANELTWISTEC AG

## HARDENED STAINLESS STEEL



| Paneltwistec :CE | Art. no. | Dimensions [mm] | Drive | PU |
| :---: | :---: | :---: | :---: | :---: |
| Countersunkhead, hardened stainless steel | 90477 | 4,0x40 | TX20 | 500 |
|  | 904775 | $4,0 \times 45$ | TX20 | 500 |
|  | 90476 | 4,0 $\times 50$ | TX20 | 500 |
| Hornrorrorror | 90447 | $4,0 \times 60$ | TX20 | 500 |
|  | 904778 | 4,5 $\times 45$ | TX20 | 200 |
| Rost ${ }^{\text {coishathe }}$ | 90479 | 4,5 550 | TX20 | 200 |
| fretf | 90488 | 4,5 560 | TX20 | 200 |
|  | 904881 | 4,5 $\times 70$ | TX20 | 200 |
|  | 100981 | 4,5×80 | TX20 | 200 |
| ADVANTAGES | 904882 | $5,0 \times 50$ | TX25 | 200 |
|  | 90488 | 5,0×60 | TX25 | 200 |
| - Limited resistance to acid | 90488 | $5,0 \times 70$ | TX25 | 200 |
| Not suitable for use with woods containing tanning agents such as | 904885 | $5,0 \times 80$ | TX25 | 200 |
| cumarú, oak, merbau, robinia, etc. | 90488 | 5,0×90 | TX25 | 100 |
| Magnetised | 904011 | $5,0 \times 100$ | TX25 | 100 |
| Stainless steel in accordance with DIN 10088 | 904012 | $6,0 \times 60$ | TX30 | 100 |
| The screw is suitable for use in timber-timber ioints in outdoor | 904013 | $6,0 \times 70$ | TX30 - | 100 |
| installations and is used in garden, façade and balcony construction | 904014 | 6,0 080 | TX30 | 100 |
| instalarions and is used in garden, façade and balcony construction | 904015 | 6,0×90 | TX30 - | 100 |
|  | 904016 | $6,0 \times 100$ | TX30 - | 100 |
|  | 904017 | 6,0 120 | TX30 - | 100 |
|  | 904018 | $6,0 \times 140$ | TX30 | 100 |
|  | 904019 | $6,0 \times 160$ | TX30 • | 100 |


| Paneltwistec $\quad$ (E) | Art. no. | Dimensions [mm] | Drive | PU |
| :---: | :---: | :---: | :---: | :---: |
| Flanged button-head, hardened stainless steel | 945778 | 8,0×80 | TX40 - | 50 |
|  | 945770 | 8,0 $\times 100$ | TX40 - | 50 |
| ( ) | 945271 | $8,0 \times 120$ | TX40 - | 50 |
|  | 94572 | 8,0 140 | TX40 - | 50 |
|  | 945364 | $8,0 \times 160$ | TX40 - | 50 |
| Rost ${ }^{\circ}$ | 945365 | $8,0 \times 180$ | TX40 - | 50 |
| fret | 945366 | $8,0 \times 200$ | TX40 | 50 |
|  | 945367 | 8,0×220 | TX40 - | 50 |
|  | 945368 | 8,0 240 | TX40 | 50 |
| ADVANTAGES | 945369 | 8,0x 260 | TX40 | 50 |
| - Also suitable for fastening over-rafter insulation | 945370 | $8,0 \times 280$ | TX40 | 50 |
| - The larger head diameter allows for considerably higher torque | 945371 | 8,0x 300 | TX40 - | 50 |
| and head pull-hrough capacity | 945372 | 8,0x 320 | TX40 - | 50 |
| . This makes for better use of the screw's tensile load-bearing strength | 945373 | 8,0x 340 | TX40 | 50 |
|  | 945374 | 8,0x 360 | TX40 - | 50 |
|  | 945375 | 8,0x 380 | TX40 - | 50 |
|  | 945376 | 8,0x 400 | TX40 - | 50 |


| Paneltwistec AG | \% C E | Art. no. | Dimensions [mm] | Drive | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Flanged button-head, hardened stainless steel | 为 | 975772 | 6,0 $\times 60$ | TX30 | 100 |
|  |  | 975773 | 6,0 $\times 80$ | TX30 | 100 |
|  |  | 97577 | $6,0 \times 100$ | TX30 | 100 |
| Thendernerness:- |  | 975775 | $6,0 \times 120$ | TX30 | 100 |
|  |  | 975776 | $6,0 \times 140$ | TX30 | 100 |
| Eidelstatio |  | 97577 | $6,0 \times 160$ | TX30 ${ }^{\circ}$ | 100 |

## Gurotec



| Paneltwistec A2 | \% C | Art. no. | Dimensions [mm] | Drive | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Flanged button-head, Stainless steel |  | 903211 | $8,0 \times 80$ | TX40 ${ }^{\circ}$ | 50 |
|  |  | 903212 | 8,0 $\times 100$ | TX40 - | 50 |
|  |  | 903213 | $8,0 \times 120$ | TX40 - | 50 |
|  | $\longrightarrow$ | 903214 | 8,0 $\times 140$ | TX40 - | 50 |
|  |  | 903215 | 8,0 $\times 160$ | TX40 - | 50 |
| Edelstany |  | 903216 | 8,0 $\times 180$ | TX40 - | 50 |
| Rost |  | 903217 | 8,0 200 | TX40 | 50 |
| rret |  | 903218 | 8,0 $\times 220$ | TX40 - | 50 |
|  |  | 903219 | 8,0 240 | TX40 - | 50 |
| ADVANTAGES |  | 903220 | 8,0 $\times 260$ | TX40 - | 50 |
| - Limited resistance to acid |  | 903221 | $8,0 \times 280$ | TX40 | 50 |
|  |  | 903222 | 8,0 $\times 300$ | TX40 | 50 |
| - Not suitable for atmospheres containing chlorine |  | 903223 | 8,0 $\times 320$ | TX40 | 50 |
|  |  | 903224 | 8,0 $\times 340$ | TX40 - | 50 |
|  |  | 903225 | 8,0 $\times 360$ | TX40 | 50 |
|  |  | 903226 | 8,00 380 | TX40 - | 50 |
|  |  | 903227 | $8,0 \times 400$ | TX40 - | 50 |



SAWTEC
WOOD CONSTRUCTION SCREW mADE OF HARDENED CARBON STEEL


## ADVANTAGES OF THE SCREW HEAD

. Saw teeth under the head reduce chip placement

- No hammering of the screws when screwing in due to TX-Drive
- Low splitting effect

Better "bite" of the screw

## ADVANTAGES FRICTION PART

- Friction part creates space for the shank, thereby reduces the insertion resistance


## ADVANTAGES THREAD

- The coarse thread is equipped with sharply rolled flanks to the tip
- Enables fast screwing-in


## ADVANTAGES DAG TIP

The special geometry of the DAG screw tip ensures a reduction of the screwing torque and also leads to a lower spliting effect when screwing-in

## DESCRIPTION

The SawTec is a wood construction screw with a special screw tip and saw teeth below the head. The screw has a double-stage cylinder head. The special geometry of the screw tip reduces the screwing torque and also leads to a lower spliting effect when screwing in.


SawTec


| Art. no. | Dimensions [mm] | Drive | PU |
| :---: | :---: | :---: | :---: |
| 954115 | $5,0 \times 40$ | TX25 • | 200 |
| 954117 | $5,0 \times 50$ | TX25 • | 200 |
| 954118 | $5,0 \times 60$ | TX25 • | 200 |
| 954119 | $5,0 \times 70$ | TX25 • | 200 |
| 954120 | $5,0 \times 80$ | TX25 • | 200 |
| 954121 | $5,0 \times 90$ | TX25 • | 200 |
| 954122 | $5,0 \times 100$ | TX25 • | 200 |
| 954124 | $5,0 \times 120$ | TX25 • | 200 |
| 954128 | $6,0 \times 60$ | TX30 - | 100 |
| 954129 | $6,0 \times 70$ | TX30 - | 100 |
| 954130 | $6,0 \times 80$ | TX30 - | 100 |
| 954131 | $6,0 \times 100$ | TX30 - | 100 |
| 954133 | $6,0 \times 120$ | TX30 - | 100 |
| 954135 | $6,0 \times 140$ | TX30- | 100 |
| 954137 | $6,0 \times 160$ | TX30- | 100 |
| 954138 | $6,0 \times 180$ | TX30 - | 100 |
| 954145 | $8,0 \times 80$ | TX40 - | 50 |
| 954146 | $8,0 \times 100$ | TX40 - | 50 |
| 954147 | $8,0 \times 120$ | TX40 - | 50 |
| 954148 | $8,0 \times 140$ | TX40 - | 50 |
| 954149 | $8,0 \times 160$ | TX40 - | 50 |
| 954150 | $8,0 \times 180$ | TX40 - | 50 |
| 954151 | $8,0 \times 200$ | TX40 - | 50 |
| 954152 | $8,0 \times 220$ | TX40 - | 50 |
| 954153 | $8,0 \times 240$ | TX40 - | 50 |
| 954154 | $8,0 \times 260$ | TX40 - | 50 |
| 954155 | $8,0 \times 280$ | TX40 - | 50 |
| 954156 | $8,0 \times 300$ | TX40 - | 50 |
| 954157 | $8,0 \times 320$ | TX40 - | 50 |
| 954158 | $8,0 \times 340$ | TX40 - | 50 |
| 954159 | $8,0 \times 360$ | TX40 - | 50 |
| 954160 | $8,0 \times 380$ | TX40 - | 50 |
| 954161 | $8,0 \times 400$ | TX40 - | 50 |
| 954162 | $10,0 \times 100$ | TX50 • | 50 |
| 954163 | $10,0 \times 120$ | TX50 • | 50 |
| 954164 | $10,0 \times 140$ | TX50 • | 50 |
| 954165 | $10,0 \times 160$ | TX50 • | 50 |
| 954166 | $10,0 \times 180$ | TX50 • | 50 |
| 954167 | $10,0 \times 200$ | TX50 • | 50 |
| 954168 | $10,0 \times 220$ | TX50 • | 50 |
| 954169 | $10,0 \times 240$ | TX50 • | 50 |
| 954170 | $10,0 \times 260$ | TX50 • | 50 |
| 954171 | $10,0 \times 280$ | TX50 • | 50 |
| 954172 | $10,0 \times 300$ | TX50 • | 50 |
| 954173 | $10,0 \times 320$ | TX50 • | 50 |
| 954174 | $10,0 \times 340$ | TX50 • | 50 |
| 954175 | $10,0 \times 360$ | TX50 • | 25 |
| 954176 | $10,0 \times 380$ | TX50 • | 25 |
| 954177 | $10,0 \times 400$ | TX50 • | 25 |

## Gurotec

## TECHNICAL INFORMATION <br> SAWTEC, CYLINDER HEAD, BLUE GALVANISED

| Dimensions |  |  |  | Extraction resistance | Head pull-through resistance | Wood-Wood shearing |  |  |  | Steel-Wood shearing |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\stackrel{-\frac{\mathrm{dk}}{1}}{\stackrel{-}{\square}}$ |  |  |  |  |  | $V\left(\alpha=0^{\circ}\right)$ <br> $V\left(\alpha=0^{\circ}\right)$ <br> $V\left(\alpha=0^{\circ}\right)$ <br> $V\left(\alpha=90^{\circ}\right)$ |  |  |  | v. <br> $V\left(\alpha=0^{\circ}\right)$ <br> v $\qquad$ <br> V $\left(\alpha=90^{\circ}\right.$ |  |  |
| $\begin{aligned} & \mathrm{dl} \mathrm{xL} \\ & {[\mathrm{~mm}]} \end{aligned}$ | $\begin{gathered} \mathrm{dk} \\ {[\mathrm{~mm}]} \end{gathered}$ | $\begin{gathered} A D \\ {[\mathrm{~mm}]} \end{gathered}$ | $\begin{gathered} \text { It } \\ {[\mathrm{mm}]} \end{gathered}$ | $F_{a x}, 90$,Rk [kN] | $F_{a x, h e a d, R k}$ <br> [kN] | Fla,Rk [kN] | Fla,Rk [kN] | Fla,Rk [kN] | Fla,Rk [kN] | $\begin{gathered} \dagger \\ {[\mathrm{mm}]} \end{gathered}$ | Fla,Rk [kN] | Fla,Rk [kN] |
|  |  |  |  |  |  |  |  | ${ }^{\prime A D}=0^{\circ}$ | $\angle A D=90^{\circ}$ |  |  |  |
|  |  |  |  |  |  | $\alpha=0^{\circ}$ | $\alpha=90^{\circ}$ | $\alpha_{\text {EE }}=90^{\circ}$ | $\alpha \mathrm{E}=0^{\circ}$ |  | $\alpha=0^{\circ}$ | $\alpha=90^{\circ}$ |
| $5,0 \times 40$ | 10,5 | 16 | 24 | 1,45 | 1,10 | 1,09 |  |  |  | 2 |  | ,44 |
| 5,0 50 | 10,5 | 20 | 30 | 1,82 | 1,10 | 1,22 |  |  |  | 2 |  | 1,67 |
| 5,0×60 | 10,5 | 24 | 36 | 2,18 | 1,10 | 1,31 |  |  |  | 2 |  | ,76 |
| 5,0x70 | 10,5 | 28 | 42 | 2,54 | 1,10 | 1,41 |  |  |  | 2 |  | 1,85 |
| $5,0 \times 80$ | 10,5 | 32 | 48 | 2,90 | 1,10 | 1,49 |  |  |  | 2 |  | ,94 |
| $5,0 \times 90$ | 10,5 | 36 | 54 | 3,27 | 1,10 | 1,49 |  |  |  | 2 |  | ,03 |
| 5, $\times 100$ | 10,5 | 40 | 60 | 3,63 | 1,10 | 1,49 |  |  |  | 2 |  | , 12 |
| 5,0×120 | 10,5 | 60 | 60 | 3,63 | 1,10 | 1,49 |  |  |  | 2 |  | , 12 |
| 6,0×60 | 13,0 | 24 | 36 | 2,46 | 1,69 | 1,70 |  |  |  | 2 |  | ,26 |
| 6,0x70 | 13,0 | 28 | 42 | 2,87 | 1,69 | 1,81 |  |  |  | 2 |  | ,36 |
| 6,0×80 | 13,0 | 32 | 48 | 3,28 | 1,69 | 1,92 |  |  |  | 2 |  | 2,46 |
| 6,0×90 | 13,0 | 36 | 54 | 3,69 | 1,69 | 2,4 |  |  |  | 2 |  | 2,57 |
| $6,0 \times 100$ | 13,0 | 40 | 60 | 4,10 | 1,69 | 2,07 |  |  |  | 2 |  | 2,67 |
| 6,0×110 | 13,0 | 50 | 60 | 4,10 | 1,69 | 2,07 |  |  |  | 2 |  | 2,67 |
| 6, $6 \times 120$ | 13,0 | 60 | 60 | 4,10 | 1,69 | 2,07 |  |  |  | 2 |  | 2,67 |
| 6,0×130 | 13,0 | 60 | 70 | 4,9 | 1,69 | 2,07 |  |  |  | 2 |  | 2,84 |
| 6,0×140 | 13,0 | 70 | 70 | 4,79 | 1,69 | 2,07 |  |  |  | 2 |  | 2,84 |
| 6,0×150 | 13,0 | 80 | 70 | 4,79 | 1,69 | 2,07 |  |  |  | 2 |  | 2,84 |
| $6,0 \times 160$ | 13,0 | 90 | 70 | 4,9 | 1,69 | 2,07 |  |  |  | 2 |  | 2,84 |
| 6,0×180 | 13,0 | 110 | 70 | 4,9 | 1,69 | 2,07 |  |  |  | 2 |  | 2,84 |

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## Gurotec



Calculation according to $\mathrm{ETA}-\mathrm{Il} / \mathrm{OO24}$. Wood density $\mathrm{\rho k}=350 \mathrm{~kg} / \mathrm{m}^{3}$. All mechanical valves provided should be viewed as subject to the assumptions that have been made and represent example calculations.
All values are calculated minimum values and are subject to typographical and printing errors.
a) The characteristic values of the load-bearing capacity Rk cannot be treated as equivalent to the max. possible load (the max. force). Characterisicic values of the lood-bearing capacity Rk should be reduced to dimensioning values Rd

Example:
Characterisic value for constant load (deed weight) $G_{k}=2,00 \mathrm{kN}$ and variable load (e. g. snow lood) $Q_{k}=3,00 \mathrm{kN}$. $\mathrm{kmod}^{2}=0,9 \cdot \gamma_{\mathrm{M}}=1,3$.
$\rightarrow$ Dimensioning value of the lood $\mathrm{Ed}_{\mathrm{d}}=2,00 \cdot 1,35+3,00 \cdot 1,5=7,20 \mathrm{kN}$.
The load-bearing capacity of the joint is therefore considered to have been demonstrated if $\mathrm{R}_{\mathrm{d}} \geq \mathrm{E}_{\mathrm{d}} \rightarrow \min \mathrm{R}_{\mathrm{k}}=\mathrm{R}_{\mathrm{d}} \cdot \gamma_{\mathrm{M}} / \mathrm{kmod}_{\bmod }$
i.e. the characteristic minimum value is calculated based on: $\min \mathrm{R}_{\mathrm{k}}=\mathrm{R}_{d} \cdot \gamma \mathrm{M} / \mathrm{kmod} \rightarrow \mathrm{Rk}=7,20 \mathrm{kN} \cdot 1,3 / 0,9=10,40 \mathrm{kN} \rightarrow$ comparison with table values.

Please note: These are planning cids. Projects must only be calculated by outhorised persons.

## Gurotec

## TOPDUO ROOFING SCREW

## THE WOOD-CONSTRUCTION SCREW FOR ALL OVER-RAFTER INSULATION SYSTEMS

## ADVANTAGES

Double thread allows the fastening of compression-resistant and non-compression-resistant insulation materials

- Due to the high pull-out resistance, the screw is
universally suitable for many applications in timber construction
Resistant to mechanical stress
- No hammering of the screws when screwing-in due to TX-Drive


## ADVANTAGES OF THE SCREW TIP



## DESCRIPTION

The Topduo roofing screw can be used to fasten both compression-resistant and non-compression-resistant above-rafter insulation. The high pull-out resistance in both connecting timbers also makes the TopDuo roofing screw suitable for many other applications in timber construction. The screw has a double thread and is available with a flanged buttonhead and cylinder head.



Topduo flanged-button head for fastening insulation material.

| Topduo roofing screw \% C E | Art. no. | Dimensions [mm] | Length [mm] ${ }^{\text {a }}$ | Drive | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Flanged button-head, special coated | 945870 | 8,0×165 | 60/80 | TX40 - | 50 |
|  | 94587 | $8,0 \times 195$ | 60/100 | TX40 - | 50 |
| (then | 945813 | 8,0×225 | 60/100 | TX40 - | 50 |
|  | 945814 | 8,0×235 | 60/100 | TX40 - | 50 |
|  | 945815 | 8,0×255 | 60/100 | TX40 - | 50 |
| ADVANTAGES/PROPERTIES | 945816 | 8,0x275 | 60/100 | TX40 | 50 |
| Can also be used for many other applications in timber-frame construction thanks to its high extraction resistance | 945817 | 8,0×302 | 60/100 | TX40 | 50 |
|  | 945818 | 8,0×335 | 60/100 | TX40 | 50 |
|  | 945819 | 8,0x365 | 60/100 | TX40 - | 50 |
|  | 945820 | 8,0× 397 | 60/100 | TX40 - | 50 |
|  | 945821 | 8,0 435 | 60/100 | TX40 | 50 |
|  | 945843 | 8,0x 472 | 60/100 | TX40 - | 50 |
|  | a) Under-head thread/drive thread |  |  |  |  |


| Topduo roofing screw | Art. no. | Dimensions [mm] | Length [mm] ${ }^{\text {a }}$ | Drive | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Cylinder head, special coated | 945956 | $8,0 \times 225$ | 60/100 | TX40 | 50 |
|  | 945965 | 8,0×235 | 60/100 | TX40 - | 50 |
| - | 945957 | $8,0 \times 255$ | 60/100 | TX40 | 50 |
|  | 945958 | 8,0 $\times 275$ | 60/100 | TX40 - | 50 |
| ADVANTAGES / PROPERTIES | 945960 | 8,0×302 | 60/100 | TX40 | 50 |
|  | 945961 | 8,0×335 | 60/100 | TX40 | 50 |
| Can also be used for many other applications in timber-frame construction thanks to its high extraction resistance | 945962 | 8,0×365 | 60/100 | TX40 - | 50 |
|  | 94596 | 8,0×397 | 60/100 | TX40 | 50 |
|  | 945964 | $8,0 \times 435$ | 60/100 | TX40 ${ }^{\circ}$ | 50 |
|  | a) Under-head thread/drive thread |  |  |  |  |



## Gurotec



Fastening options

$65^{\circ}$ screw connection


[^2]
## CALCULATING QUANTITIES FOR TOPDUO ROOFING SCREW STATICALLY NON.PRESSURE-RESISTANT INSULATING MATERIALS AT $\sigma 10 \%$ < 50 KPA

## Design sample for specified assumptions, project-related design may yield significantly more favourable results

| Number of Topduo screws per m² |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Insulation thickness | 40 | 60 | 80 | 100 | 120 | 140 | 140 | 160 | 180 | 200 | 220 | 240 | 260 | 280 |
| Boarding thit | hickness Oon rafters) | 24 | 24 | 24 | 24 | 24 | - | 24 | 24 | 24 | 24 | 24 | 24 | 24 | 24 |
| Dimensions Topduo Flanged button-head acc. (ylinder-headd |  | $8 \times 165^{\text {b }}$ | $8 \times 195^{\text {b }}$ | $8 \times 225$ | $8 \times 235$ | $8 \times 255$ | $8 \times 275$ | $8 \times 302$ | $8 \times 335$ | 8×335 | $8 \times 365$ | $8 \times 365$ | $8 \times 397$ | $8 \times 435$ | $8 \times 435$ |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] |
|  | $0^{\circ} \leq D W \leq 10^{\circ}$ | 2,20 | 2,20 | 2,38 | 2,38 | 2,38 | 2,38 | 2,38 | 2,29 | 2,29 | 2,48 | 3,01 | 3,57 | 4,08 | 4,76 |
|  | $10^{\circ}<$ DN $\leq 25^{\circ}$ | 2,38 | 2,38 | 2,60 | 2,60 | 2,60 | 2,60 | 2,60 | 2,60 | 2,60 | 3,17 | 3,81 | 4,40 | e) | e) |
|  | $25^{\circ}<\mathrm{DN} \leq 40^{\circ}$ | 2,72 | 2,72 | 3,01 | 3,1 | 3,01 | 3,01 | 3,01 | 3,01 | 3,01 | 3,57 | 4,40 | 5,19 | e) | e) |
|  | $40^{\circ}<\mathrm{DN} \leq 60^{\circ}$ | 2,86 | 3,01 | 3,17 | 3,17 | 3,36 | 3,36 | 3,36 | 3,36 | 3,36 | 3,57 | 4,40 | 5,19 | e) | e) |
| $\begin{aligned} & \text { Snow lood zone 3t) } \\ & \text { Wind zone 29) } \\ & \text { Alfitude WV } \\ & \leq 600 \mathrm{~m} \end{aligned}$ | $0^{\circ} \leq 0 W \leq 10^{\circ}$ | 1,79 | 1,79 | 1,97 | 2,04 | 2,04 | 2,04 | 2,04 | 2,12 | 2,60 | 3,81 | 4,40 | 5,19 | e) | e) |
|  | $10^{\circ}<\mathrm{DN} \leq 25^{\circ}$ | 2,29 | 2,29 | 2,48 | 2,60 | 2,60 | 2,60 | 2,60 | 2,72 | 3,36 | 4,76 | e) | e) | e) | e) |
|  | $25^{\circ}<\mathrm{DW} \leq 40^{\circ}$ | 2,38 | 2,48 | 2,72 | 2,72 | 2,72 | 2,86 | 2,86 | 2,86 | 3,57 | 5,19 | e) | e) | e) | e) |
|  | $40^{\circ}<\mathrm{DN} \leq 60^{\circ}$ | 2,60 | 2,60 | 2,86 | 2,86 | 2,86 | 2,86 | 2,86 | 3,01 | 3,57 | 5,19 | e) | e) | e) | e) |

a) Quantity always refers to the less favourable valve from Topduo Flanged button-head and Cylinder-head
b) Topduo Flanged button-head only, () Includes snow lood zones 1,2 and $2^{*}$, d) Includes all wind zones aparf from North Sea islands
e) Use of our project assessment service is recommended. The design examples listed here represent unfavourable, i.e. statically safe, instances.
f) Includes snow load zones 1,2 and 3, g) Includes wind zones 1 and 2 (inland)

Further assumptions:
Design with ECS design software in accordance with EA- $11 / 0024$; screw-in angle $65^{\circ}$; gabled roof; ridge height above ground max. 18 m ; gross density insulation $1,50 \mathrm{kN} / \mathrm{m}^{3}$; rafters $\mathrm{C} 248 / \geq 12 \mathrm{~cm}$; counter batten $\mathrm{C} 244 / 6 \mathrm{~cm}$; rafter centre distance $0,70 \mathrm{~m}$; roofing dead weight $0,55 \mathrm{kN} / \mathrm{m}^{2}$; snow guard available; quantity calculation regarding wind pressure after the most unfavourable roof area.
All listed values should be viewed as subject to the assumptions that have been made. They therefore represent example calculations and are subject to typographical and printing errors.
Please note: These are planning aids. Projects must only be calculated by authorised persons.

## CALCULATING QUANTITIES FOR TOPDUO ROOFING SCREW <br> STATICALLY PRESSURE-RESISTANT INSULATING MATERIALS AT $\sigma_{10} \% \geq 50$ KPA

## Design sample for specified assumptions, project-related design may yield significantly more favourable results

Number of Topduo screws per $\mathrm{m}^{2}$

|  | Insulation thickness | 40 | 60 | 80 | 100 | 120 | 140 | 160 | 180 | 200 | 220 | 240 | 260 | 280 | 300 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Boarding thi | hickness (on rafters) | 24 | 24 | 24 | 24 | 24 | 24 | 24 | 24 | 24 | 24 | 24 | 24 | 24 | 24 |
| Dimensions Topduo Flanged button-heed acc. (ylinder-headd ${ }^{(0)}$ |  | $8 \times 195^{\text {b }}$ | $8 \times 225$ | $8 \times 235$ | $8 \times 255$ | $8 \times 275$ | $8 \times 302$ | $8 \times 335$ | $8 \times 335$ | $8 \times 365$ | $8 \times 365$ | $8 \times 397$ | $8 \times 435$ | $8 \times 435$ | $8 \times 472^{\text {b }}$ |
|  |  | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] |
| Snow lood zone 2 ${ }^{*}$ (), Wind zone $4^{\text {d }}$ Altitude NN $\leq 285 \mathrm{~m}$ | $0^{\circ} \leq \mathrm{DN} \leq 10^{\circ}$ | 1,96 | 2,06 | 2,06 | 2,06 | 2,06 | 2,06 | 2,06 | 2,06 | 2,06 | 2,06 | 2,12 | 1,80 | 2,40 | 2,32 |
|  | $10^{\circ}<\mathrm{DN} \leq 25^{\circ}$ | 2,11 | 2,05 | 1,97 | 1,94 | 1,97 | 1,90 | 1,85 | 2,14 | 2,01 | 2,74 | 2,57 | 2,38 | 3,23 | 2,93 |
|  | $25^{\circ}<\mathrm{DN} \leq 40^{\circ}$ | 2,48 | 2,41 | 2,28 | 2,35 | 2,41 | 2,35 | 2,18 | 2,67 | 2,49 | 3,48 | 3,22 | 2,96 | 4,42 | 3,79 |
|  | $40^{\circ}<\mathrm{DN} \leq 60^{\circ}$ | 2,31 | 2,30 | 2,56 | 2,65 | 2,74 | 2,65 | 2,42 | 2,9 | 2,74 | 4,00 | 3,70 | 3,48 | 4,87 | 4,47 |
| Snow load zone $3^{\text {(t) }}$ Wind zone ${ }^{\text {g }}$ ) Altitude NN $\leq 400 \mathrm{~m}$ | $0^{\circ} \leq \mathrm{DN} \leq 10^{\circ}$ | 2,65 | 2,54 | 2,39 | 2,34 | 2,26 | 2,23 | 2,34 | 2,34 | 2,16 | 2,46 | 2,32 | 2,19 | 2,86 | 2,65 |
|  | $10^{\circ}<\mathrm{DN} \leq 25^{\circ}$ | 4,04 | 3,81 | 3,55 | 3,33 | 3,33 | 3,15 | 3,15 | 2,99 | 2,99 | 3,66 | 3,37 | 3,06 | 4,37 | 3,74 |
|  | $25^{\circ}<\mathrm{DN} \leq 40^{\circ}$ | 4,46 | 4,16 | 3,84 | 3,58 | 3,58 | 3,58 | 3,37 | 3,37 | 3,37 | 4,67 | 4,20 | 3,92 | e) | e) |
|  | $40^{\circ}<\mathrm{DN} \leq 60^{\circ}$ | 3,55 | 3,26 | 3,26 | 3,26 | 3,44 | 3,26 | 2,96 | 3,66 | 3,44 | e) | 4,67 | 4,27 | e) | e) |

a) Quantity always refers to the less favourable valve from Topduo Flanged button-head and Cylinder-head
b) Topduo Flanged button-head only, () Includes snow load zones 1,2 and $2^{*}$ each with snow guard, d) Includes all wind zones aparif from North Sea islands
e) Use of our project assessment service is recommended. The design examples listed here represent unfavourabbe, i.e. statically safe, instances.
f) Includes snow load zones 1,2 and 3 , g) Includes wind zones 1 and 2 (inland)

Further assumptions:
Design with ECS design software in accordance with EAA-11/0024; screw-in angle roof thruss screw $65^{\circ} /$ wind pressure screw $90^{\circ}$; gabled roof; ridge height above ground max. 18 m ; gross density insulation $1,50 \mathrm{kN} / \mathrm{m}^{3}$; rafters $\mathrm{C} 248 / \geq 12 \mathrm{~cm}$; counter batten C 24
$4 / 6 \mathrm{~cm} ;$ rafter centre distance $0,70 \mathrm{~m}$; roofing dead weight $0,55 \mathrm{kN} / \mathrm{m}^{2}$; snow guard available; quantity calculation with respect to wind pressure after the most unfavourable roof area.
All listed values should be viewed as subject to the assumptions that have been made. They therefore represent example calculations and are subject to typographical and printing errors.
Please note: These are planning aids. Projects must only be calculated by authorised persons.
Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by outhorised
persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of sability. We will be happy to refer you to someone.

## EuroTec calculation service

## On-rafter insulation according to ETA-1 1/0024

by phone 02331 6245-444 • by fax 02331 6245-200 • by e-mail technik@eurotec.team

Please contact our technical department or use the free calculation services in the service section of our website.
Contact
Trader:

Contact person:
e-mail: $\qquad$

Project: $\qquad$

## Project details



[^3]


Further products

| Lifing anchor und ball supporting bolt | $136-147$ |
| :--- | :--- |
| Ideefix | $148-155$ |
| SonoTec sond insulation cork | $156-167$ |
| Bolt anchor | $168-171$ |
| Silent EPDM decoupling profile | $172-173$ |
| Ecktec | $174-175$ |

## Gurotec

## LIFTING ANCHOR UND BALL SUPPORTING BOLT

FOR THE TRANSPORT OF PREFABRICATED WALL MODULES

## ADVANTAGES

- Easy assembly
- Reusable corpus
- Can be used in solid structural timber and cross-laminated timber
- Especially made for transporting large loads
- $360^{\circ}$ rotation of the load is possible



## DESCRIPTION

The Lifting anchor is specifically designed for use with a ball supporting bolt. The lifting anchor can be used to transport prefabricated wall modules. The fact that it is sed with screws means the anchor can be used several times. 8 screws are included in delivery.

## INSTRUCTIONS FOR USE

The product only works in combination with the ball supporting bolt (Ø: 20 $\mathrm{mm}, \mathrm{l}: 50 \mathrm{~mm}$ ) provided for this purpose.
The specifications of the product data sheet must be observed!
Please consult with our technical department and download the product data sheet from our website www.eurotec.team runter.

Please note! This product is subject to important conditions! Please observe the instructions of use. To be able to ensure the safety of transport, the screws must be replaced after use.



Self-alignment of the leg in the direction of force

ONLY TO BE CARRIED OUT BY QUALIFIED PROFESSIONALS!
Minimum width of the material:
120 mm
Minimum thickness of the material: 60 mm
Bis 80 mm material thickness: Through bore
From $80 \mathrm{~mm}+$ :
Blind hole / pocket

| Art. no. | Name | Dimensions [mm] ${ }^{\text {a/ }}$ | Material | PU |
| :---: | :---: | :---: | :---: | :---: |
| 94892 | lifiting anchor | $60 \times 40$ | S/235 | 4 |
| a) Height X Dimeter |  |  |  |  |
| *Delivery incl. screws |  |  |  |  |


| Art. no. | Name | Dimensions $[\mathrm{mm}]^{00}$ | Material | F1 [kN] | F2 [kN] | F3 [kN] | PU |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: |
| 944893 | Ball supporing bolt | $50 \times 20$ | 5 S235 | 10 | 8,5 | 6,5 | 1 |
| a) Heightx Diameter |  |  |  |  |  |  |  |

## Gurotec



TRANSPORTATION OF SMALLER ELEMENTS


## DESCRIPTION LIFTING ANCHOR MINI

The new Lifting anchor Mini is particularly suitable for transporting smaller loads, such as beam girders or supports. Since the inner diameter has been reduced from $\varnothing 20 \mathrm{~mm}$ (Liffing anchor) to $\varnothing 16 \mathrm{~mm}$ (Lifting anchor Mini), there is also a new smaller ball supporting bolt. A special feature of the Lifting anchor Mini is a stop on the upper edge, which simplifies installation in the case of a through hole.


| Art. no. | Name | Dimensions $[\mathrm{mm}]^{00}$ | Material | PU |
| :--- | :--- | :--- | :--- | ---: |
| 944901 | Litfing Anchor Mini | $49 \times 45$ | S235JR | 4 | a) Height $x$ Diameter

*Incl. 8 TX25 fully threaded screws TX25 6,0 x 60

| Art. no. | Name | Dimensions [mm] ${ }^{\text {a) }}$ | Material | Fl [kN] | F2 [kN] | F3 [kN] | PU |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 944893 | Ball supporting bolt | $50 \times 20$ | S/235 | 10 | 8,5 | 6,5 | 1 |
| a) Height x Diameter |  |  |  |  |  |  |  |



## Gurotec

## LIFTING ANCHOR

TECHNICAL INFORMATION

HORIZONTAL WALL OR BEAM: SET UPRIGHT, THEN LIFT

| CII- wall or beam |  |  |  |
| :---: | :---: | :---: | :---: |
| Connection in the | Connetor | Stop bracket $\beta$ | Total weight [kg] wih 2 strunds |
| End grain area | Lifing anchor $840 \mathrm{~mm}+8 \times \mathrm{VS5} 6 \times 60$ | $30^{\circ}$ | 444 |
|  |  | $45^{\circ}$ | 528 |
|  |  | $60^{\circ}$ | 569 |
|  |  | $75^{\circ}$ | 588 |
|  |  | $\beta$ | wilh nstrous |
|  |  | $90^{\circ}$ | nx297 |



Note
The tables illustrate the 'Setting upright and subsequently lifting a horizontal wall or horizontal beam' load case (lifting from a horizontal position leading to vertical suspension). The connectors are to be screwed flush, as well as at right angles to the surfaces of the narrow sides and side or end grain surfaces, into the centre plane of the components.

## VERTICAL WALL OR BEAM: LIFT

| CLI - wall or beam |  |  |  |
| :---: | :---: | :---: | :---: |
| Connection in the | Connector | Stop bracket $\beta$ | Total weight [kg] with 2 strands |
|  |  | $30^{\circ}$ | 601 |
|  |  | $45^{\circ}$ | 886 |
|  |  | $60^{\circ}$ | 1135 |
| Narrow surface | Lifting Anchor $040 \mathrm{~mm}+8 \times \mathrm{V} 556 \times 60$ | $75^{\circ}$ | 1311 |
|  |  | $\beta$ | bein Ströngen |
|  |  | $90^{\circ}$ | nx 688 |



## Note

The tables illustrate an example of "Liffing a standing wall or beam". (liffing from the horizontal to vertical suspension). The table values are only valid for lifting or assembly states.

CEILING LYING: LIFTING


## (TABLE ON THE NEXT PAGE)

Please note: Verity the assumptions made. The stated values, and type and number of joining devices are based on preiminaryy measurements. Projects are to be dimensioned exclusively by outhorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

## Gurotec



## Notes

The tables illustrates an example of "lifting of horizontal ceiling elements". (Liffing from the horizontal to vertical suspension). The connectors must be screwed in flush with the surface, plus perpendicular to the component surface.

## Warning!

Ball supporting bolts are designed for lifting and holding individual loads (not people!). In addition, they are not suitable for continuous load rotation. Contamination (e.g. grinding sludge, oil and emulsion deposits, dust, etc.) can impair the function of ball supporting bolts.

Damaged ball supporting bolts can put people's lives at risk. Before each use, ball supporting bolts must be inspected for visible defects (e.g. deformations, fractures, cracks, damage, missing balls, corrosion, function of the unlocking mechanism).

## Damaged ball supporting bolts must be mitdrawn from further use.

## Handling and loading

Press the button $(A)$ to release the balls. The balls are locked again by releasing the button (A).
Please note: The button $(A)$ is locked when the spring force has caused it to spring back to its original position. Do not press the button when loaded!
The load values F1 / F2 / F3 (see page 2) apply to liffing in a steel receptacle and x min.
$=1.5 \mathrm{~mm}$

## Maintenance

Ball supporting bolts must be subjected to a safety inspection by a competent person at least once a year.

## Visual inspection

Deformations, fractures, cracks, missing / damaged balls, corrosion, screw connection damage on the shackle.

## Functional test

The balls' locking and unlocking mechanism must close automatically by spring force. Full shackle mobility is guaranteed.


| ${ }_{1}$ | 1 | $\mathrm{d}_{2}$ | $\mathrm{d}_{3}$ | $\mathrm{d}_{4}$ | in. $1_{2}$ |  | 3 | 4 | , | 1 | ヶ | 8 | xmin | ** xmax | nox. OHII | $F_{1} \mathrm{lkH}$ | $\mathrm{F}_{2} \mathrm{ll}^{\text {c/ }}$ | \|il $\mathrm{F}_{3}$ | ${ }_{3} \mathrm{kl\mid}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | no ${ }^{50}$ | 25 |  | ${ }^{230}$ | 19, |  | ${ }_{3}{ }^{5}$ | 520 | 236 | ${ }_{3}$ | 56 | 140 | 15 | ${ }^{5}$ | n, 0 | 100 | is | ${ }_{6}$ |  |

## Original EC conformity mark

The product complies with the regulations set down in the EC Directive 2006/42/EC
Make: Ball supporting bolt
Type: EH 22350
Applied standards: DIN EN 13155

Please note: Verify the assumptions made. The stated values, and type and number of joining devices are hased on preliminary meassurements. Projects are to be dimensioned exclusively by authorised
persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

## Gurotec

## LIFTING ANCHOR MIN|

TECHNICAL INFORMATION

HORIZONTAL WALL OR BEAM: SET UPRIGHT, THEN LIFT

| CII- Wall or beam |  |  |  |
| :---: | :---: | :---: | :---: |
| Connection in the | Connector | Stop bracket | Total weight [kg] |
|  |  | $\beta$ | with 2 strands |
| End grain area | Lifing anchor mini $940 \mathrm{~mm}+8 \times \mathrm{VSS} 6 \times 60$ | $30^{\circ}$ | 248 |
|  |  | $45^{\circ}$ | 295 |
|  |  | $60^{\circ}$ | 318 |
|  |  | $75^{\circ}$ | 378 |
|  |  | $\beta$ | wilh nstrons |
|  |  | $90^{\circ}$ | nx166 |



## Note

The tables illustrate the 'Setting upright and subsequently lifting a horizontal wall or horizontal beam load case llifting from a horizontal position leading to vertical suspension). The connectors are to be screwed flush, as well as at right angles to the surfaces of the narrow sides and side or end grain surfaces, into the centre plane of the components.

## VERTICAL WALL OR BEAM: LIFT



CEILING LYING: LIFTING


## (TABLE ON THE NEXT PAGE)

Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by authorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

## Gurotec

| CLI - Ceiling |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Connection in the | Connectors | Stop bracket | Ground plan bracket | Total weight [kg] |
|  |  | $\beta$ | $\delta$ | with 4 strands |
| Side area | Liffing anchor + $8 \times$ VSS $6 \times 60$ | $30^{\circ}$ | $5^{\circ}$ | 714 |
|  |  |  | $15^{\circ}$ | 665 |
|  |  |  | $25^{\circ}$ | 595 |
|  |  |  | $35^{\circ}$ | 529 |
|  |  |  | $45^{\circ}$ | 475 |
|  |  |  | $60^{\circ}$ | 419 |
|  |  |  | $75^{\circ}$ | 389 |
|  |  | $45^{\circ}$ | $5^{\circ}$ | 1161 |
|  |  |  | $15^{\circ}$ | 1091 |
|  |  |  | $25^{\circ}$ | 986 |
|  |  |  | $35^{\circ}$ | 884 |
|  |  |  | $45^{\circ}$ | 799 |
|  |  |  | $60^{\circ}$ | 710 |
|  |  |  | $75^{\circ}$ | 645 |
|  |  | $60^{\circ}$ | $5^{\circ}$ | 1727 |
|  |  |  | $15^{\circ}$ | 1648 |
|  |  |  | $25^{\circ}$ | 1524 |
|  |  |  | $35^{\circ}$ | 1394 |
|  |  |  | $45^{\circ}$ | 1281 |
|  |  |  | $60^{\circ}$ | 1155 |
|  |  |  | $75^{\circ}$ | 1061 |
|  |  | $75^{\circ}$ | $5{ }^{\circ}$ | 2385 |
|  |  |  | $15^{\circ}$ | 2339 |
|  |  |  | $25^{\circ}$ | 2257 |
|  |  |  | $35^{\circ}$ | 2160 |
|  |  |  | $45^{\circ}$ | 2063 |
|  |  |  | $60^{\circ}$ | 1943 |
|  |  |  | $75^{\circ}$ | 1841 |
|  |  | $\beta$ | $\delta$ | with 2 strands |
|  |  | $30^{\circ}$ | $0^{\circ}$ | 721 |
|  |  |  | $90^{\circ}$ | 189 |
|  |  | $45^{\circ}$ | $0^{\circ}$ | 17 |
|  |  |  | $90^{\circ}$ | 322 |
|  |  | $60^{\circ}$ | $0^{\circ}$ | 1738 |
|  |  |  | $90^{\circ}$ | 530 |
|  |  | $75^{\circ}$ | $0^{\circ}$ | 2392 |
|  |  |  | $90^{\circ}$ | 920 |
|  |  | $\beta$ | б | wihn strands |
|  |  | $90^{\circ}$ | $0^{\circ}$ | nx688 |

## Note

The tables illustrate an example of "Lifting of horizontal ceiling elements". (Liffing from the horizontal to vertical suspension). The connectors must be screwed in flush with the surface, plus perpendicular to the component surface.

## OPERATING INSTRUCTIONS FOR THE BALL SUPPORTING BOLT

## Warning!

Ball supporting bolts are designed for lifting and holding individual loads (not people!). In addition, they are not suitable for continuous load rotation. Contamination (e.g. grinding sludge, oil and emulsion deposits, dust, etc.) can impair the function of ball supporting bolts.

Damaged ball supporting bolts can put people's lives at risk. Before each use, ball supporting bolts must be inspected for visible defects (e.g. deformations, fractures, cracks, damage, missing balls, corrosion, function of the unlocking mechanism).


Damaged ball supporting bolts must be withdrawn from further use.

## Handling and loading

Press the button (A) to release the balls. The balls are locked again by releasing the button (A).
Please note: The button $(A)$ is locked when the spring force has caused it to spring back to its original position. Do not press the button when loaded!
The load values F1 / F2 / F3 (see page 2) apply to liffing in a steel receptacle and x min. $=1.5 \mathrm{~mm}$

## Maintenance

Ball supporting bolts must be subjected to a safety inspection by a competent person at least once a year.

## Visual inspection

Deformations, fractures, cracks, missing / damaged balls, corrosion, screw connection damage on the shackle.

## Functional test

The balls' locking and unlocking mechanism must close automatically by spring force.
Full shackle mobility is guaranteed.


| $d_{1}$ | 1 | $d_{2}$ | $d_{3}$ | $d_{4} \mathrm{~min}$. | $I_{2}$ | 13 | 14 | 5 | $16$ | 17 | 18 | X min.* | x max.* | DHII | $F_{1} \mathrm{kN}{ }^{*}$ | $\mathrm{F}_{2} \mathrm{kN} *$ | $\mathrm{F}_{3} \mathrm{kN}{ }^{*}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20,0 | 50 | 24,50 | 30,0 | 25,00 | 19,70 | 36,5 | 52,0 | 32,6 | 36 | 56 | 114,0 | 1,5 | 25 | 20,0 | 10,0 | 8,5 | 6,5 |
| *with five-fold protection against breakage |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

*with five-fold protection against breakage

Original EC conformity mark
The product complies with the regulations set down in the EC Directive 2006/42/EC
Make: Ball supporting bolt
Type: EH 22350
Applied standards: DIN EN 13155

Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary meassurements. Projects are to be dimensioned exclusively by authorised persons in accordance with the State Building Sode. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

## Eurotec

## IDEEFIX

## HIDDEN WOOD CONNECTOR

## ADVANTAGES

- High load absorption for tensile and transverse loads
- Adjustable tension/detachable
- Universal application
- Low wood-weakening effect
- For single- or multiple-row serial connections
- High extraction resistance


## - Strong connection

- Maximization of load capacity
- Time and cost saving alternative
- Non-visible connections
- According to approval/ETA no predrilling for screws required (from screw lengths $>245 \mathrm{~mm}$ recommended


## INSTRUCTIONS FOR USE

The wood is predrilled for the IdeeFix. Then the IdeeFix is first inserted into the drill hole without screws. Then, thanks to its low splitting effect, the screws can be inserted without further predrilling. In the middle of the IdeeFix is a thread into which another screw can be inserted.



## CLT system angle with IdeeFix



## Gurotec

IDEEFIX 30/40/50
TECHNICAL INFORMATION


| Ideefix |  |  | Timber <br> Dimensions <br> Min. cross <br> section post |  | Tension connection with anti-twist element |  | Mortise joint with anti--twist element |  | Tensile load with threaded bolt |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ns |  |  |  | Drilling depth for post | Drilling depth for cross-piece | Drilling depth for post | Drilling depth for cross-piece | Perm. Values | Char. Values | Screw pattern |
| $d_{c}$ | $a_{g}$ | $V_{c}$ | [mm] | [mm] | [mm] | [mm] | [mm] | [mm] | $\mathrm{Nze}_{\text {ze }}$ [ kN$]$ | $\mathrm{Rl}_{1,1,1}[\mathrm{kN}]$ | pc. |
| 30 | M12 | 3 | 80 | 80 | 27 | . | 20 | 7 | 7,62 | 17,33 |  |
| 40 | M16 | 5 | 120 | 120 | 35 | . | 25 | 10 | 12,65 | 28,79 | 0 |
| 50 | M20 | 5 | 160 | 160 | 45 | - | 30 | 15 | 20,81 | 47,35 |  |
| 30 | M12 | 3 | 60 | 80 | 27 | - | 20 | 7 | 5,11 | 13,00 |  |
| 40 | M16 | 5 | 80 | 120 | 35 | - | 25 | 10 | 9,49 | 21,59 | 6 |
| 50 | M20 | 5 | 120 | 160 | 45 | - | 30 | 15 | 15,61 | 35,51 |  |
| 30 | M12 | 3 | 40 | 80 | 27 | - | 20 | 7 | 3,81 | 8,67 |  |
| 40 | M16 | 5 | 60 | 120 | 35 | - | 25 | 10 | 6,33 | 14,39 | \% |
| 50 | M20 | 5 | 80 | 160 | 45 | - | 30 | 15 | 10,41 | 23,67 |  |
| 30 | M12 | 3 | 60 | 60 | 27 | - | 20 | 7 | 3,81 | 8,67 |  |
| 40 | M16 | 5 | 80 | 80 | 35 | $\cdot$ | 25 | 10 | 6,33 | 14,39 | 8) |
| 50 | M20 | 5 | 120 | 120 | 45 | . | 30 | 15 | 10,41 | 23,67 |  |

dc is the diameter and the total height of the connector
$\mathrm{ag}_{\mathrm{g}}$ is the metric connection thread of the connector
vc is the height of the integrated anti-wwist system
Fully threaded screw, GoFix ${ }^{\mathbb{}}$ FK IF $305,0 \times 40 \mathrm{~mm}$ - IF $406,0 \times 60 \mathrm{~mm}$ - IF $508,0 \times 90 \mathrm{~mm}$
The connection is drawn together using a threaded rod or construction screw with a DIN 440 R washer
Tension connection as a mortise joint with simultaneous absorption of transverse forces
Rk characterisicic value calculated according to DIN $1052: 2004-08$ Timber pk $380 \mathrm{~kg} / \mathrm{m}^{3} \mathrm{Nze}$. recommended permissible load $\mathrm{R}, \mathrm{k} \times 0,8 \mathrm{kmod}: 1,3 \mathrm{ym}: 1,4$. Factor 1,4 average load safery factor
Please note: The stated values are planning aids. Projects must only be calculated by authorised persons.

## MAIN-SECONDARY BEAM



| Ideefix |  |  | Timber Dimensions |  | Timber Dimensions |  | Main-secondary beam with anti-twist element |  | Load-bearing capacity with threaded bolt |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dimensions [mm] |  |  | Min. cross section of secondary beam |  | Min. cross section of main beam |  | Drilling depth for SB | Drilling depth for MB | Perm. Values | Char. Values | Screw pattern |
| $d^{\text {d }}$ | $a_{g}$ | $\mathrm{v}_{\mathrm{c}}$ | w [mm] | $\mathrm{h}[\mathrm{mm}]$ | w [mm] | $\mathrm{h}[\mathrm{mm}]$ | [mm] | [mm] | Vze. [kN] | R23,k[kN] | pc. |
| 30 | M12 | 3 | 80 | 80 | 80 | 80 | 20 | 7 | 4,32 | 8,94 | $\checkmark$ |
| 40 | M16 | 5 | 120 | 120 | 120 | 120 | 25 | 10 | 6,98 | 14,66 | co |
| 50 | M20 | 5 | 160 | 160 | 160 | 160 | 30 | 15 | 10,88 | 21,09 |  |
| 30 | M12 | 3 | 60 | 80 | 60 | 80 | 20 | 7 | 3,50 | 1,97 | $\square$ |
| 40 | M16 | 5 | 80 | 120 | 80 | 120 | 25 | 10 | 5,63 | 12,80 | 0 |
| 50 | M20 | 5 | 120 | 160 | 120 | 160 | 30 | 15 | 8,65 | 19,68 |  |
| 30 | M12 | 3 | 40 | 80 | 40 | 80 | 20 | 7 | 3,50 | 7,97 |  |
| 40 | M16 | 5 | 60 | 120 | 60 | 120 | 25 | 10 | 5,63 | 12,80 | (8) |
| 50 | M20 | 5 | 80 | 160 | 80 | 160 | 30 | 15 | 8,65 | 19,68 |  |
| 30 | M12 | 3 | 60 | 60 | 60 | 60 | 20 | 7 | 3,50 | 1,97 | $\square$ |
| 40 | M16 | 5 | 80 | 80 | 80 | 80 | 25 | 10 | 5,63 | 12,80 | 2) |
| 50 | M20 | 5 | 120 | 120 | 120 | 120 | 30 | 15 | 8,65 | 19,68 |  |

$d_{c}$ is the diameter and the total height of the connector
ag is the metric connection thread of the connector
Vc is the height of the integrated anti--wist system
System - Fully threaded screw, GoFix ${ }^{\text {B }}$ FK IF $305,0 \times 40 \mathrm{~mm}$ - IF $406,0 \times 60 \mathrm{~mm}$ - IF $508,0 \times 90 \mathrm{~mm}$
The connection is drown together using a threaded rod or construction screw with a DIN 440 R washer
MB-SB connection as a mortise joint with simultaneous absorption of tensile forces
Rk characterisicic value calculated according to DIN $1052: 2004-08$ Timber pk $380 \mathrm{~kg} / \mathrm{m}^{3} \mathrm{Nze}$. recommended permissible load $\mathrm{R}, \mathrm{k} \times 0,8 \mathrm{kmod}: 1,3 \mathrm{ym}: 1,4$. Factor 1,4 average lood safery factor
Please note: The stated values are planning aids. Projects must only be calculated by authorised persons.

## Gurotec

## MAIN-SECONDARY BEAM, DOUBLE-SIDED CONNECTION, WITH FIXING SCREW



| IdeeFix |  |  | Timber <br> Dimensions <br> Min. cross section of secondary beam |  | TimberDimensionsMin. cross sectionof main beam |  | Main-secondary beam with anti-twist element |  | Load-bearing capacity with threaded bolt |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ons |  |  |  | Drilling depth for SB | Diilling depth for MB | Perm. Values | Char. Values | Screw pattern |
| $d^{\text {c }}$ | $\mathrm{ag}_{\mathrm{g}}$ | $V_{C}$ | w [mm] | h [mm] |  |  | w [mm] | h [mm] | [mm] | [mm] | $V_{\text {ze. }}$ [ $[\mathrm{kN}]$ | R23,k[kN] | p. |
| 30 | M12 | 3 | 80 | 80 | 80 | 80 | 20 | 10 | 2,34 | 5,32 |  |
| 40 | M16 | 5 | 120 | 120 | 120 | 120 | 25 | 15 | 3,60 | 8,19 |  |
| 50 | M20 | 5 | 160 | 160 | 160 | 160 | 30 | 20 | 5,03 | 11,44 |  |
| 30 | M12 | 3 | 60 | 80 | 60 | 80 | 20 | 10 | 2,34 | 5,32 | I |
| 40 | M16 | 5 | 80 | 120 | 80 | 120 | 25 | 15 | 3,60 | 8,19 |  |
| 50 | M20 | 5 | 120 | 160 | 120 | 160 | 30 | 20 | 5,03 | 11,44 |  |
| 30 | M12 | 3 | 40 | 80 | 40 | 80 | 20 | 10 | 2,34 | 5,32 |  |
| 40 | M16 | 5 | 60 | 120 | 60 | 120 | 25 | 15 | 3,60 | 8,19 | (8) |
| 50 | M20 | 5 | 80 | 160 | 80 | 160 | 30 | 20 | 5,03 | 11,44 |  |
| 30 | M12 | 3 | 60 | 60 | 60 | 60 | 20 | 10 | 2,34 | 5,32 |  |
| 40 | M16 | 5 | 80 | 80 | 80 | 80 | 25 | 15 | 3,60 | 8,19 | (8) |
| 50 | M20 | 5 | 120 | 120 | 120 | 120 | 30 | 20 | 5,03 | 11,44 |  |

de is the diameter and the total height of the connector
ag is the metric connection thread of the connector
Vcis the height of the integrated anti-wwist system
System - Fully threaded screw, Gofix ${ }^{\circledR}$ FK IF $305,0 \times 40 \mathrm{~mm}$ - IF $406,0 \times 60 \mathrm{~mm}$ - IF $508,0 \times 90 \mathrm{~mm}$
Position retention using Gofix ${ }^{\text {® }}$ SK IF $305,0 \times 100 \mathrm{~mm}$, IF $406,0 \times 140 \mathrm{~mm}$, IF $508,0 \times 160 \mathrm{~mm}$
MB-SB connection as mortise joint for double-sided connection of secondary beam
Rk characteristic value calculated according to DIN $1052: 2004-08$ Timber pk $380 \mathrm{~kg} / \mathrm{m}^{3} \mathrm{Nze}$. recommended permissible load $\mathrm{R}, \mathrm{k} \times 0,8 \mathrm{kmod}: 1,3 \mathrm{ym}: 1,4$. Favtor 1,4 average lood safety factor
Please note: The stated values are planning oids. Projects must only be calculated by authorised persons.

## MAIN-SECONDARY BEAM MUUTIPLE CONNECTION, SINGLE-ROW



| Ideefix |  |  | Timber Dimensions Min. cross section of secondary beam |  | Edge and centre distance |  | Main-secondary beam Multiple connection |  | Lood-bearing capacity Single-row |  | $\theta$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ns [ |  |  |  | $\begin{aligned} & \text { Edge } \\ & \text { distance } \end{aligned}$ | Centre distance | Drilling depth for SB | Drilling depth for MB | Perm. Values | Char. Values | Number of Connectors |
| $d_{c}$ | $\mathrm{ag}_{\mathrm{g}}$ | $V_{c}$ | w [mm] | h [mm] | [mm] | [mm] | [mm] | [mm] | $V_{z e}$. $[\mathrm{kN}]$ | R23,k[kN] | pc. |
| 30 | M12 | 3 | 80 | 80 | 50 | 50 | 20 | 7 | 4,32 | 8,94 | 1 |
| 40 | M16 | 5 | 120 | 120 | 60 | 60 | 25 | 10 | 6,98 | 14,66 | 1 |
| 50 | M20 | 5 | 160 | 160 | 80 | 80 | 30 | 15 | 10,88 | 21,09 | 1 |
| 30 | M12 | 3 | 80 | 150 | 50 | 50 | 20 | 10 | 8,64 | 17,88 | 2 |
| 40 | M16 | 5 | 120 | 180 | 60 | 60 | 25 | 15 | 13,96 | 29,32 | 2 |
| 50 | M20 | 5 | 160 | 240 | 80 | 80 | 30 | 20 | 21,76 | 42,18 | 2 |
| 30 | M12 | 3 | 80 | 200 | 50 | 50 | 20 | 10 | 12,96 | 26,82 | 3 |
| 40 | M16 | 5 | 120 | 240 | 60 | 60 | 25 | 15 | 20,94 | 43,98 | 3 |
| 50 | M20 | 5 | 160 | 320 | 80 | 80 | 30 | 20 | 32,64 | 63,27 | 3 |
| 30 | M12 | 3 | 80 | 250 | 50 | 50 | 20 | 10 | 17,28 | 35,76 | 4 |
| 40 | M16 | 5 | 120 | 300 | 60 | 60 | 25 | 15 | 27,92 | 58,64 | 4 |
| 50 | M20 | 5 | 160 | 400 | 80 | 80 | 30 | 20 | 43,52 | 84,36 | 4 |
| 30 | M12 | 3 | 80 | 300 | 50 | 50 | 20 | 10 | 21,60 | 44,70 | 5 |
| 40 | M16 | 5 | 120 | 360 | 60 | 60 | 25 | 15 | 34,90 | 73,30 | 5 |
| 50 | M20 | 5 | 160 | 480 | 80 | 80 | 30 | 20 | 54,40 | 105,45 | 5 |
| 30 | M12 | 3 | 80 | 350 | 50 | 50 | 20 | 10 | 25,92 | 53,64 | 6 |
| 40 | 116 | 5 | 120 | 420 | 60 | 60 | 25 | 15 | 41,88 | 87,96 | 6 |
| 50 | M20 | 5 | 160 | 560 | 80 | 80 | 30 | 20 | 65,28 | 126,54 | 6 |
| 30 | M12 | 3 | 80 | 400 | 50 | 50 | 20 | 10 | 30,24 | 62,58 | 7 |
| 40 | M16 | 5 | 120 | 480 | 60 | 60 | 25 | 15 | 48,86 | 102,62 | 7 |
| 50 | M20 | 5 | 160 | 640 | 80 | 80 | 30 | 20 | 76,16 | 117,63 | 7 |
| 30 | M12 | 3 | 80 | 450 | 50 | 50 | 20 | 10 | 34,56 | 71,52 | 8 |
| 40 | M16 | 5 | 120 | 540 | 60 | 60 | 25 | 15 | 55,84 | 117,28 | 8 |
| 50 | M20 | 5 | 160 | 720 | 80 | 80 | 30 | 20 | 87,04 | 168,72 | 8 |

## de is the diameter and the total height of the connector

ag is the metric connection thread of the connector
V c is the height of the integrated anti-wwist system - Fully threaded screw, GoFix ${ }^{(2)}$ FK
IF $305,0 \times 40 \mathrm{~mm} \cdot$ IF $406,0 \times 60 \mathrm{~mm} \cdot$ IF $508,0 \times 90 \mathrm{~mm}$
The connection is drawn together using a threaded rod or constructionscrew with a DIN 440 R washer
MB-SB connection as a mortise joint with simultaneous absorption of tensile forces
Rk characterisic value calculated according to DNN $1052: 2004-08$ Timber pk $380 \mathrm{~kg} / \mathrm{m}^{3} \mathrm{Nze}$. recommended permissible lood $\mathrm{R}_{1} \mathrm{k} \times 0,8 \mathrm{kmod}: 1,3 \mathrm{ym}: 1,4$. Fovtor 1,4 average load safety factor
Please note: The stated values are planning aids. Projects must only be calculated by authorised persons.

## Gurotec

## MAIN-SECONDARY BEAM MULTIPLE CONNECTION, DOUBLE-ROW



| IdeeFix |  |  | Timber <br> Dimensions <br> Min. cross section of secondary beam |  | Edge and centre distance |  | Main-secondary beam Multiple connection |  | Load-bearing capacity Single-row |  | $\theta 0$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | sions [ |  |  |  | Edge distance | Centre distance | Drilling depth for SB | Drilling depth for MB | Perm. Values | Char. Values | Number of connectors |
| $d_{c}$ | $\mathrm{ag}_{\mathrm{g}}$ | $V_{c}$ | w [mm] | h [mm] | [mm] | [mm] | [mm] | [mm] | $V_{z e}$. [kN] | R23,k[kN] | pc. |
| 30 | M12 | 3 | 150 | 80 | 50 | 50 | 20 | 10 | 8,64 | 17,88 | 2 |
| 40 | M16 | 5 | 180 | 120 | 60 | 60 | 25 | 15 | 13,6 | 29,32 | 2 |
| 50 | M20 | 5 | 240 | 160 | 80 | 80 | 30 | 20 | 21,76 | 42,18 | 2 |
| 30 | M12 | 3 | 150 | 150 | 50 | 50 | 20 | 10 | 17,28 | 35,76 | 4 |
| 40 | M16 | 5 | 180 | 180 | 60 | 60 | 25 | 15 | 27,92 | 58,64 | 4 |
| 50 | M20 | 5 | 240 | 240 | 80 | 80 | 30 | 20 | 43,52 | 84,36 | 4 |
| 30 | M12 | 3 | 150 | 200 | 50 | 50 | 20 | 10 | 25,92 | 53,64 | 6 |
| 40 | M16 | 5 | 180 | 240 | 60 | 60 | 25 | 15 | 41,88 | 87,96 | 6 |
| 50 | M20 | 5 | 240 | 320 | 80 | 80 | 30 | 20 | 65,28 | 126,54 | 6 |
| 30 | M12 | 3 | 150 | 250 | 50 | 50 | 20 | 10 | 34,56 | 71,52 | 8 |
| 40 | M16 | 5 | 180 | 300 | 60 | 60 | 25 | 15 | 55,84 | 117,28 | 8 |
| 50 | M20 | 5 | 240 | 400 | 80 | 80 | 30 | 20 | 87,04 | 168,72 | 8 |


| 30 | M12 | 3 | 150 | 300 | 50 | 50 | 20 | 10 | 43,20 | 89,40 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 40 | M16 | 5 | 180 | 360 | 60 | 60 | 25 | 15 | 69,80 | 146,60 |
| 50 | M20 | 5 | 240 | 480 | 80 | 80 | 30 | 20 | 108,80 | 210,90 |
| 30 | M12 | 3 | 150 | 350 | 50 | 50 | 20 | 10 | 51,84 | 1007,88 |
| 40 | M16 | 5 | 180 | 420 | 60 | 60 | 25 | 15 | 83,76 | 175,92 |
| 50 | M20 | 5 | 240 | 560 | 80 | 80 | 30 | 20 | 130,56 | 253,08 |


| 30 | M12 | 3 | 150 | 400 | 50 | 50 | 20 | 10 | 60,48 | 125,16 | 14 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 40 | M16 | 5 | 180 | 480 | 60 | 60 | 25 | 15 | 97,72 | 205,24 | 14 |
| 50 | M20 | 5 | 240 | 640 | 80 | 80 | 30 | 20 | 152,32 | 295,26 | 14 |
| 30 | M12 | 3 | 150 | 450 | 50 | 50 | 20 | 10 | 69,12 | 143,04 | 16 |
| 40 | M16 | 5 | 180 | 540 | 60 | 60 | 25 | 15 | 111,68 | 234,56 | 16 |
| 50 | M20 | 5 | 240 | 720 | 80 | 80 | 30 | 20 | 174,08 | 337,44 | 16 |

## $\mathrm{de}_{\mathrm{c}}$ is the diameter and the total height of the connector

ag is the metric connection thread of the connector
vcis the height of the integrated anti--wwiss system
Fully threaded screw, GoFix ${ }^{\circledR}$ FK IF $305,0 \times 40 \mathrm{~mm}$ - IF $406,0 \times 60 \mathrm{~mm}$ - IF $508,0 \times 90 \mathrm{~mm}$
The connection is drown together using a threaded rod or constructionscrew with a DIN 440 R washer
MB-SB connection as a mortise joint with simultaneous absorption of tensile forces
Rk characteristic value calculated according to DIN $1052: 2004-08$ Timber pk $380 \mathrm{~kg} / \mathrm{m}^{3} \mathrm{Nze}$. recommended permissible lood R,k $\times 0,8 \mathrm{kmod}: 1,3 \mathrm{ym}$ : 1,4 . Factor 1,4 average load safety factor
Please note: The stated values are planning cids. Projects must only be calculated by cuthorised persons.


## SONOTEC SOUND INSULATION CORK

## THE PERFECT SOLUTION FOR SOUND INSULATION

## ADVANTAGES

- Sustainable material
- High load bearing capacity
- Hidden installation
- Easy to use

- Impermeable to water and gas due to component-specific requirements


## MATERIAL

The Sonotec sound insulation cork is a combination of the components cork and natural rubber. This product is suitable for the application of vibration damping where very high isolation values are required and can be used as invisible insulators (pads/strips) with a low resonant frequency and medium to low load.

## LOAD ABSORPTION

Different loads have to be absorbed when decoupling the timber vertical truss from the concrete. These are located in the $0,1 \mathrm{~N} / \mathrm{mm}^{2}-3 \mathrm{~N} / \mathrm{mm}^{2}$ stat. permanent load range. A timber beam (C24 softwood) may only be loaded up to $2,5 \mathrm{~N} / \mathrm{mm}^{2}$ (characteristic) perpendicular to the grain. Our products cover load cases from $0,1 \mathrm{~N} / \mathrm{mm}^{2}-3 \mathrm{~N} / \mathrm{mm}^{2}$ ab. The cork can thus be used both in lightweight and solid construction with cross-laminated fimber (CLT).

## NOISE REDUCTION

The SonoTec sound insulation cork can reduce noise by up to 40 dB .



## Gurotec

## SONOTEC SOUND INSULATION CORK

THE PERFECT SOLUTION FOR SOUND INSULATION


| Art. no. | Name | Dimensions [mm] | Material thickness [mm] | PU |
| :--- | :--- | :--- | :--- | :--- |
| 945305 | skO2 | $80 \times 1100$ | 6 | 20 |
| 945306 | SK02 | $100 \times 1100$ | 6 | 20 |



| Art. no. | Name | Dimensions [mm] | Material thickness [mm] | PU |
| :--- | :--- | :--- | :--- | ---: |
| 945507 | SK03 | $80 \times 1100$ | 6 | 20 |
| 945308 | SK03 | $100 \times 1100$ | 6 | 20 |


| SonoTec sound insulation cork | Art. no. | Name | Dimensions [mm] | Material thickness [mm] | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Material: SK04 | 945309 | SKO4 | $80 \times 1100$ | 6 | 20 |
|  | 945310 | SKO4 | $100 \times 1100$ | 6 | 20 |

## SONOTEC SOUND INSULATION CORK FOR VARIOUS APPLICATIONS

## THE PERFECT SOLUTION FOR SOUND INSULATION




SonoTec for wooden support


SonoTec for invisible ground anchor


SonoTec for tiension rods (leff)
and tie bar simply (right)

| Art. no. | Dimensions [mm] | Material | Can be combined with |  | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Ar-Mr. | Name |  |
| 945311 | $6 \times 70 \times 230$ | SKO4 | 954088 | HH flat shearing ongle | 5 |
| 945312 | $4 \times 80 \times 230$ | SKO4 | 954180 | CII system angle | 5 |
| 945314 | $6 \times 100 \times 230$ | SKO4 | 954087 | HB lar shearing ongle | 5 |
| 945313 | $6 \times 120 \times 230$ | SKO4 | 954112 | Shearing angle $120 \times 230$ | 5 |

## Gurotec

## TECHNICAL DATA

|  | SKO2 | SKO3 | SKO4 |
| :---: | :---: | :---: | :---: |
| Temperature $\left[\mathrm{C}^{\circ}\right] /$ span width |  | Load ranges $\left[\mathrm{N} / \mathrm{mm}^{2}\right]$ | $-10 /+100$ |
| Density $\left[\mathrm{KG} / \mathrm{m}^{3}\right]$ | 700 | 1100 | $-10 /+100$ |
| Shore hardness $[$ shore A] | 35.50 | $45 \cdot 60$ | 1125 |
| Break rotatio $[\%]$ | $>200$ | $>300$ | 60.80 |
| Tensile strength $\left[\mathrm{N} / \mathrm{mm}^{2}\right]$ | $>2,0$ | $>5,0$ | $>100$ |
| $23^{\circ}(/ 70$ h compression $[\%]$ | $<15$ | $<15$ | $>6,0$ |

## IDENTIFYING THE CORRECT MATERIAL: AN EXAMPLE

We precisely identify the right material for you. So you still get an idea of how the right material is identified, we have outlined a sample identification process for you below.

First of all, we need the static continuous load that the sound insulation cork is to absorb. This is specified by the architect, structural engineer or stress analyst in question.
One of three different materials is selected depending on the static continuous load:


Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by outhorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

| Static continuous load $\mathrm{N} / \mathrm{mm}^{2}$ | Product | Dimensions $[\mathrm{mm}]$ | $80 \times 1100$ |
| :---: | :---: | :---: | :---: |
| $0,10-0,39$ | SKO2 | Art. no. |  |
| $0,10-0,39$ | SKO2 | $100 \times 1100$ | 945305 |
| $0,40-1,40$ | SKO3 | $80 \times 1100$ | 945306 |
| $0,40-1,40$ | SKO3 | 945307 |  |
| $1,50-3,10$ | SK04 | $100 \times 1100$ | 945308 |
| $1,50-3,10$ | SKO4 | $80 \times 1100$ | 945309 |

In the second step, the material's natural frequency is determined; this depends on the occurring load. The values are approximately taken from the following table.

|  |  | 6 mm |  |  | 12 mm |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { Lood } \\ {\left[\mathrm{N} / \mathrm{mm}^{2}\right]} \end{gathered}$ | Natural frequency <br> [ $\mathrm{Hz}_{2}$ ] | Deflection [mm] | Modulus of elasticity @10 Hz | Natural frequency <br> [ $\mathrm{Hz}_{2}$ ] | Deflection [mm] | Modulus of elasticity @10 Hz |
| SK02 | 0,1 | 44 | 0,2 | 4,0 | 27 | 0,5 | 3,7 |
|  | 0,2 | 33 | 0,5 | 4,5 | 19 | 1,3 | 4,0 |
|  | 0,3 | 27 | 0,8 | 5,6 | 17 | 1,9 | 5,1 |
|  | 0,4 | 27 | 1,1 | 6,9 | 17 | 2,6 | 6,5 |
| SK03 | 0,5 | 50 | 0,2 | 11,5 | 31 | 0,4 | 10,5 |
|  | 0,8 | 38 | 0,4 | 15,75 | 22 | 1,0 | 14,0 |
|  | 1,1 | 31 | 0,7 | 19,5 | 20 | 1,6 | 18,0 |
|  | 1,5 | 31 | 0,9 | 28,5 | 20 | 2,2 | 27,0 |
| SK04 | 1,6 | 58 | 0,3 | 18,5 | 36 | 0,6 | 17,0 |
|  | 2,4 | 44 | 0,6 | 24,5 | 25 | 1,3 | 22,0 |
|  | 3,2 | 35 | 1,0 | 30,5 | 23 | 2,0 | 28,0 |
|  | 4,0 | 35 | 1,5 | 43,0 | 23 | 2,7 | 41,0 |

*Values for SKO2 are based on test results provided by the University of Coimbra / Institute for Research and Technological Development in Construction Sciences. The values for SK03 and SKO4 are generalised. The ongoing tests confirm the values. The results will replace the described values.
As an example, the following sample calculation assumes a load of $0,3 \mathrm{~N} / \mathrm{mm}^{2}$. Our SKO2 material was chosen due to the specified load.
From the above table, we can see that the natural frequency must therefore be 27 Hz . We can illustrate this as follows in the graphs below.

## SK02 Natural frequency [Hz]



## Gurotec

In the next step, we take a closer look at the interference frequency.
To this end, we look at the graphs below and can thus conclude that the sound reduction in the low frequency range has deteriorated. Low frequencies (basses) can only be isolated by mass. The frequencies to be isolated for building acoustics start in the 80 Hz range, so this is negligible. 80 Hz can be assumed if no interference frequencies are specified.
The sound reduction in dB can be determined in two ways:
1:
Based on an interference frequency of 80 Hz , a sound reduction of approx.
17 dB can be read off the following graph. These values are achieved under ideal conditions (optimum room temperature, room humidity, etc.).


2:
A sound insulation factor can be calculated from the natural frequency identified previously ( 27 Hz ) and the specified interference frequency $(80 \mathrm{~Hz})$.

## Sound insulation factor $\mathrm{f} / \mathrm{fO}$ : Interference frequency / natural frequency $\rightarrow 80 \mathrm{~Hz} / 27 \mathrm{~Hz} \approx 2,96$

The sound reduction can then be read off based on the factor calculated previously. This is 17 dB under ideal conditions.

Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by outhorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.


In the last step, the material's deflection is identified.
This step is particularly important for the building's designers. The deflection is also identified using the continuous load, and there is a separate graph for each material. For the sample calculation with SKO2 and $0,3 \mathrm{~N} / \mathrm{mm}^{2}$, the following graph shows a deflection of $0,8 \mathrm{~mm} .7$

The graphs shown here are naturally adapted to the factors identified previously.

## SK02 Deflection [mm]



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For our SK03 and SKO4 materials, the following graphs apply to the deflection:

## SK03 Deflection [mm]



Please note: Verity the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by authorised persons in accordance wiht the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.


## PROPERTIES OF CORK

The cork bark has a honeycomb-shaped cell structure with over 40 million cells per $\mathrm{cm}^{3}$. The cells have a high proportion of an air-like gas mixture, which results in the cork's low weight on the one hand and the high compression capacity and elasticity on the other. The cork can therefore be compressed by up to half it size and can return to its original shape after compression.

Almost half of the cork bark is made up of suberin, a non-combustible biopolymer. The substance lines the individual cells and makes them impermeable to liquids and gases. The bark's structure and thickness protect the cork oak from heat, drying out and infections. This natural protective insulation makes cork oak an ideal insulating and sealing material for technical purposes.


Very good sound and thermal insulation
Impermeable to liquids and gases
Good resistance to fire and high temperatures
High frictional resistance
Compressible and elastic
Good wear resistance
Low weight - floats on water
Hypoallergenic and anti-static - does not absorb dust High flexibility - comfortable and soft

## Gurotec

## ENVIRONMENT

Cork is one of the most natural and environmentally friendly raw materials in the world. Cork oak is also the only tree that can completely regenerate itseff affer each harvest. The fact that cork can be recycled and revsed in new products makes it an ideal raw material with regard to sustainability.

## NATURAL RUBBER

Alongside cork, natural rubber is another natural and renewable raw material. Natural rubber is a rubber-like substance and is extracted from the milky sap (also known as latex) of the rubber tree. The rubber tree grows in the tropics of Africa, South America and Asia.
Natural rubber accounts for around $40 \%$ of global rubber production. In contrast, synthetic rubber is made using crude oil as a basis and consumes far more energy during the manufacturing and transport processes.

Natural rubber is made into various products, most of them are used in tyre production. Other applications include seals, binders and mattresses.


## SONOTEC ANGULAR DECOUPLER

## PERFECT COMPLEMENT TO THE EUROTEC SHEARING ANGLES AND THE CLT SYSTEM ANGLE

## ADVANTAGES

- Underlay enables straightforward assembly
- Sustainable material
- Invisible
- High load-bearing capacity
- REACH-compliant


## DESCRIPTION

The Eurotec SonoTec Angular Decoupler forms the perfect complement to the Eurotec shearing angles and the CLT System Angle. The underlay is made from SKO4, which is a compound formed from cork and natural rubber. The product is suitable for vibration damping applications in which very high insulation values are required. SonoTec angular decouplers are used as invisible insulators (pads/strips) with a low resonance frequency and a medium-low load.

## INSTRUCTIONS FOR USE

SonoTec angular decouplers feature cut-outs for concrete screws, making them suitable for use in concrete. The double layer allows an increase in the separation layer to 12 mm . The specifications for Sonotec SK04 Sound Insulation Cork apply. The material can be screwed through when used in wood. The application must be determined in advance by a structural engineer. No statement can be made regarding noise reduction since this is dependent on the construction.



| Art. no. | Dimensions [mm] | Material | Can be combined with |  | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Aft. no. | Name |  |
| 945311 | $230 \times 70 \times 6$ | SK04 | 954088 | HH flot sheoring ongle | 5 |
| 945312 | $230 \times 80 \times 6$ | SK04 | 954180 | CII sysiem ongle | 5 |
| 945314 | $230 \times 100 \times 6$ | SKO4 | 954087 | HB lat shearing angle | 5 |
| 945313 | $230 \times 120 \times 6$ | SKO4 | 954112 | Shearing ongle $120 \times 230$ | 5 |



## Gurotec

## BOLT ANCHOR

FOR FASTENING IN CONCRETE


ADVANTAGES
High load-bearing capacity

- Wide range of applications

Fewer fastening points required due to spreader clip

## INSTRUCTIONS FOR USE

The Eurotec Bolt anchor is a force-controlled expanding anchor for pushthrough installations. The galvanized steel bolt anchor is approved for use in non-cracked concrete, the stainless steel A4 bolt anchor for both non-cracked and cracked concrete. Despite the high load-bearing capacity, small axial and edge distances can be maintained. Different anchoring depths and dimensions allow a wide range of applications for connecting attachments of various materials to concrete. The A4 bolt anchor can be used both indoors and outdoors, while the galvanized steel bolt anchor can only be used indoors in dry conditions. Each Bolt anchor is equipped with an expansion clip, which ensures high load-bearing capacity and reduces the number of fastening points required.


| Bolt anchor A4 | \% $\times$ | Art. no. | Dimensions [mm] | Spanner gap | PU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| With washer, stainless steel A4, for cracked concrete and non-cracked concrete |  | 946142 | 8,0x 75 | SW13 | 100 |
|  |  | 946143 | 8,0 $\times 100$ | SW13 | 100 |
|  |  | 946144 | 10,0 $\times 100$ | SW17 | 50 |
|  |  | 946145 | 10,0 $\times 120$ | SW17 | 50 |
|  |  | 946146 | 10,0 $\times 140$ | SW17 | 50 |
|  |  | 946148 | 12,0x 140 | SW19 | 25 |


| Bolt anchor | Art. no. | Dimensions [mm] | Spanner gap | PU |
| :---: | :---: | :---: | :---: | :---: |
| With washer, electrogalvanised, for non-cracked concrete | 946170* | 6,0x55 | SwIo | 200 |
|  | 946671* | 6,0×85 | SwIo | 100 |
|  | 946172* | $8,0 \times 50$ | SW13 | 100 |
|  | 946173 | 8,0×75 | SW13 | 100 |
|  | 946174 | $8,0 \times 95$ | SW13 | 100 |
|  | 946175 | $8,0 \times 115$ | SW13 | 100 |
|  | 946176 | $8,0 \times 135$ | SW13 | 50 |
|  | 946177* | $10,0 \times 60$ | SW17 | 100 |
|  | 946178 | $10,0 \times 80$ | SW17 | 50 |
|  | 946179 | $10,0 \times 100$ | SW17 | 50 |
|  | 946180 | 10,0 $\times 120$ | SW17 | 50 |
|  | 946181 | $10,0 \times 140$ | Sw17 | 50 |
|  | 946182* | $12,0 \times 80$ | SW19 | 50 |
|  | 946183 | 12,0×95 | SW19 | 50 |
|  | 946184 | $12,0 \times 110$ | SW19 | 50 |
|  | 946185 | $12,0 \times 130$ | SW19 | 25 |
|  | 946186 | $12,0 \times 160$ | SW19 | 25 |
|  | 946187 | $12,0 \times 180$ | SW19 | 25 |
|  | 946188 | $16,0 \times 125$ | SW24 | 20 |
|  | 946189 | $16,0 \times 140$ | SW24 | 20 |
|  | 946190 | $16,0 \times 180$ | SW24 | 10 |
|  | nach DIN 400: |  |  |  |
|  | 946191 | $12,0 \times 200$ | SW19 | 20 |
|  | 946192 | $12,0 \times 220$ | SW19 | 20 |
|  | 946193 | $12,0 \times 240$ | SW19 | 15 |
|  | 946194 | $12,0 \times 260$ | SW19 | 15 |
|  | 946195 | $16,0 \times 220$ | SW24 | 10 |
|  | 946196 | $16,0 \times 240$ | SW24 | 10 |
|  | 946197 | $16,0 \times 260$ | SW24 | 10 |
|  | *Screws not regulated by EIA-14/0409 |  |  |  |

APPLICATION


1 Create drill hole


2 Clean drill hole thoroughly


Drive in bolt anchor with a hammer


Screw on the hexagonal nut until the appropriate torque is reached

## Eurotec

## TECHNICAL INFORMATION



| $\begin{gathered} \text { Dimensions } \\ {[\mathrm{mm}]} \end{gathered}$ | Min. Subsurface thickness hmin [mm] | Dilll diumeter <br> $\mathrm{do}_{0}[\mathrm{~mm}]$ | Min. Depith of drill hole | Min. Depth of drill hole | Max. Drill diameter in ottacheded part | Max. attuchment thickness | Installation torque |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0x Lengh |  |  |  |  |  |  | Tinst $[\mathrm{Nm}]$ |

Bolt anchor with washer according to DIN 125 A

| $6,0 \times 55^{*}$ | 100 | 6 | 50 | 35 | 7 | 5 | 11 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $6,0 \times 85 *$ | 100 | 6 | 50 | 35 | 7 | 35 | 11 |
| 8,0 $\times 50$ * | 100 | 8 | 55 | 30 | 9 | 5 | 15 |
| $8,0 \times 75$ | 100 | 8 | 55 | 40 | 9 | 15 | 15 |
| $8,0 \times 95$ | 100 | 8 | 55 | 40 | 9 | 35 | 15 |
| 8,0 $\times 115$ | 100 | 8 | 55 | 40 | 9 | 55 | 15 |
| $8,0 \times 135$ | 100 | 8 | 55 | 40 | 9 | 75 | 15 |
| $10,0 \times 60^{*}$ | 100 | 10 | 65 | 30 | 12 | 5 | 25 |
| 10,0x80 | 100 | 10 | 65 | 50 | 12 | 5 | 25 |
| $10,0 \times 100$ | 100 | 10 | 65 | 50 | 12 | 25 | 25 |
| $10,0 \times 120$ | 100 | 10 | 65 | 50 | 12 | 45 | 25 |
| $10,0 \times 140$ | 100 | 10 | 65 | 50 | 12 | 65 | 25 |
| $12,0 \times 80^{*}$ | 110 | 12 | 80 | 50 | 14 | 5 | 40 |
| $12,0 \times 95$ | 110 | 12 | 80 | 65 | 14 | 5 | 40 |
| $12,0 \times 110$ | 110 | 12 | 80 | 65 | 14 | 20 | 40 |
| $12,0 \times 130$ | 110 | 12 | 80 | 65 | 14 | 40 | 40 |
| $12,0 \times 160$ | 110 | 12 | 80 | 65 | 14 | 70 | 40 |
| $12,0 \times 180$ | 110 | 12 | 80 | 65 | 14 | 90 | 40 |
| $16,0 \times 125$ | 120 | 16 | 90 | 80 | 18 | 15 | 80 |
| $16,0 \times 140$ | 120 | 16 | 90 | 80 | 18 | 30 | 80 |
| $16,0 \times 180$ | 120 | 16 | 90 | 80 | 18 | 70 | 80 |

Bolt anchor with washer according to 0 IN 440

| $12,0 \times 200$ | 110 | 12 | 80 | 65 | 14 | 110 | 40 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $12,0 \times 220$ | 110 | 12 | 80 | 65 | 14 | 130 | 40 |
| $12,0 \times 240$ | 110 | 12 | 80 | 65 | 14 | 150 | 40 |
| $12,0 \times 260$ | 110 | 12 | 80 | 65 | 14 | 170 | 40 |
| $16,0 \times 220$ | 120 | 16 | 90 | 80 | 18 | 110 | 80 |
| $16,0 \times 240$ | 120 | 16 | 90 | 80 | 18 | 130 | 80 |
| $16,0 \times 260$ | 120 | 16 | 90 | 80 | 18 | 150 | 80 |

Bolt onthor A4

| $8,0 \times 75$ | 100 | 8 | 60 | 45 | 9 | 15 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $8,0 \times 100$ | 100 | 8 | 60 | 45 | 9 | 40 |
| $10,0 \times 100$ | 120 | 10 | 75 | 60 | 12 | 20 |
| $10,0 \times 120$ | 120 | 10 | 75 | 60 | 12 | 45 |
| $10,0 \times 140$ | 120 | 10 | 75 | 60 | 12 | 20 |
| $12,0 \times 140$ | 140 | 12 | 85 | 70 | 14 | 55 |

* Not reguluted by EAA-14/0409


ECS SOFTWARE
Do you already know the ECS calculation program? Here you can easily calculate all necessary information for your specific construction site. Of course, this also works with our other products.
3
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## Gurotec

## Sllent EPDM DECOUPLING PROFILE

## FOR SOUND INSULATION AND MATERIAL SEPARATION

## ADVANTAGES

Versatile applications

- Can be individually cut to size (supplied as a roll)

Ageing-resistant
. UV-stable

- Ozone-resistant

Free of conflict materials

## PROPERTIES

Density: approx. $1,4 \mathrm{~g} / \mathrm{cm}^{3}$
Usage temperature: $-30^{\circ} \mathrm{C}-+90^{\circ} \mathrm{C}$
Shore hardness $48=0,500 \mathrm{~N} / \mathrm{mm}^{2}=0,05 \mathrm{kN} / \mathrm{m}^{2}$

## INSTRUCTIONS FOR USE

Cut the decoupling profile to the desired length and place it in the chosen position, then fasten it in place at intervals of approx. $40-60 \mathrm{~cm}$, for example using the Eurotec Hammer tacker.


| Art. no. | Name | Thickness [mm] | Width [mm] | Lenght [mm] | Color | Material | PU |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 945382 | Silent EPM decoupling proile | 5 | 95 | 20 | Black | EPDM | 1 |


| Material properties |  |  |  |
| :---: | :---: | :---: | :---: |
| Property | Measurement method | Unit | Value |
| Hardness | DIN 507619 -1 | Shore A | 48 |
| Density | DIN5349 | $\mathrm{g} / \mathrm{m}^{3}$ | 1,23 |
| Tearstrengh | DIN5354 | MPa | 8,5 |
| Elongation of brak | DIW53504 | \% | 510 |
| Compresion set | DIW 150815-1 | \% | $\leq 40$ |
| Temperature resistance |  | ${ }^{\circ}$ | -30/100 ${ }^{\circ} \mathrm{C}$ |

Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned excusively by authorised persons in accordance with the State Building Code. As per LBauO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.


## Eurotec

## ECKTEC

## THE SPACE-SAVING ALTERNATIVE TO THE CONVENTIONAL BRACE

## ADVANTAGES

Supports load absorption with horizontal forces
Pre-assembly at the factory optional


Many different areas of use

## DESCRIPTION

The EckTec connector can replace the conventional brace.
This allows a better look without disruptive braces, especially at low installation heights.

## INSTRUCTIONS FOR USE

The EckTec connector is fixed with two $4 \times 40$ Paneltwistecs. The first KonstruX ST $8 \times 155$ fully-threaded screws are then set at $25^{\circ}$ in the posts. After mounting the cross beam, the other $8 \times 95$ KonstruX ST fully threaded screws can be set at $90^{\circ}$. Min. cross-section of beam: $120 \times 120 \mathrm{~mm}$.


| Load capacities EckTec 100 | M1,Rd $[\mathrm{kNm}]$ | F1,Rd $[\mathrm{kN}]$ |
| :--- | :--- | ---: |
| Timber $-\left(24, \mathrm{pk}=350 \mathrm{~kg} / \mathrm{m}^{3} ; \mathrm{kmod}=1,0\right.$ | 1,39 |  |
| Torque | 0,96 | 8,4 |
| Torque and traction (combined) |  |  |




## Gurotec

## INDIVIDUAL SOLUTIONS FOR COMPLEX CONSTRUCTIONS

Your construction site is a bit more complex and you are missing the perfect connector for special tasks? No problem!

On request, we manufacrute individual components, adapted to your needs, so that you can build worry-free!
Due to the ever-increasing popularity of wood as a building material in terms of environmental protection and cross laminated timber explicitly in building construction, we have increasingly focused on the topic of fastening and anchoring of prefabricated timber elements.

In this context, the efficiency as well as the quality of the products from the complex field of timber engineering is in the foreground. The core of this demanding architecture consists of complicated shapes, enormous spans of the structures as well as high static challenges. For our customers we are able to develop and manufacture unique solutions in these areas of modular construction. These include hall structures for industry, trade and agriculture; but also bridges or more complex roof structures.


## SPECIAL ELEMENTS

We offer customized solutions for your projects. From floor anchor plates with cross bracing in heavy timber construction connected by steel cables to cross flat connectors for heavily loaded timber connections with individual hole patterns.

Optimal load distribution thanks to individual adaptations to your projects
Better utilization of the individual connectors, for highly stressed junctions in engineered timber construction


## Eurotec

## EUROTEC MODULE CONNECTORS

Our new products include shearing angles, shearing plates, tie rods and tension straps. These are used for anchoring walls, columns and ceilings.

The special features of shearing angles are the different installation heights and the type of perforation, depending on the application.

In order to secure aligned components against shear forces, we also developed the shearing plate, which can be used in a variety of ways to cover all possible anchoring cases.

In our product range you will find several variants of the tension straps. They can be used to create timber-timber, timber-concrete and steel-steel connections. Special holes for bolting at an angle of $45^{\circ}$ make the tension straps particularly efficient and unique.

The Eurotec tie bar is used to absorb tensile forces to enable simple and fast base point anchoring of timber elements in timber, steel or concrete substrates.


## CONDITIONS OF SALE AND DELIVERY

All sales to buyers, customers and contract partners, hereinafter referred to as customers, are made exclusively subject to the following terms and conditions unless other agreements are made in writing in the individual case:

## 1. SCOPE, GENERAL PROVISIONS

Our terms and conditions shall apply exclusively! We will not accept contradictory terms and conditions of our customers that deviate from our conditions unless we have given our express written consent to their validity. Our terms and conditions shall apply even if we execute orders without reservation despite being aware of contradictory conditions or conditions that deviate from our terms and conditions. Our terms and conditions shall also apply to all future transactions with our customers. Customers can access the latest version of these Standard Terms and Conditions at www.eurotec.team at any time.

## 2. OFFERS, WRITTEN FORM

Our offers are non-binding and subject to alteration without notice until we issue our final order confirmation. Contracts and agreements, as well as transactions brokered by our representatives, shall become binding only when we issue our written order confirmation. Verbal agreements, even within the framework of contract execution, are not valid unless confirmed by us in writing.

## 3. PRICES, PACKAGING, OFFSETTING

Unless otherwise indicated by the order confirmation, our prices are ex-works and exclusive of packaging. This is billed separately. The minimum order value is $£ 50.00$. For smaller quantities, we charge a flat processing fee of $€ 30.00$.
a) Our prices are exclusive of statutory value added tax. This is stated and charged separately in the invoice at the statutory rate applicable on the date of billing.
b) Our customer may only claim a right of offsetting insofar as counterclaims are established to be legally binding or are undisputed or accepted. A right of retention may only be exercised with respect to counterclaims resulting from the same contractual relationship.

## 4. DELIVERY, DELIVERY PERIOD AND FORCE MAJEURE

Unless otherwise agreed in writing, the place of performance shall be our company premises. The goods are shipped at the customer's risk and expense by third parties acting on our behalf. From the time at which the goods are made ready for delivery and the customer has been informed of their readiness for shipping, the customer shall bear the risk of accidental loss or deterioration of the item. This shall apply even if shipping is delayed as a result of circumstances for which we are not responsible. Punctual handing over of the goods to a shipping company requires that the order be placed on time by our customer. If the goods are handed over to the appointed shipping company punctually, we will not be liable for delayed delivery to the customer. This shall apply even if a delivery deadline was agreed with the customer, especially in the case of delivery to a construction site. The customer may be exempted from rush charges incurred in relation to this if there is a legal basis for deducting this surcharge from the forwarder's bill.
Statements relating to delivery periods are always to be seen only as approximate and non-binding. They shall begin on the date of our order confirmation but not before all of the order details are clarified in full. They refer to the time of consignment ex-works and shall be considered met when the goods are reported to be ready for dispatch. Without prejudice to our rights arising due to the customer's default, they shall be extended by the period for which the customer is in arrears to us with respect to their obligations arising from this or other orders.
Even if they arise at our suppliers, the following grounds are among those that shall release us from the obligation to adhere to the delivery period and shall entitle us to extend the delivery periods, to make partial deliveries or to wholly or partially withdraw from the part of the contract that is not yet fuffilled without becoming liable to pay damages as a result, unless we are guilty of intent or gross negligence: interruptions of operations and difficulties in delivery of any kind, e. g. shortages of machinery, goods, materials or fuels, or incidents of force majeure, e. g. export and import embargos, fires, strikes, lock-outs or new official measures that adversely affect production costs and shipping.

## 5. SHIPPING

Goods are shipped at the expense and risk of the customer even if prepaid delivery was agreed. Additional costs for express shipping shall always be borne by the customer. Freight costs paid by us are to be seen only as an advancement of freight charges on behalf of the customer. Additional freight costs for urgent and express parcels shall be borne by the customer, even if we have borne the transport costs on individual occasions. Goods reported as ready for shipping must be accepted immediately and will be charged as exworks. If the goods are to be shipped abroad or passed directly to third parties, they must be examined and accepted in our factory; otherwise, the goods shall be deemed to have been delivered in accordance with the contract to the exclusion of any complaints. The risk, including that of confiscation, shall be transferred to the customer when the goods are handed over to the forwarder or freight carrier and, at the latest, when they leave our facility. Return shipments always require prior consultation with our internal sales depariment. Goods that are free of defects are only taken back with our express consent. A credit note is then issued for the value of the goods with deduction of a $25 \%$ return fee per item or against a minimum fee of $€ 50$ for returning the goods to storage. Strictly no debit notes are accepted.
6. DESIGN AND PROPERTY RIGHTS

The customer shall bear sole responsibility and be liable for ensuring that the goods it orders do not violate thirdparty property rights. No verification is performed on our part in this respect. The customer shall indemnify us against injunctions or claims for damages by third parties. If an iniunction is requested against us, the customer shall meet the legal costs and shall compensate us for the damages we have incurred.

## 7. ACCEPTANCE, QUANTITY TOLERANCES AND CALL-OFFS

For contracts with ongoing deliveries, the goods are to be accepted in monthly quantities that are as consistent as possible over the course of the contractual period. If a call-off is not made on time, we shall be entitled, after the expiry of a grace period that we have granted, to divide the order at our own discretion, withdraw from the part of the contract that has not yet been executed, or make a claim for damages due to non-performance. In the case of call-off orders, the call-offs must always be made within 12 calendar months. Over- or under-shipment by up to $10 \%$ of the order shall be permissible.

### 8.1 PAYMENT TERMS FOR INVOICES, RIGHT OF RETENTION

Invoices shall be payable with a $2 \%$ discount within 10 days of the invoice date or net within 30 days, regardless of when the goods are received and without prejudice to the right to make a complaint for defects. Payment by means of acceptance or customer's bill of exchange shall require special written agreement in advance. Discount charges will be charged in the case of payment by means of acceptance, which must have a term no longer than 3 months and be issued within 1 week of the invoice date. Credit notes for bills of exchange or cheques shall apply subject to receipt and regardless of the purchase price's earlier due date in the event of defaut by the customer. They shall be issued with the value at the date on which the equivalent amount will be available to us; the discount charges will be charged at the respective bank rate. In the event that the payment term is exceeded, interest and commissions
may be charged without prejudice to other rights at the respective bank rate for overdrafts but at a rate at least $5 \%$ above the respective discount rate of the Deutsche Bundesbank [German Federal Bank]. If the payment terms are not adhered to or we become aware of circumstances that, in our view, are sufficient to reduce the customer's credit worthiness, all of our claims shall become payable immediately regardless of the term of any bills of exchange that have been accepted or credited.
We shall then also be entitled to perform outstanding deliveries only in exchange for advance payment, to withdraw from the contract after a reasonable grace period, and to demand compensation for default. We may also prohibit the resale or processing of the delivered goods and demand their return or the transfer of indirect possession of the delivered goods at the customer's expense. The customer hereby already authorises us to enter its premises and confiscate the delivered goods in the above cases. We shall be entitled to the usual securities for our claims according to their nature and extent, even if they are subbect to conditions or of limited duration. Offsetting or withholding payments as a result of any counterclaims or notifications of defects shall be prohibited, except where claims are undisputed or established to be legally binding.

### 8.2 TERMS OF PAYMENT FOR WEB-SHOP CUSTOMERS

Payment shall be made exclusively in advance. Once the order process in our online shop is complete, you will receive an email with the bank details for our business account. The invoiced amount must be transferred to our account within 7 days. We cannot carry out your order until the payment arrives.

## 9. RETENTION OF TITLE

Until all liabilities arising from the business relationship are paid in full and, in particular, until all bills of exchange and cheques, including finance bills, given as payment are cashed, the goods delivered by us shall remain our property and may be taken back by us at the customer's expense in the event of default in payment. Until this point, the customer shall not be entitled to pledge or assign the goods to third parties as a security; it may sell them on or process them only within the framework of its ongoing business transactions. The customer shall be obliged to inform us immediately of any seizure by third parties of the goods delivered subject to retention of title.
In the event of further processing, the customer shall not acquire ownership of the goods delivered by us as set out in section 950 of the German Civil Code (BGB), as any processing is carried out by the customer on our behalf. Without prejudice to the rights of third-party suppliers, the newly created thing shall serve as security for us up to the amount of our total claims arising from the business relationship. It shall be kept safe for us by the customer and shall be regarded as goods for the purpose of these terms and conditions. If the item is intermixed or otherwise combined with other objects that to do not belong to us, we shall acquire at least co-ownership of the new thing in proportion to the value of the contract item to that of other objects that have been processed with it. If the customer sells the goods delivered by us, regardless of their condition, it hereby already assigns to us all claims against its customers arising from sales, as well as all ancillary rights, until all of our claims arising from delivery of goods are paid in full. At our request, the customer shall be obliged to notify its downstream customers of the assignment and to hand over the information and documents we require in order to assert our rights against its downstream customers.
If the total value of the securities given to us exceeds our claims arising from delivery by more than $20 \%$, we shall be obliged to retransfer securities to this extent at the customer's request. If the retention of fitle or assignment is invalid in the territory in which the goods are located, a security corresponding to the retention of title or assignment in this territory shall be deemed to be agreed. If the customer's cooperation is required in this process, it shall take all necessary measures to establish such rights.

## 10. NOTIFICATION OF DEFECTS, LIABILITY

Our customer shall be entitled to a warranty only if they have properly fulfilled their legal obligations under sections 377 and 378 of the German Commercial Code (HGB) with respect to the duties of examination and notification. If defects are present, we shall be entitled at our choice to either repair the defects or provide a replacement; if we are not prepared or not able to do so, and especially if repair/replacement is delayed beyond reasonable deadlines for reasons that we are responsible for, or if repair/replacement otherwise fails, our customer shall be entitled at its choice to withdraw from the contract or to demand a corresponding reduction in the price. Unless otherwise stipulated below, further claims of the customer shall be excluded regardless of their legal basis. We shall not be liable for damage that did not occur to the delivered item itself. In particular, we shall not be liable for lost profit or other pecuniary losses of the customer. The above exemption from liability shall not apply if the damage is caused by intent or gross negligence; it shall also not apply if the customer asserts claims for damages for non-performance due to the lack of a warranted characteristic. If we breach an essential contractual duty through negligence, our duty of reimbursement for property damage or personal injury shall be restricted to the level of cover provided by our product liability insurance.
We are prepared to allow the customer to view our policy. The warranty period is 6 months calculated from the date of transfer of risk. This period is a limitation period. The period shall also apply to claims under sections 1 and 4 of the German Product Liability Act (ProdHaftG). Insofar as our liability is excluded or restricted, this shall also apply to the personal liability of our employees, workers, staff, representatives and agents. Goods that are subject to a complaint must not be sent back without obtaining our prior written consent, as otherwise we may refuse to accept them at the sender's expense. Goods that have been partially or wholly processed will not be taken back under any circumstances. The customer is obliged to make sure that the purchased product is suitable for the intended application using technical descriptions, where available, and based on their specialist knowledge and to familiarise themselves with the application of this product. If they are not familiar with the product's application, our company staff are available to provide advice. All information and advice from our staff is provided carefully and conscientiously. Under no circumstances does this information and advice replace the indispensable consultancy services of architects and specialist planning companies or the services they provide during construction. Only the authorised professional groups are entitled to provide these services.

## 11. PLACE OF PERFORMANCE AND JURISDICTION, MISCELLANEOUS

Our company's registered office shall be the place of performance for all obligations arising from this contract, including liabilities from cheques and bills of exchange. Provided our customer is a merchant, the place of jurisdiction for all disputes arising from the contractual relationship shall be, at our choice, the Local Court of Hagen. Contracts with our customer shall be governed exclusively by German law to the exclusion of the UN Convention on Contracts for the International Sale of Goods of 11 April 1980. The language of the contract shall be German.

Hagen, 16. February 2018
E.,.r.o. Tec GmbH

Unter dem Hofe 5-58099 Hagen
Managing directors: Markus Rensburg, Gregor Mamys
Court of registration: Local Court of Registration number HRB 3817 VAT ID No.: DE 812674291
Tax number: 321/5770/0639
Tel. +4923316245-0 • Fax +49233162 45-200 • email inf@@urotec.team • www.eurotec.team

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## SO, <br> HOW CAN WE HELP YOU?


E.u.r.o.Tec GmbH

Unter dem Hofe 5-D.58099 Hagen
Te. +49 233162 45-0
Fax +49 $23316245-200$
E-Mail info@eurotecteam
wwweurofectean/en


[^0]:    Hole pattern with the Angle-bracket screw

[^1]:    Please note: Verify the assumptions made. The stated values, and type and number of joining devices are based on preliminary measurements. Projects are to be dimensioned exclusively by authorised persons in accordance with the State Building Code. As per LBuuO, please contact a qualified structural engineer for a paid proof of stability. We will be happy to refer you to someone.

[^2]:    Façade construction with the Topduo roofing screw.

[^3]:    $\square$ Panelłwistec countersunk head*Paneltwistec washer head* $\square$ Topduo flange button head screw**Topduo cylinder-head**

